

**Best
Available
Copy**

EXTENDED ARRAY EVALUATION PROGRAM:
SPECIAL REPORT NO. 14. EVALUATION OF THE
NOISE CHARACTERISTICS AND THE DETECTION
AND DISCRIMINATION CAPABILITIES OF THE
VERY LONG PERIOD EXPERIMENT (VLPE) SINGLE
STATIONS AND THE VLPE NETWORK

David G. Lambert, et al

Texas Instruments, Incorporated

Prepared for:

Advanced Research Projects Agency
Air Force Technical Applications Center

1 November 1973

DISTRIBUTED BY:

NTIS

National Technical Information Service
U. S. DEPARTMENT OF COMMERCE
5285 Port Royal Road, Springfield Va. 22151



ALEX(01)-STR-73-14

**EVALUATION OF THE NOISE CHARACTERISTICS AND THE DETECTION AND
DISCRIMINATION CAPABILITIES OF THE VERY LONG PERIOD EXPERIMENT
(VLPE) SINGLE STATIONS AND THE VLPE NETWORK**

SPECIAL REPORT NO. 14

EXTENDED ARRAY EVALUATION PROGRAM

Prepared by
D. G. Lambert, S. R. Prahl, and A. C. Strauss

TEXAS INSTRUMENTS INCORPORATED
Equipment Group
Post Office Box 6015
Dallas, Texas 75222

Prepared for
AIR FORCE TECHNICAL APPLICATIONS CENTER
AFTAC Project No. VELA T/2705/B/ASD
Alexandria, Virginia 22314

Sponsored by
ADVANCED RESEARCH PROJECTS AGENCY
Nuclear Monitoring Research Office
ARPA Program Code No. 2F10
ARPA Order No. 1714

1 November 1973

Acknowledgment: This research was supported by the Advanced Research Projects Agency, Nuclear Monitoring Research Office, under Project VELA-UNIFORM, and accomplished under the technical direction of the Air Force Technical Applications Center under Contract No. F33657-72-C-0725.

ABSTRACT

This report presents an evaluation of the noise characteristics of eight VLPE stations, the detection and discrimination capabilities of eleven VLPE stations, and the VLPE network.

Spatial and temporal noise relationships are presented for eight VLPE stations. Maximum likelihood m_b detection estimates show for the 50 percent detection threshold at single stations an m_b of about 4.7 and for the VLPE network an m_b of about 4.2. Matched filters applied to a selected suite of events increases the number of detections by a factor of two. The discrimination capability of the single VLPE stations and the VLPE network is presented in terms of M_s versus m_b , Love to Rayleigh wave amplitude ratios, and surface wave radiation patterns.

Neither the Advanced Research Projects Agency nor the Air Force Technical Applications Center will be responsible for information contained herein which has been supplied by other organizations or contractors, and this document is subject to later revision as may be necessary. The views and conclusions presented are those of the authors and should not be interpreted as necessarily representing the official policies, either expressed or implied, of the Advanced Research Projects Agency, the Air Force Technical Applications Center, or the US Government.

TABLE OF CONTENTS

| SECTION | TITLE | PAGE |
|---------|---|--------|
| | ABSTRACT | iii |
| I. | INTRODUCTION | I-1 |
| II. | DATA BASE | II-1 |
| | A. GENERAL DESCRIPTION FOR NOISE ANALYSIS | II-1 |
| | B. GENERAL DESCRIPTION FOR SIGNAL ANALYSIS | II-1 |
| | C. STATION CALIBRATIONS | II-7 |
| III. | VLPE SPATIAL AND TEMPORAL NOISE RELATIONSHIPS | III-1 |
| | A. INTRODUCTION | III-1 |
| | B. LONG-TERM BROAD-BAND VERTICAL EARTH NOISE | III-1 |
| | 1. METHOD OF ANALYSIS | III-1 |
| | 2. RESULTS | III-2 |
| | C. MAXIMUM TRACE AMPLITUDE VERSUS RMS | III-6 |
| | D. THREE COMPONENT HORIZONTAL RMS SPECTRA | III-6 |
| | 1. DISCUSSION | III-6 |
| | 2. VERTICAL AND HORIZONTAL RMS SPECTRA | III-10 |
| | 3. INTERCOMPONENT NOISE CORRELATION | III-10 |
| | E. SUMMARY | III-17 |
| IV. | VLPE DETECTION CAPABILITY | IV-1 |
| | A. INTRODUCTION | IV-1 |
| | B. MAXIMUM-LIKELIHOOD ESTIMATES OF DETECTION CAPABILITY | IV-1 |
| | 1. DISCUSSION | IV-1 |
| | 2. VLPE SINGLE STATION DETECTION CAPABILITY | IV-5 |

UNCLASSIFIED

Security Classification

AD 763 302

| DOCUMENT CONTROL DATA - R & D | | |
|---|--|--|
| (Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified) | | |
| 1. ORIGINATING ACTIVITY (Corporate author) Texas Instruments Incorporated Equipment Group Dallas, Texas 75222 | | 2a. REPORT SECURITY CLASSIFICATION UNCLASSIFIED |
| | | 2b. GROUP |
| 3. REPORT TITLE Evaluation of the Noise Characteristics and the Detection and Discrimination Capabilities of the Very Long Period Experiment (VLPE) Single Stations and the VLPE Network, Special Report No. 14 | | |
| 4. DESCRIPTIVE NOTES (Type of report and inclusive dates) Special | | |
| 5. AUTHOR(S) (First name, middle initial, last name) David G. Lambert, Sidney R. Prael, and Alan C. Strauss | | |
| 6. REPORT DATE 1 November, 1973 | 7a. TOTAL NO. OF PAGES 288 | 7b. NO. OF REFS 20 |
| 8a. CONTRACT OR GRANT NO. Contract No. F33657-72-C-0725 | 9a. ORIGINATOR'S REPORT NUMBER(S) ALEX(01)-STR-73-14 | |
| b. PROJECT NO. AFTAC Project No. VELA T/2705/B/ASD | 9b. OTHER REPORT NO(S) (Any other number(s) may be assigned this report) | |
| 10. DISTRIBUTION STATEMENT APPROVED FOR PUBLIC RELEASE, DISTRIBUTION UNLIMITED | | |
| 11. SUPPLEMENTARY NOTES ARPA Order No. 1714 | 12. SPONSORING MILITARY ACTIVITY Advanced Research Projects Agency Nuclear Monitoring Research Office Arlington, Virginia 22209 | |
| 13. ABSTRACT <p>This report presents an evaluation of the noise characteristics of eight VLPE stations, the detection and discrimination capabilities of eleven VLPE stations, and the VLPE network.</p> <p>Spatial and temporal noise relationships are presented for eight VLPE stations. Maximum likelihood m_b detection estimates show for the 50 percent detection threshold at single stations an m_b of about 4.7 and for the VLPE network an m_b of about 4.2. Matched filters applied to a selected suite of events increases the number of detections by a factor of two. The discrimination capability of the single VLPE stations and the VLPE network is presented in terms of M_s versus m_b, Love to Rayleigh wave amplitude ratios, and surface wave radiation patterns.</p> | | |

Reproduced by
NATIONAL TECHNICAL
INFORMATION SERVICE
U. S. Department of Commerce
Springfield VA 22151

DD FORM 1473
1 NOV 65

UNCLASSIFIED

Security Classification

UNCLASSIFIED

Security Classification

| 14 | KEY WORDS | LINK A | | LINK B | | LINK C | |
|----|----------------------------|--------|----|--------|----|--------|----|
| | | ROLE | WT | ROLE | WT | ROLE | WT |
| | VLPE | | | | | | |
| | VLPE Noise Characteristics | | | | | | |
| | VLPE Detection Thresholds | | | | | | |
| | VLPE Discrimination | | | | | | |
| | $M_s:m_b$ | | | | | | |
| | LQ/LR | | | | | | |
| | Radiation Patterns | | | | | | |
| | Maximum Likelihood | | | | | | |

UNCLASSIFIED

Security Classification

ia

TABLE OF CONTENTS
(continued)

| SECTION | TITLE | PAGE |
|---------|--|-------|
| | 3. VLPE NETWORK DETECTION CAPABILITY | IV-17 |
| C. | MIXED EVENT PROBABILITIES | IV-26 |
| D. | MATCHED FILTER AND THREE COMPONENT ADAPTIVE PROCESSOR PERFORMANCE | IV-29 |
| | 1. DISCUSSION | IV-29 |
| | 2. DATA BASE | IV-31 |
| | 3. MATCHED FILTER APPLICATION | IV-36 |
| | a. REFERENCE WAVEFORM FILTERS | IV-36 |
| | b. CHIRP MATCH FILTERS | IV-37 |
| | c. THE THREE COMPONENT ADAPTIVE PROCESSOR | IV-38 |
| | 4. SNNR GAINS-REFERENCE WAVEFORM AND CHIRP FILTERS | IV-39 |
| | 5. IMPROVEMENTS IN SURFACE-WAVE DETECTION | IV-52 |
| | 6. SUMMARY AND CONCLUSIONS | IV-59 |
| V. | VLPE DISCRIMINATION CAPABILITY | V-1 |
| A. | INTRODUCTION | V-1 |
| B. | M_s VERSUS m_b | V-1 |
| | 1. SINGLE VLPE STATIONS | V-1 |
| | 2. VLPE NETWORK | V-1 |
| | 3. SUMMARY | V-23 |
| C. | LOVE TO RAYLEIGH WAVE AMPLITUDE RATIOS (LQ/LR) | V-23 |
| D. | SURFACE WAVE RADIATION PATTERNS | V-30 |
| VI. | SUMMARY | VI-1 |
| A. | NOISE SUMMARY | VI-1 |
| B. | SUMMARY OF VLPE DETECTION CAPABILITY | VI-2 |

TABLE OF CONTENTS
(continued)

| SECTION | TITLE | PAGE |
|---------|---|--------|
| | C. SUMMARY OF VLPE DISCRIMINATION CAPABILITY | VI-3 |
| VII. | ACKNOWLEDGMENTS | VII-1 |
| VIII. | REFERENCES | VIII-1 |
| | APPENDIXES | |

LIST OF FIGURES

| FIGURE | TITLE | PAGE |
|--------|--|--------|
| II-1 | MAP WITH VLPE STATIONS AND GENERAL LOCATIONS OF EVENTS ANALYZED | II-3 |
| III-1 | VERTICAL GROUND NOISE AMPLITUDE AT VLPE STATIONS AT 20-40 SECOND PERIOD | III-3 |
| III-2 | VERTICAL GROUND NOISE AMPLITUDE AT VLPE STATIONS AT 17-25 AND 30-40 SECOND PERIODS | III-4 |
| III-3 | VERTICAL GROUND NOISE AMPLITUDE AT VLPE STATIONS AT 17-25 AND 30-40 SECOND PERIODS | III-5 |
| III-4 | MAXIMUM ZERO TO PEAK TRACE AMPLITUDE/ RMS AMPLITUDE AS A FUNCTION OF BAND- WIDTH | III-8 |
| III-5 | THREE COMPONENT GROUND NOISE SPECTRA AT EILAT, ISRAEL | III-11 |
| III-6 | THREE COMPONENT GROUND NOISE SPECTRA AT ALBUQUERQUE, NEW MEXICO | III-12 |
| III-7 | THREE COMPONENT GROUND NOISE SPECTRA AT LA PAZ, BOLIVIA | III-13 |
| III-8 | THREE COMPONENT GROUND NOISE SPECTRA AT MATSUSHIRO, JAPAN | III-14 |
| III-9 | INTERCHANNEL NOISE CROSS CORRELATION AT VLPE STATIONS | III-15 |
| III-10 | INTERCHANNEL NOISE CROSS CORRELATION AT VLPE STATIONS | III-16 |
| IV-1 | VLPE M_s VERSUS ALPA/NORSAR M_s | IV-3 |
| IV-2 | NORSAR M_s VERSUS ALPA M_s | IV-4 |
| IV-3 | DETECTION STATISTICS FOR VLPE STATION 1 (CTA) | IV-6 |
| IV-4 | DETECTION STATISTICS FOR VLPE STATION 2 (CHG) | IV-7 |
| IV-5 | DETECTION STATISTICS FOR VLPE STATION 3 (FBK) | IV-8 |
| IV-6 | DETECTION STATISTICS FOR VLPE STATION 4 (TLO) | IV-9 |
| IV-7 | DETECTION STATISTICS FOR VLPE STATION 5 (EIL) | IV-10 |

LIST OF FIGURES
(continued)

| FIGURE | TITLE | PAGE |
|--------|---|-------|
| IV-8 | DETECTION STATISTICS FOR VLPE STATION 6(KON) | IV-11 |
| IV-9 | DETECTION STATISTICS FOR VLPE STATION 7(OGD) | IV-12 |
| IV-10 | DETECTION STATISTICS FOR VLPE STATION 8(KIP) | IV-13 |
| IV-11 | DETECTION STATISTICS FOR VLPE STATION 9(ALQ) | IV-14 |
| IV-12 | DETECTION STATISTICS FOR VLPE STATION 10(ZLP) | IV-15 |
| IV-13 | DETECTION STATISTICS FOR VLPE STATION 11(MAT) | IV-16 |
| IV-14 | DETECTION STATISTICS FOR VLPE NETWORK 1 WITH AT LEAST ONE OPERATIONAL STATION | IV-20 |
| IV-15 | DETECTION STATISTICS FOR VLPE NETWORK 1 WITH AT LEAST TWO OPERATIONAL STATIONS | IV-21 |
| IV-16 | DETECTION STATISTICS FOR VLPE NETWORK 2 WITH AT LEAST ONE OPERATIONAL STATIONS | IV-22 |
| IV-17 | DETECTION STATISTICS FOR VLPE NETWORK 2 WITH AT LEAST TWO OPERATIONAL STATIONS | IV-23 |
| IV-18 | DETECTION STATISTICS FOR VLPE NETWORK 3 WITH AT LEAST ONE OPERATIONAL STATION | IV-24 |
| IV-19 | DETECTION STATISTICS FOR VLPE NETWORK 3 WITH AT LEAST TWO OPERATIONAL STATIONS | IV-25 |
| | LOCATION OF AREAS OF INTEREST | IV-35 |
| IV-21 | REFERENCE WAVEFORM FILTER IMPROVEMENT VERSUS REFERENCE WAVEFORM/TEST EVENT SEPARATION | IV-45 |
| IV-22 | CHIRP FILTER LENGTH VERSUS DISTANCE (TRANSVERSE COMPONENT) | IV-51 |
| IV-23 | CHIRP FILTER LENGTH VERSUS DISTANCE (VERTICAL COMPONENT) | IV-51 |
| IV-24 | SURFACE WAVE DETECTION DATA FOR REFERENCE WAVEFORM FILTER VERSUS BANDPASS FILTER | IV-53 |
| IV-25 | SURFACE WAVE DETECTION DATA FOR CHIRP FILTER VERSUS BANDPASS FILTER | IV-54 |

LIST OF FIGURES
(continued)

| FIGURE | TITLE | PAGE |
|--------|--|-------|
| IV-26 | SURFACE WAVE DETECTION DATA FOR COMBINED REFERENCE WAVEFORM AND CHIRP FILTERS VERSUS BANDPASS FILTER | IV-56 |
| IV-27 | SURFACE WAVE DETECTION DATA FOR THE NETWORK MATCHED FILTER VERSUS NETWORK BANDPASS FILTER | IV-57 |
| IV-28 | SURFACE WAVE DETECTION DATA FOR THE TCA PROCESSOR VERSUS BANDPASS FILTER. | IV-58 |
| V-1 | M_s VERSUS m_b AT CTA, 6/1/72 - 12/31/72 | V-3 |
| V-2 | M_s VERSUS m_b AT CHG, 1/1/72 - 12/31/72 | V-4 |
| V-3 | M_s VERSUS m_b AT FBK, 1/1/72 - 3/20/72 | V-5 |
| V-4 | M_s VERSUS m_b AT TLO, 1/1/72 - 8/31/72 | V-6 |
| V-5 | M_s VERSUS m_b AT EIL, 6/1/72 - 12/31/72 | V-7 |
| V-6 | M_s VERSUS m_b AT KON, 1/1/72 - 12/31/72 | V-8 |
| V-7 | M_s VERSUS m_b AT OGD, 1/1/72 - 8/31/72 | V-9 |
| V-8 | M_s VERSUS m_b AT KIP, 6/1/72 - 12/31/72 | V-10 |
| V-9 | M_s VERSUS m_b AT ALQ, 6/1/72 - 12/31/72 | V-11 |
| V-10 | M_s VERSUS m_b AT ZLP, 12/1/72 - 12/31/72 | V-12 |
| V-11 | M_s VERSUS m_b AT MAT, 12/22/72 - 12/31/72 | V-13 |
| V-12 | M_s VERSUS m_b (M_s DETERMINED BY ONE OR MORE VLPE STATION ESTIMATES) | V-21 |
| V-13 | M_s VERSUS m_b (M_s DETERMINED BY TWO OR MORE VLPE STATION ESTIMATES) | V-22 |
| V-14 | LOVE TO RAYLEIGH WAVE AMPLITUDE RATIOS OF EURASIAN EVENTS SEEN BY VLPE STATIONS | V-24 |
| V-15 | LOCATION OF SEISMIC REGIONS | V-27 |
| V-16 | THEORETICAL AND OBSERVED LQ/LR RADIATION PATTERN FOR EVENT 97. | V-32 |
| V-17 | THEORETICAL AND OBSERVED LQ/LR RADIATION PATTERN FOR EVENT 105. | V-33 |

LIST OF TABLES

| TABLE | TITLE | PAGE |
|-------|---|-------|
| II-1 | VERY LONG PERIOD EXPERIMENT (VLPE) STATIONS AND LOCATIONS | II-2 |
| II-2 | VLPE DIGITAL DATA AVAILABLE AT SDAC AS OF AUGUST 31, 1973 | II-4 |
| II-3 | SUMMARY OF EVENTS PROCESSED FOR JANUARY 1, 1972 - MARCH 20, 1972, JUNE 1, 1972 - AUGUST 31, 1972, AND NOVEMBER 1, 1972 - DECEMBER 31, 1972 | II-5 |
| III-1 | MAXIMUM ZERO TO PEAK TRACE AMPLITUDE VERSUS RMS AMPLITUDE FOR VLPE STATIONS | III-7 |
| III-2 | VERY LONG PERIOD EXPERIMENT (VLPE) STATIONS AND LOCATIONS | III-9 |
| IV-1 | VLPE SINGLE STATION DETECTION THRESHOLDS IN TERMS OF m_b and M_s | IV-19 |
| IV-2 | VLPE NETWORK DETECTION THRESHOLDS IN TERMS OF m_b and M_s | IV-27 |
| IV-3 | NETWORK MIXED EVENT PROBABILITY STATISTICS | IV-28 |
| IV-4 | EARTHQUAKE EVENT LIST | IV-32 |
| IV-5 | PRESUMED EXPLOSION EVENT LIST | IV-34 |
| IV-6 | RESULTS OF REFERENCE WAVEFORM FILTERING | IV-40 |
| IV-7 | RESULTS OF CHIRP FILTERING | IV-46 |
| V-1 | VLPE NETWORK RAYLEIGH WAVE MAGNITUDES (M_s) | V-15 |
| V-2 | TABLE OF ARITHMETIC MEANS OF LOG (LQ/LR) VALUES AND THEIR RESPECTIVE VARIANCES AND ANTILOGS (AS A FUNCTION OF REGION) | V-26 |
| V-3 | TABLE OF ARITHMETIC MEANS OF LQ/LR RATIOS (AS A FUNCTION OF REGION AND STATION) | V-29 |

SECTION I

INTRODUCTION

This report presents an evaluation of the noise characteristics of eight of the Very Long Period Experiment (VLPE) single stations and the detection and discrimination capabilities of eleven VLPE stations and the VLPE network. The purpose of the VLPE is to improve detection and discrimination capabilities with the use of a small network of high gain, high quality, long-period digital seismographs at various locations throughout the world.

The VLPE instrumentation has been described in detail by Pomeroy, et. al., (1969), and studies of the data from the station of Ogdensburg, New Jersey have been presented by Savino, et. al., (1971). A general review of eight of the long-period stations with their capabilities and the application of various filter techniques on digitally recorded data have also been given by Savino, et. al., (1972).

Recent reports by Alsup and Becker (1973a, 1973b) describe the vertical and three component structure of the earth noise for eight VLPE stations. Lambert and Becker (1973) presented the preliminary detection and discrimination capabilities of nine VLPE stations, the VLPE network, and the VLPE-NORSAR-ALPA combined network.

The data base for this report extends the study of vertical and horizontal earth noise with VLPE data during November and December 1972, and January 1973. The data base for the signal analysis is extended and consists of 874 Eurasian events for a total of 3577 event-station combinations. The results of techniques applied to these data include the following:

- An analysis of the long-term broad band vertical earth noise, maximum trace amplitude versus RMS amplitude, three component broad band earth noise, and intercomponent noise correlation.
- Maximum-likelihood estimates of detection capability based on m_b for VLPE single stations and the VLPE network.
- The estimated reduction of mixed events in terms of probabilities for various VLPE networks based on the present VLPE capability.
- Preliminary analysis of the Matched filters and Three Component Adaptive processor on a restricted suite of events.
- Discrimination capability of single VLPE stations and the VLPE network as functions of M_s versus m_b , Love to Rayleigh wave amplitude ratios, and surface wave radiation patterns.

In Section II, the data base is presented in detail with a complete listing of all event data and the calibration curves for all VLPE stations. Section III presents the VLPE spatial and temporal noise relationships. In Sections IV and V, we present the detection and discrimination capabilities of the VLPE single stations and the VLPE network. Finally, conclusions based on this analysis and recommendations for future studies are given in Section VI.

SECTION II

DATA BASE

A. GENERAL DESCRIPTION FOR NOISE ANALYSIS

The data base for the VLPE noise analysis consists of 379 one hour vertical noise samples for stations in Australia (CTA), Thailand (CHG), Israel (EIL), Norway (KON), Hawaii (KIP), New Mexico (ALQ), Bolivia (ZLP) and Japan (MAT) during November and December 1972, and January 1973. In addition, 133 one hour horizontal noise samples were analyzed for stations at EIL, ALQ, ZLP, and MAT.

B. GENERAL DESCRIPTION FOR SIGNAL ANALYSIS

We use digital recordings from all available VLPE stations for Eurasian events during three time periods: January 1, 1972 through March 20, 1972, June 1, 1972 through August 31, 1972, and November 1, 1972 through December 31, 1972. The first time period (Network 1) includes station data from Thailand (CHG), Alaska (FBK), Spain (TLO), Israel (EIL), Norway (KON), and New Jersey (OGD). The second time period (Network 2) includes data from Australia (CTA), Thailand (CHG), Spain (TLO), Israel (EIL), Norway (KON), New Jersey (OGD), Hawaii (KIP) and New Mexico (ALQ). The third time period (Network 3) includes data from CTA, CHG, EIL, KON, OGD, KIP, ALQ, Bolivia (ZLP) and Japan (MAT). The geographic location of each station is given in Table II-1 and shown in Figure II-1.

Tapes that were available for processing for the year 1972 covering the three time periods are listed in Table II-2. Attempts were made to process and analyze all available data. Table II-3 summarizes the number of events processed at each station. A considerable amount of data was lost

TABLE II-1
 VERY LONG PERIOD EXPERIMENT (VLPE)
 STATIONS AND LOCATIONS

| Station | Designator | Latitude | Longitude |
|---------------------------|------------|----------|-----------|
| Charter Towers, Australia | CTA | 20.09S | 146.26E |
| Chiang Mai, Thailand | CHC | 18.79N | 98.98E |
| Fairbanks, Alaska | FBK | 64.90N | 148.01W |
| Toledo, Spain | TLO | 39.86N | 4.02W |
| Eilat, Israel | EIL | 29.55N | 34.95E |
| Kongsberg, Norway | KON | 59.65N | 9.59E |
| Ogdensburg, New Jersey | OGD | 41.07N | 74.62W |
| Kipapa, Hawaii | KIP | 21.42N | 158.02W |
| Albuquerque, New Mexico | ALQ | 34.94N | 106.46W |
| Lapaz, Bolivia | ZLP | 16.50S | 68.13W |
| Matsushiro, Japan | MAT | 36.54N | 138.21E |

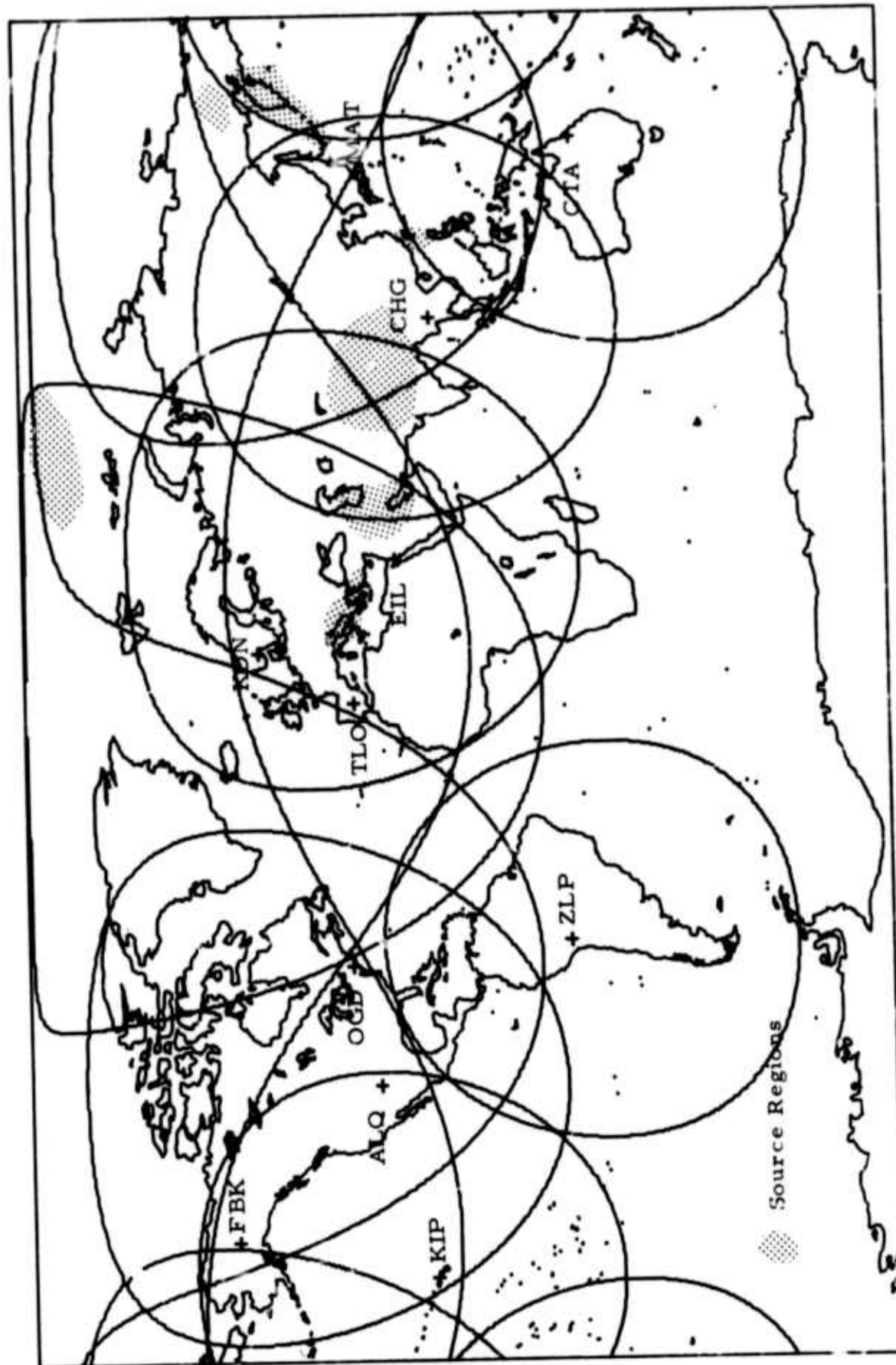


FIGURE II-1

MAP OF VLPE STATIONS AND CIRCLES AROUND EACH SITE WITH RADIUS OF 50° DISTANCE

TABLE II-2
VLPE DIGITAL DATA AVAILABLE AT SDAC
AS OF AUGUST 31, 1973
* Test Tape

| Year 1972 | CTA | CHG | FBK | TLO | EIL | KON | OGD | KIP | ALQ | ZLP | MAT |
|-----------|--------------|----------------|------|---------------|--------------|---------------|------------------------|---------------|---------------|---------------|-------|
| January | | 1-31 | 1-31 | 1-31 | | 1-31 | 1-31 | | | | |
| February | 19-20* | 1-29 | 1-29 | 1-24 28-29 | 24-25 | 1-29 | 1-29 | | | | |
| March | | 1-4 15-26 | 1-31 | 1-28 | 10-31 | 1-3 6-31 | 1-14 | 15-31 | 31 | | |
| April | 24-30 | 1-27 | 1-25 | 1-26 | 1-5 9-24 | 1-12 17-30 | 6-30 | 1-30 | 1-30 | | |
| May | 1-31 | 30-31 | | 11-26 | 5-31 | 1-31 | 1-4 30-31 | 1-11 14-31 | 1-19 30-31 | | |
| June | 1-30 | 1-12 | | 10-30 | 1-30 | 1-30 | 1 6-30 | 1-30 | 1-30 | | |
| July | 1-31 | | | 1-31 | 1-31 | 1-31 | 1-31 | 1-31 | 1-31 | | |
| August | 1-31 | 17-18 25-30 | | 1-31 | 1-31 | 1-31 | 1-21 24-28 30-31 | 1-31 | 1-7 31 | | |
| September | 1-30 | 22-28 | | 1-30 | 1-2 15-18 | 1-30 | 1-21 29-30 | 1-30 | 1-31 | | |
| October | 1-31 | | | 1-26 | 11-23 | 1-31 | 1-6 | 1-31 | 1-31 | | |
| November | 1-30 | 3-30 | | | | 1-30 | 7-10 18-27 30 | 1-30 | 1-5 10-30 | 4-24 26-30 | |
| December | 1-7 11-31 | 1-31 | | | 3-31 | 1-31 | 1-31 | 1-31 | 1-31 | 1-31 | 22-31 |

TABLE II-3

SUMMARY OF VLPE EVENTS PROCESSED FOR
 JANUARY 1, 1972 - MARCH 20, 1972,
 JUNE 1, 1972 - AUGUST 31, 1972, AND
 NOVEMBER 1, 1972 - DECEMBER 31, 1972

| Station Number | Station Code | Events Processed | Events Detected | Events Not Detected | Mixed Events | System Clipping Spikes, etc. |
|----------------|--------------|------------------|-----------------|---------------------|--------------|------------------------------|
| 1 | CTA | 313 | 73 | 135 | 71 | 34 |
| 2 | CHG | 387 | 119 | 140 | 87 | 41 |
| 3 | FBK | 298 | 67 | 186 | 40 | 5 |
| 4 | TLO | 463 | 130 | 229 | 93 | 11 |
| 5 | EIL | 363 | 100 | 171 | 50 | 42 |
| 6 | KON | 485 | 153 | 226 | 101 | 5 |
| 7 | OGD | 263 | 51 | 113 | 34 | 65 |
| 8 | KIP | 543 | 136 | 225 | 132 | 50 |
| 9 | ALQ | 331 | 50 | 125 | 73 | 83 |
| 10 | ZLP | 107 | 15 | 52 | 26 | 14 |
| 11 | MAT | 24 | 6 | 10 | 3 | 5 |
| Totals | | 3577 | 900 | 1612 | 710 | 355 |

during the first half of 1972 (January through June) due to operational and recording problems (see Lambert and Becker, 1973, for details). The quality of data improved significantly during the latter part of 1972 and in fact, virtually all field data tapes processed were useable.

The results are tabulated in Appendix II-B through II-L for each station with appropriate comments. A total of 3577 event-station combinations are listed; many events were recorded at several stations.

A total of 874 Eurasian events or 862 earthquakes and 12 presumed explosions are tabulated in Appendix II-A. Information for each event includes the date, origin time, epicenter location, m_b , the seismic region, and a code indicating the source list for the event. Events 116, 260, 339, 456, 626, 652, 672, 679, 699, 755, 797, and 865 are presumed to be explosions. (Three events, numbers 277, 291, and 351 from Western Idaho, California - Mexico border, and Easter Island region were inadvertently included in the list and were processed and analyzed with the 874 Eurasian events.)

The detection capability based on the presence of Love waves was not attempted. Erratic static gains were encountered from time to time on the horizontal components at most stations and especially during the first half of 1972. However, Love wave amplitudes were measured when possible.

We reviewed the m_b determinations for all events where possible to determine whether any regional or near regional m_b values were included in the average m_b . It was found that the PDE lists several events from Italy where near station values of m_b had been included. The reported m_b values for these events were from 0.2 to 0.6 magnitude units larger than the average of the teleseismic values. We accepted only the teleseismic m_b values as valid estimates. Those values of m_b which were changed are recorded and noted with an asterisk in Appendixes II-B through II-L. The original m_b values are listed in Appendix II-A. All graphs in this report which have m_b values as parameters use the revised teleseismic m_b values.

C. STATION CALIBRATIONS

The instrument calibration and system response data were originally supplied by Lamont Doherty Geological Observatory and more recently by the Albuquerque Seismological Center, Environmental Research Laboratories of NOAA. These data are shown for all of the VLPE stations in Appendix II-M.

SECTION III

VLPE SPATIAL AND TEMPORAL NOISE RELATIONSHIPS

A. INTRODUCTION

The vertical structure of earth noise for VLPE stations at Australia (CTA), Thailand (CHG), Alaska (FBK), Spain (TLO), Israel (EIL), Norway (KON), New Jersey (OGD), and Hawaii (KIP) was reported by Alsup and Becker (1973a). A total of 604 one hour noise samples was included in the above analysis for parts of August through October 1971, and June through August 1972.

Alsup and Becker (1973b) have also reported on the three component structure of earth noise for 491 one hour noise samples and for the corresponding stations and times indicated above.

This report extends the study of vertical and horizontal earth noise for VLPE data during November and December 1972, and January 1973, and includes 379 one hour vertical noise samples for stations in Australia (CTA), Thailand (CHG), Israel (EIL), Norway (KON), Hawaii (KIP), New Mexico (ALQ), Bolivia (ZLP), and Japan (MAT). Further, a total of 133 one hour horizontal noise samples was analyzed for stations EIL, ALQ, ALP, and MAT.

B. LONG-TERM BROAD BAND VERTICAL EARTH NOISE

1. Method of Analysis

Each one hour noise sample was selected from digital VLPE recordings free of seismic events. Root-mean-square (RMS) ground motion amplitudes, $m\mu$ (i.e. corrected for instrument response) were determined for three period bands of 17 to 25 seconds, 20 to 40 seconds, and 30 to 40 seconds. The 20-40 second band is intended to show long term gross trends while the 17-25 and 30-40 second bands are intended to show contrasts and variability of the trends.

2. Results

Figure III-1 shows the RMS amplitude ($m\mu$) in the 20-40 second period band versus Julian day (1972-1973) for stations CTA, CHG, EIL, KON, KIP, ALQ, ZLP, and MAT. CHG, KIP, KON, and ALQ had data for most of the 90 day time period (November, December 1972, and January 1973) studied. Stations CTA, EIL, ZLP, and MAT could be sampled only intermittently due to data being unavailable or unreadable.

In general, we observe a relatively stable low level of noise at most stations with the exception of CHG which had high and variable noise levels during November and December 1972. At all stations RMS amplitudes are observed to rise above the base level by factors of four to five over a one to two day period and then return to the base level. Based on the past data (Alsup and Becker 1973 a) and these data, it appears that there are slowly changing long term seasonal variations in the noise fields at most VLPE sites, although nothing definitive can be said at this time.

Figures III-2 and III-3 show the RMS amplitude ($m\mu$) for the 17 to 25 second and 30 to 40 second period bands versus Julian day (1972 and 1973). The dot represents the 17 to 25 second period band and the triangle denotes the 30 to 40 second period band. Availability of data was the same as for the 20 to 40 second period band discussed above. We observe the following:

- The RMS amplitudes ($m\mu$) in the 30 to 40 second period band are less variable and on the average two to four times lower than the RMS amplitudes ($m\mu$) in the 17 to 25 second period band.
- Generally, RMS amplitudes do not increase or decrease in unison between period bands over short periods of time. This suggests that the noise in these two period bands is relatively uncorrelated.

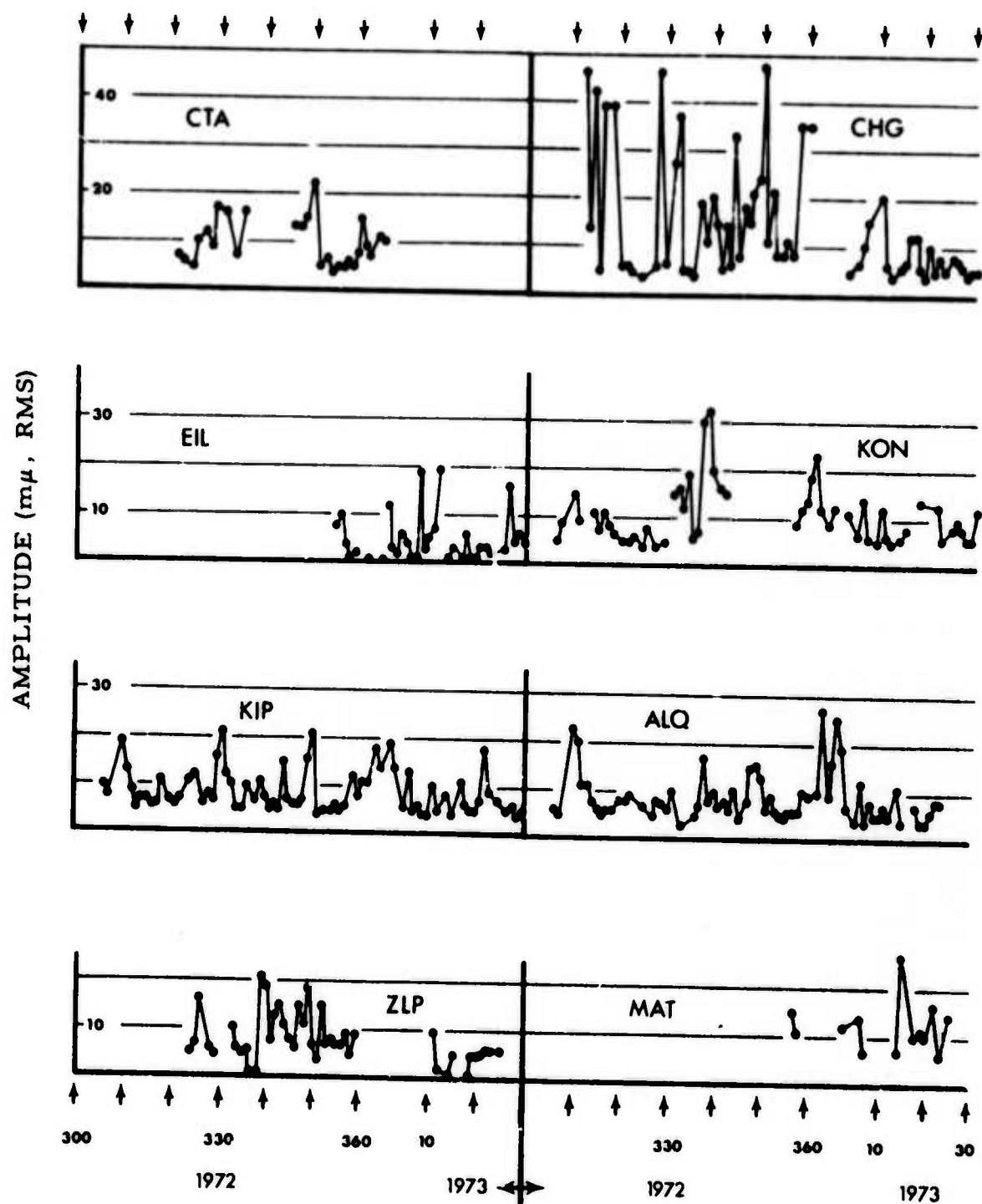


FIGURE III-1
VERTICAL GROUND NOISE AMPLITUDE AT
VLPE STATIONS AT 20-40 SECONDS

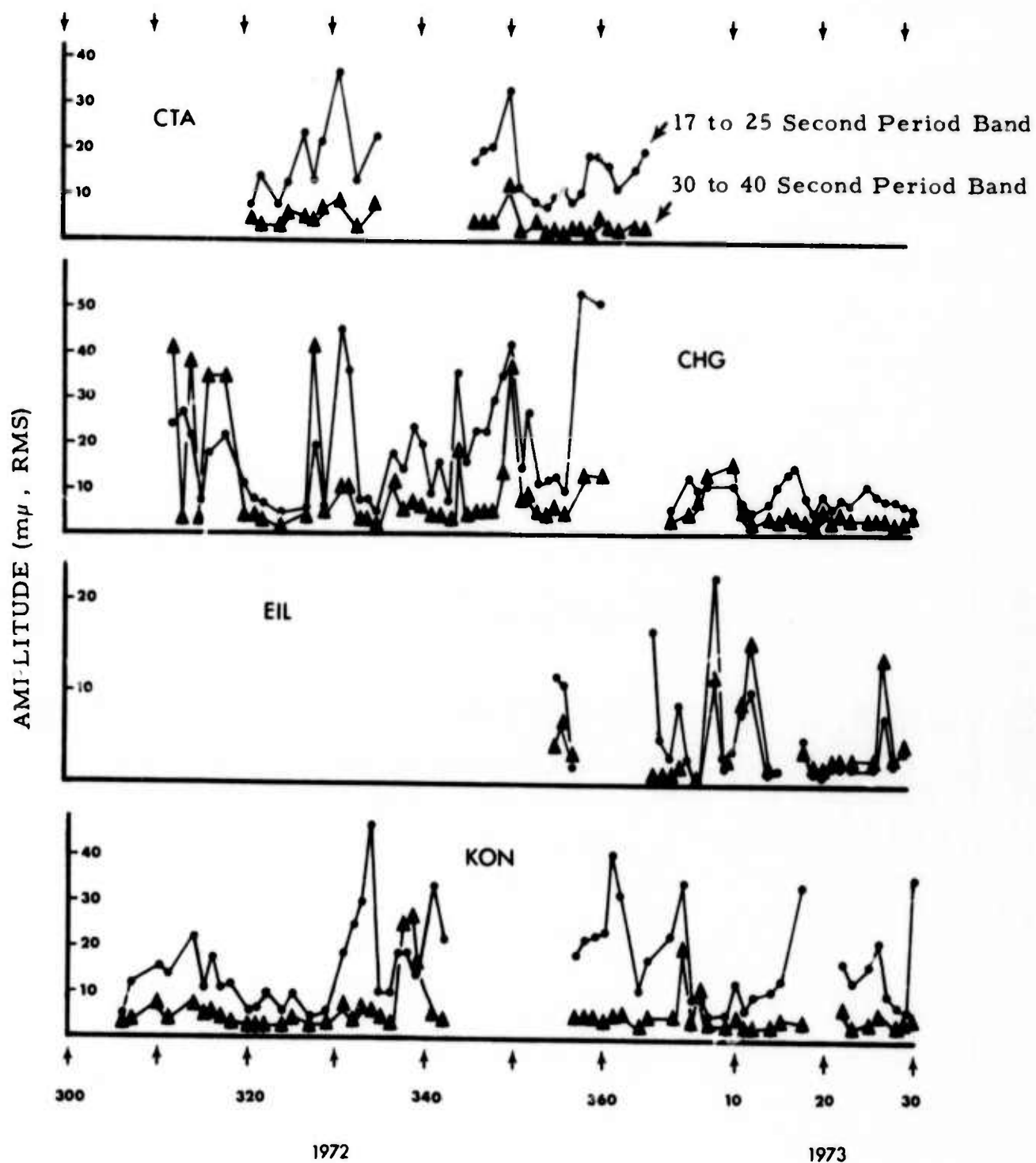


FIGURE III-2
VERTICAL GROUND NOISE AMPLITUDE AT VLPE STATIONS
AT 17-25 AND 30-40 SECONDS

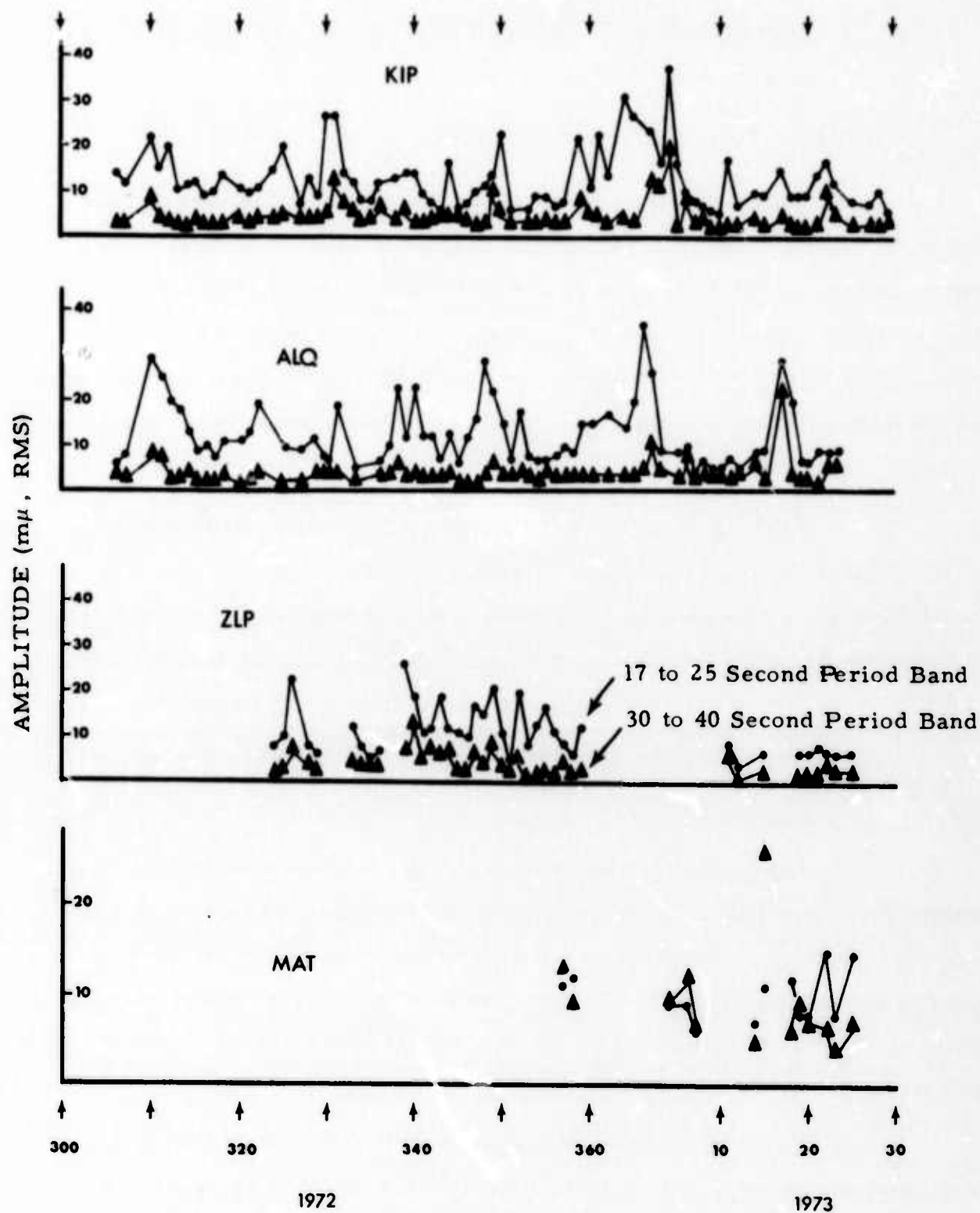


FIGURE III-3
VERTICAL GROUND NOISE AMPLITUDE AT VLPE STATIONS
AT 17-25 AND 30-40 SECONDS

- Correspondence between 20 to 40 second and 30 to 40 second period bands is observed at all stations.

C. MAXIMUM TRACE AMPLITUDE VERSUS RMS AMPLITUDE

Maximum zero to peak noise trace amplitudes versus RMS amplitude in period bands of 17 - 25, 20 - 40, and 30 - 40 seconds were determined in the following manner. One hundred seventy, one hour noise samples from March and November of 1972 were bandpass filtered in the period bands described above and then RMS amplitudes were computed and the maximum zero-to-peak (ZP) trace amplitudes were measured within the same period bands.

Table III-1 lists the ZP/RMS amplitude ratios (uncorrected for instrument response) and their standard deviations for each station. Figure III-4 shows the relationship between the bandwidth over which the RMS amplitudes were determined and the ZP/RMS amplitude ratios. An increase in the bandwidth yields an increase in the ZP/RMS amplitude ratio.

D. THREE COMPONENT BROAD BAND EARTH NOISE

1. Discussion

Simultaneous three component earth noise structure at VLPE stations was reported by Alsup and Becker (1973b) for 491 hours of noise sampling. Times and stations covered were the same as for the vertical earth noise mentioned above. This report includes supplementary data on stations not covered by Alsup and Becker. Total hours of data examined from each station studied are listed in Table III-2.

One hour samples of the noise field from the vertical, north-south, and east-west VLPE digital output recordings were analyzed in a manner similar to the vertical earth noise study mentioned above. This data is displayed as average values of RMS ground motion of each component

| STATION | $\frac{\text{MAX Z-P AMP}}{\text{RMS AMP}} (\Delta T=30-40)$ | $\frac{\text{MAX Z-P AMP}}{\text{RMS AMP}} (\Delta T=20-40)$ | $\frac{\text{MAX Z-P AMP}}{\text{RMS AMP}} (\Delta T=17-25)$ | NUMBER OF SAMPLES |
|---------|--|--|--|-------------------|
| CTA | 5.06 ± 1.49 | 6.72 ± 2.78 | 5.36 ± 2.58 | 16 |
| CHG | 4.63 ± 1.51 | 6.09 ± 2.42 | 5.01 ± 1.57 | 21 |
| FBK | 3.47 ± 1.02 | 4.54 ± 1.73 | 4.10 ± 1.49 | 20 |
| KON | 3.40 ± 1.00 | 4.01 ± 1.25 | 3.75 ± 1.02 | 43 |
| OGD | 4.04 ± 1.31 | 5.31 ± 2.64 | 4.76 ± 2.03 | 13 |
| KIP | 3.38 ± 0.79 | 4.05 ± 1.29 | 3.60 ± 1.08 | 26 |
| ALQ | 3.57 ± 0.95 | 4.37 ± 1.13 | 4.08 ± 1.38 | 22 |
| ZLP | 4.03 ± 1.64 | 5.93 ± 3.00 | 5.10 ± 2.31 | 9 |
| AVERAGE | 3.82 ± 1.27 | 4.84 ± 2.08 | 4.27 ± 1.65 | 170 |

TABLE III-1

ZERO TO PEAK AMPLITUDE VERSUS RMS AMPLITUDE FOR VLPE STATIONS

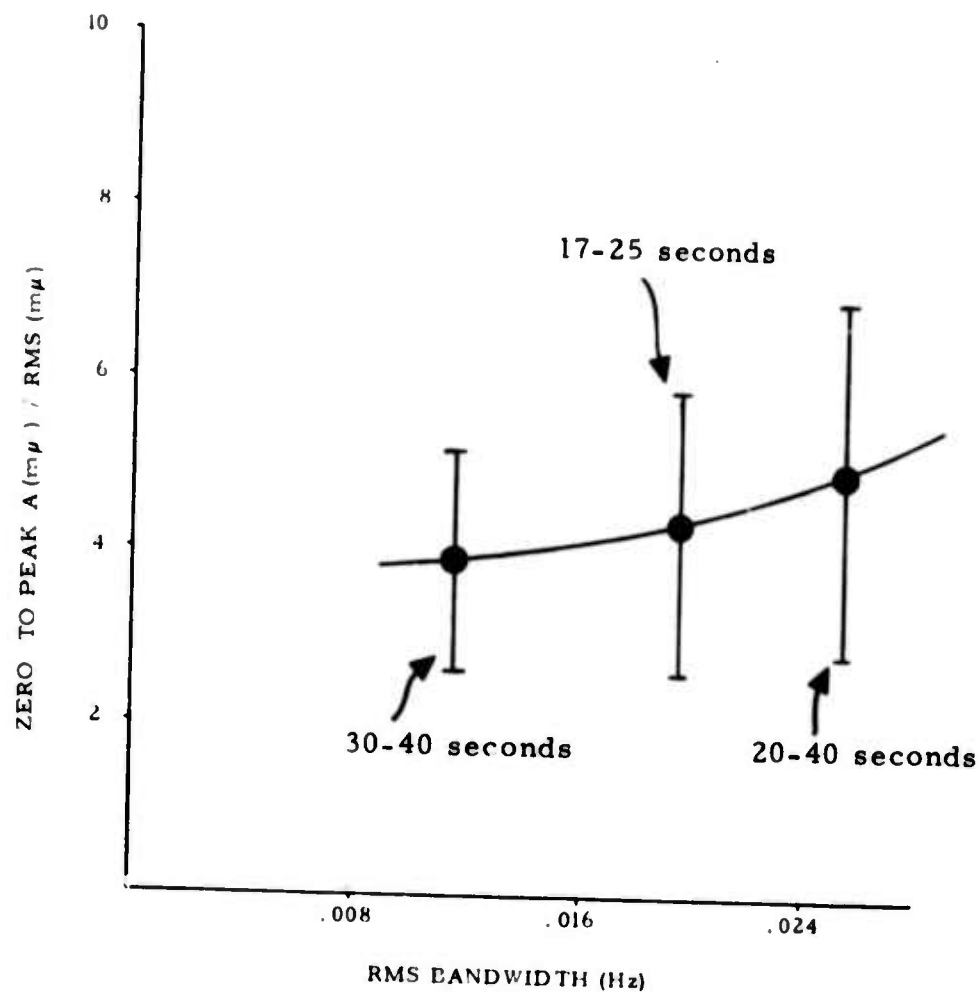


FIGURE III-4
 MAXIMUM ZERO TO PEAK TRACE AMPLITUDE/RMS AMPLITUDE
 AS A FUNCTION OF BANDWIDTH

TABLE III-2
VERY LONG PERIOD EXPERIMENT (VLPE) STATIONS AND LOCATIONS

| Station | Designator | Latitude | Longitude | Number of Samples |
|-------------------------|------------|----------|-----------|-------------------|
| Eilat, Israel | EIL | 29.55N | 34.95E | 18 |
| Albuquerque, New Mexico | ALQ | 34.94N | 106.46W | 66 |
| La Paz, Bolivia | ZLP | 16.50S | 68.13W | 38 |
| Matsushiro, Japan | MAT | 36.54N | 138.21E | 11 |

versus frequency. Intercomponent correlation of each component for each station was also calculated.

2. Vertical and Horizontal Noise Spectra

Mean RMS ground motion amplitudes for simultaneous vertical and horizontal noise are shown in the left half of Figures III-5 through III-8. The symbols indicate the average of RMS values observed at each location. The means and standard deviations for the RMS calculations are also given in Appendix III-A.

Generally the horizontal component displays similar characteristics to those seen in the vertical noise field. The lowest ground noise levels are in the 25-40 second range. A microseismic peak is clearly evident in all stations (except EIL) at the approximately 17 second period. The horizontal noise is more variable and greater in magnitude than the vertical noise at periods greater than 30-35 seconds. Stations FIL and MAT deviate slightly from the normal spectra of other stations. This could reflect either a recording difficulty at the times these data were recorded or a lack of data.

Conversion from RMS amplitude to log amplitude plots of the noise data was justified by Alsup and Becker (1973b) because the distribution of the logarithmic data closely approximates a normal distribution. Log amplitude plots are displayed on the right half of Figures III-5 through III-8. The means and standard deviations of these data are also given in Appendix III-B. Included on the log amplitude plots are flags of the standard deviations of the mean values. Variability of the log amplitude values is relatively constant across the bandwidth.

3. Intercomponent Noise Correlation

Interchannel cross correlations as a function of period are shown in Figures III-9 and III-10. The cross correlations between each channel pair (Z-vertical channel, N-north south channel, and E-east west

EILAT, ISRAEL

AVERAGED ONE-HOUR SEISMIC
 NOISE (SIMULTANEOUS THREE-
 COMPONENTS, 18 HOURS TOTAL)

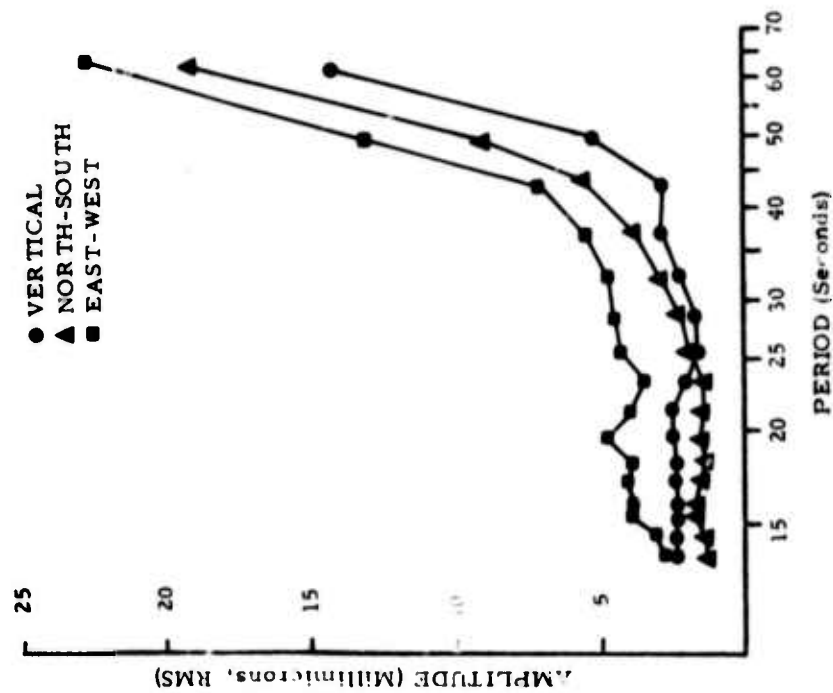
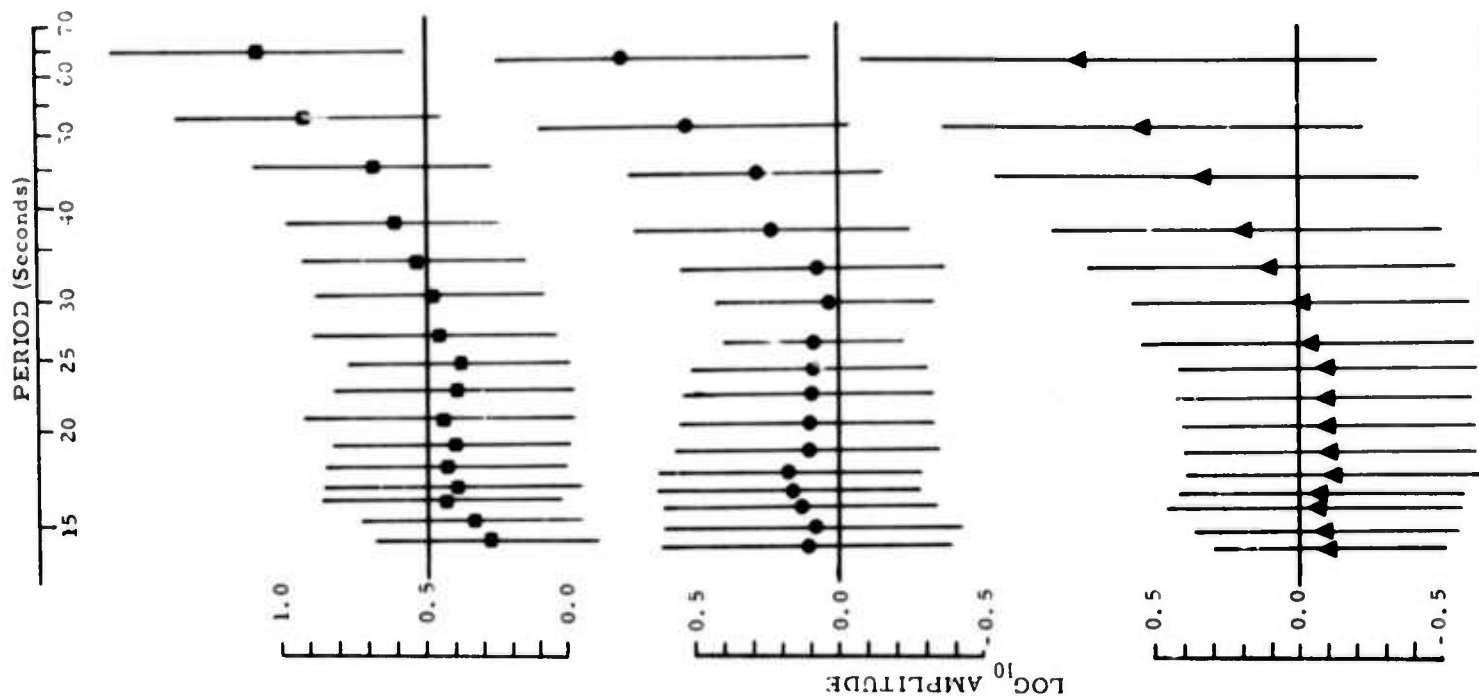


FIGURE III-5
 SUMMARY OF THREE-COMPONENT
 NOISE AT EILAT, ISRAEL



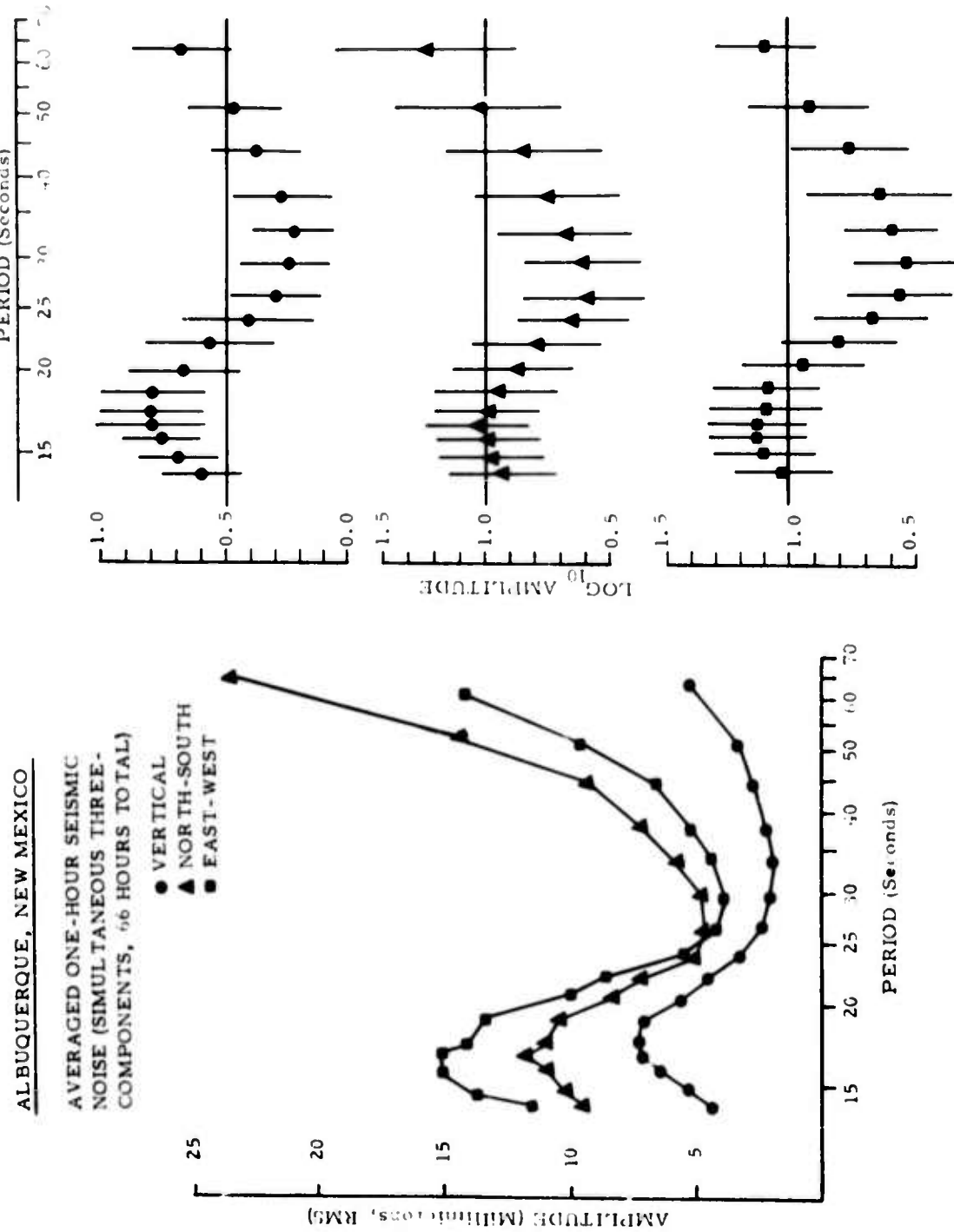


FIGURE III-6
SUMMARY OF THREE-COMPONENT NOISE
AT ALBUQUERQUE, NEW MEXICO

LA PAZ, BOLIVIA

AVERAGED ONE HOUR SEISMIC
NOISE (SIMULTANEOUS THREE-
COMPONENTS, 38 HOURS TOTAL)

- VERTICAL
- ▲ NORTH-SOUTH
- EAST-WEST

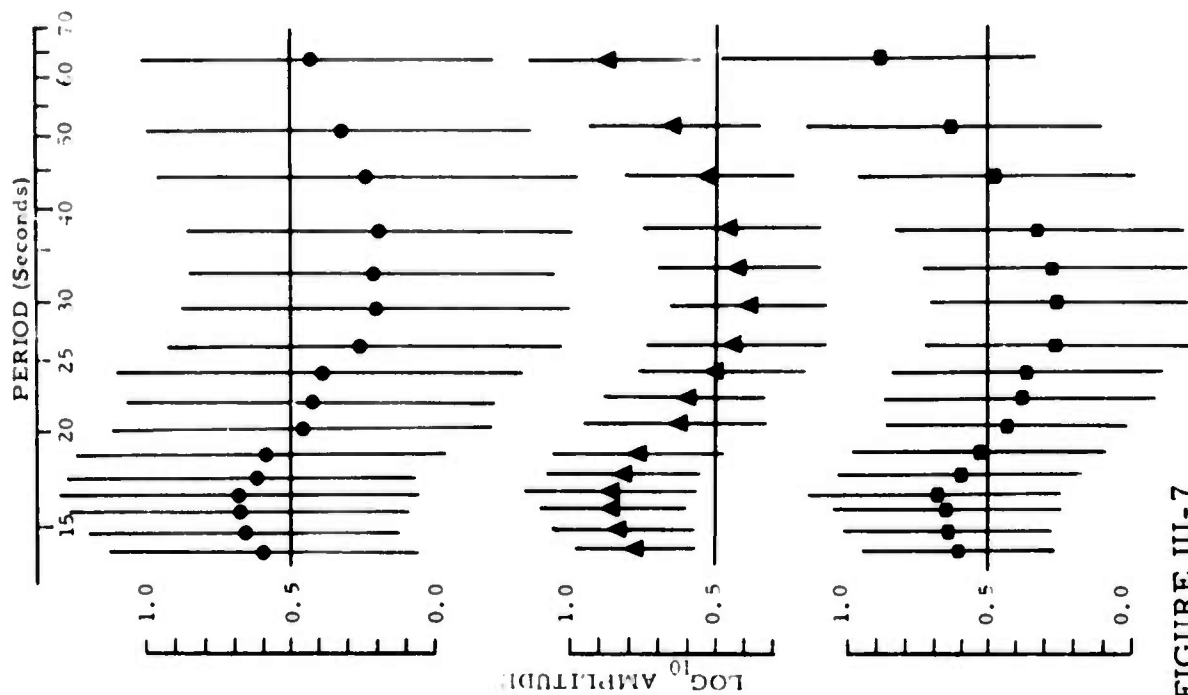
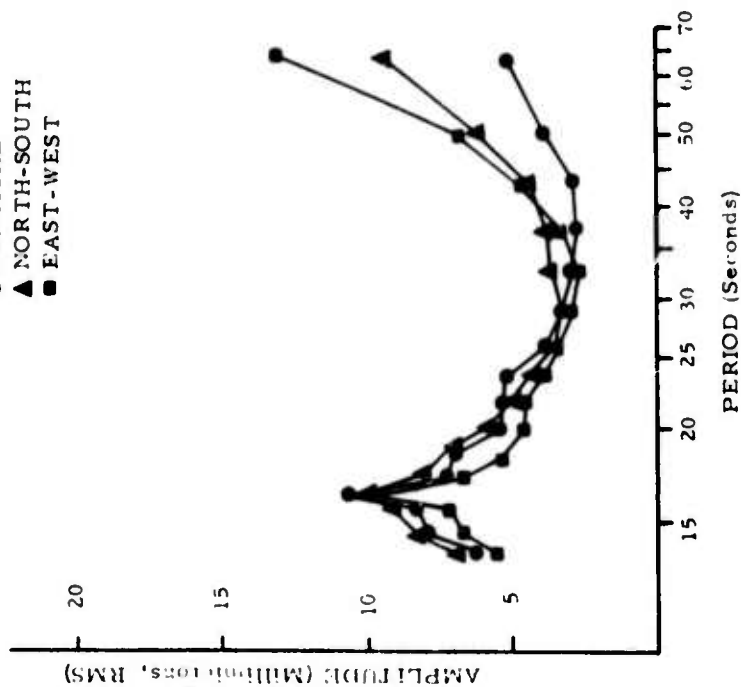


FIGURE III-7
SUMMARY OF THREE-COMPONENT NOISE
AT LA PAZ, BOLIVIA

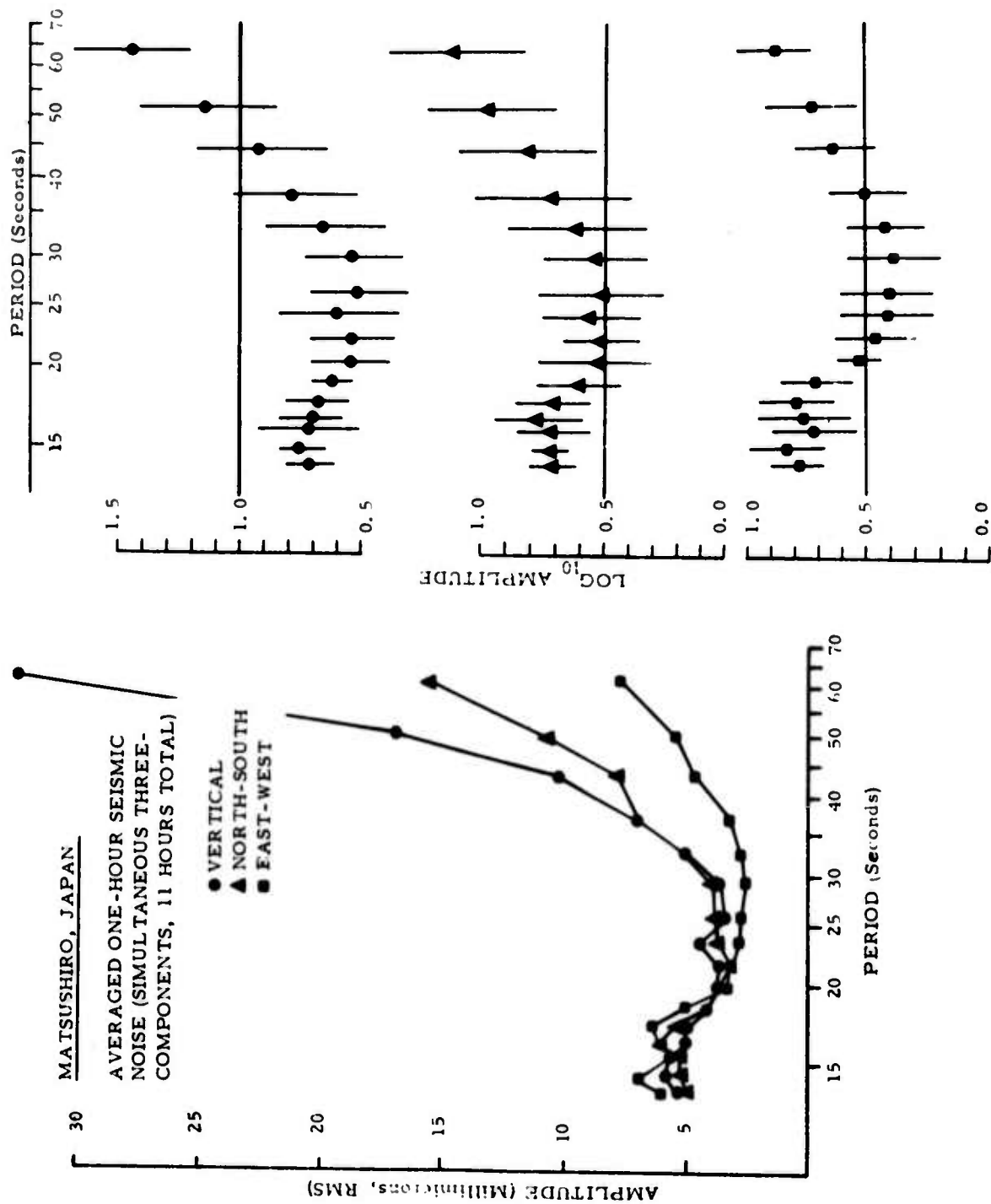


FIGURE III-8

SUMMARY OF THREE-COMPONENT NOISE AT MATSUSHIRO, JAPAN

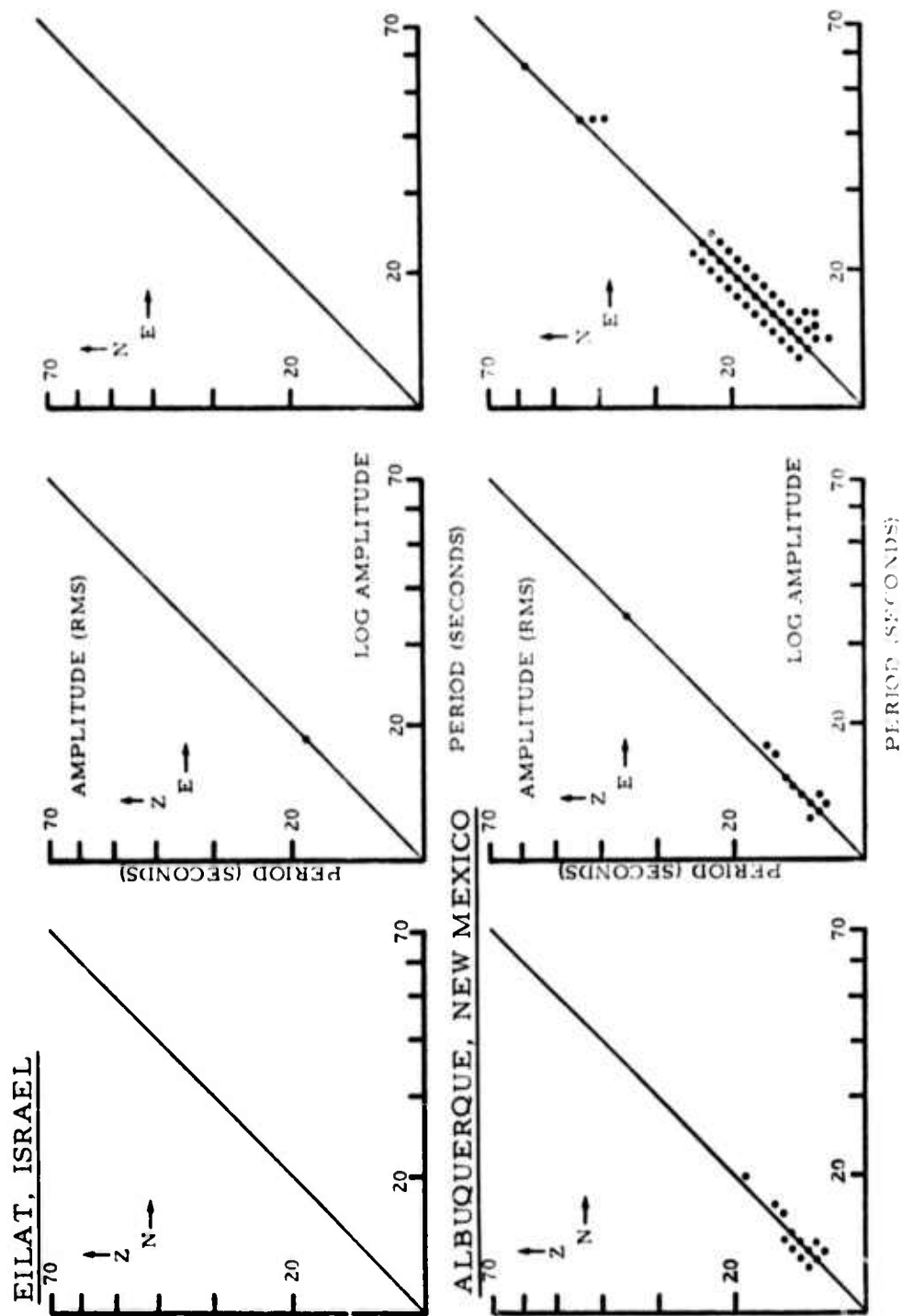


FIGURE III-9

INTERCHANNEL NOISE CROSS CORRELATION AT VLPE STATIONS. LINEAR COEFFICIENT OF CORRELATION: BLANK (LESS THAN .70) AND STIPPLED (GREATER THAN .70).

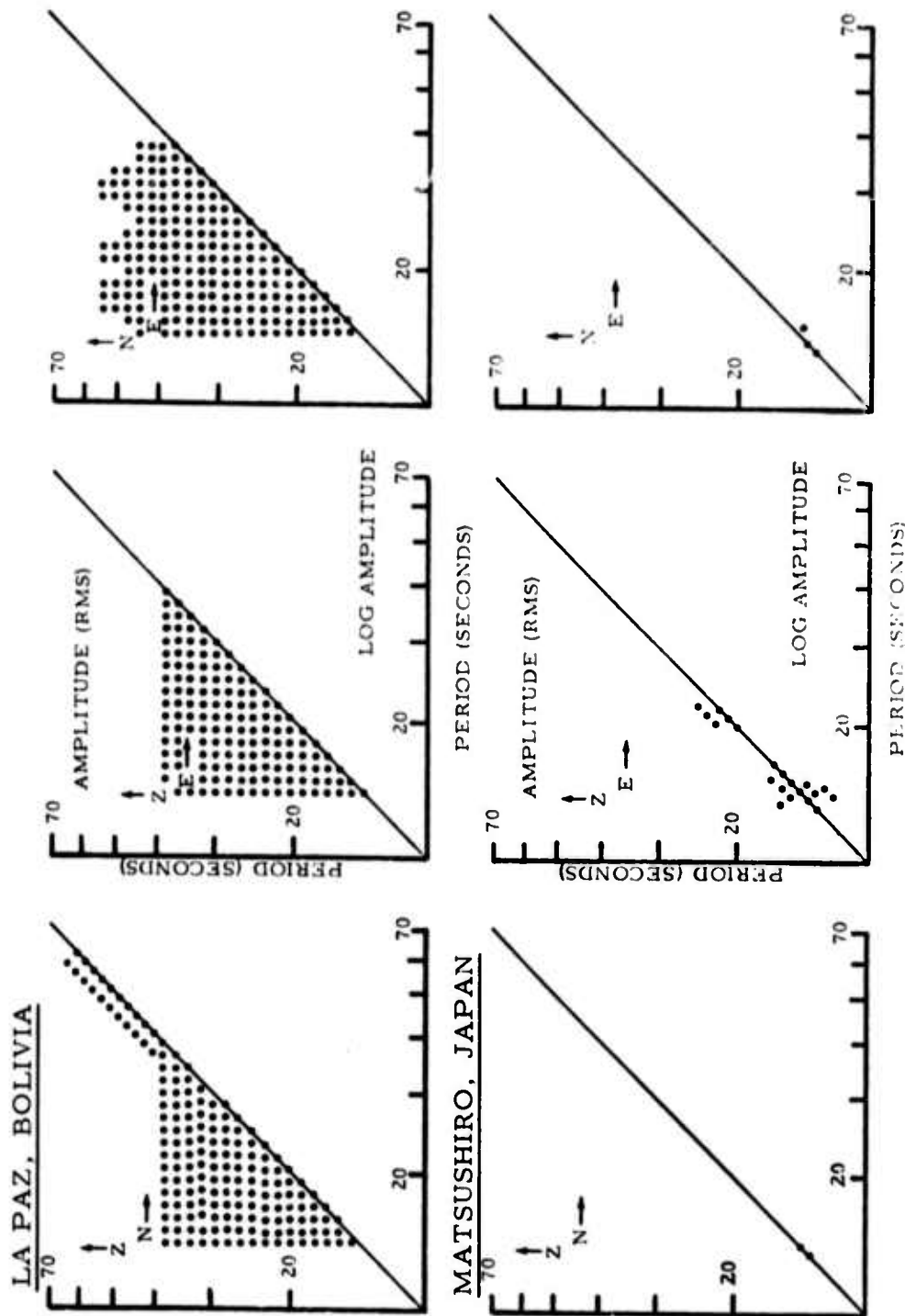


FIGURE III-10

INTERCHANNEL NOISE CROSS CORRELATION AT VLPE STATIONS. LINEAR COEFFICIENT OF CORRELATION: BLANK (LESS THAN .70) AND STIPPLED (GREATER THAN .70).

channel) are shown. The RMS amplitude correlations are displayed in the upper left half of each plot and the log amplitude correlations in the lower right half. The basic correlation data also are given in Appendix III-C and III-D. Weak to moderate correlation in the period band of 14.3 to 21.3 seconds is seen between all channels at ALQ and MAT. This might be related to the microseismic peak which occurs at the 17-20 second period. In general correlation is weak except at location ZLP. Considering the standard deviations of the RMS amplitudes of this location the high correlations must have resulted from poor data. The cross correlation study points out that each channel must be treated separately in any attempt to improve detection capability.

E. SUMMARY

Data from vertical and simultaneous three component noise samples from VLPE sites show the following:

- The presence of a "stable noise minimum" is evident in the approximate period range of 22-35 seconds.
- At most VLPE sites a microseismic peak is present in the 17-20 second period range.
- There is a levelling off of the vertical and horizontal noise field at periods below the microseismic peak while at periods above 30-35 seconds great variability in the horizontal noise field is present relative to the vertical noise field.
- Seasonal variations in the vertical noise fields are suggested by the slowly changing long term nature of the vertical noise fields.
- Intercomponent frequency dependent cross correlation of the RMS amplitudes is rarely present but when present, it occurs

only at the same periods on both correlated components.

Despite this occasional correlation, we interpret this to mean that in general noise on one component is independent of noise on the other two.

A larger and more continuous data base is needed before conclusive statements can be made about the seasonal variations in the noise field. Stations EIL, ZLP, and MAT should be studied in greater detail.

SECTION IV

VLPE DETECTION CAPABILITY

A. INTRODUCTION

In this section, we present the results of various processing and analysis techniques as they apply to the detection capabilities of the VLPE.

The results of estimating detection capabilities utilizing the maximum likelihood procedure is given in part B. Part C discusses the effects of the VLPE network on events classified as "mixed events" at single VLPE sites, and Part D gives the results of the application of Matched Filters (Chirp and Master waveform) and the Three Component Adaptive Processor to events located in Central Asia.

B. MAXIMUM LIKELIHOOD ESTIMATES OF DETECTION CAPABILITY

1. Discussion

We present the results of estimating the surface wave detection capabilities for eleven individual VLPE stations and three VLPE networks.

The three VLPE networks considered are as follows: Network 1, includes the January 1 through March 20, 1972 ensemble of events. Network 2, includes the June 1 through August 31, 1972 ensemble of events, and Network 3 includes the November 1 through December 31, 1972 ensemble of events. Stations and data for these networks were previously described in Section II-B.

The method of estimating detection capabilities utilized here is based on a maximum-likelihood procedure, which has been described in detail by Ringdal, 1974. Briefly this method assumes that the probability

of detecting an event of magnitude m may be described as a cumulative Gaussian probability integral.

$$(1) \quad P(\text{Detect } m) = (2\pi\sigma^2)^{-\frac{1}{2}} \int_{-\infty}^m e^{-\frac{(t-\mu)^2}{2\sigma^2}} dt$$

Given a set of decisions detection versus no detection for events of various magnitudes, the procedure then is to find the mean and standard deviation values (μ, σ) that maximizes the probability of the observed pattern of detections/no detections occurring. The reliability of the detection capability estimate is of course, limited by the quality and quantity of the observed data; a specific discussion of the assumptions and limitations to the method is given by Ringdal (1974).

The above model applies equally well to estimating detectability in terms of body-wave magnitudes and surface-wave magnitudes. In the VLPE case, it would be desirable to express detection thresholds in terms of M_s values. However, we do not have reliable M_s estimates for all events in our data base. To use the average M_s value for all VLPE stations that detected each event would not be correct, as is illustrated in Figure IV-1, where VLPE M_s values are plotted versus NORSAR and ALPA M_s averages. It is seen that the VLPE values are biased high for low magnitude events; this is because only one or two of the better stations detect, and consequently the VLPE M_s estimate is based upon stations with larger than average amplitudes.

On the other hand, we have not been able to compute ALPA and NORSAR M_s values for all events in the data base. Thus, it has not been possible to use these two large arrays as references for this report; however, we plan to do this in our future studies. At this point it should be noted that NORSAR and ALPA give consistent M_s values for all magnitudes, and although the scatter is fairly large, NORSAR appears to show slightly higher values. (Figure IV-2)

For this report, we have thus been confined to give VLPE detection threshold estimates in terms of body-wave magnitudes. In order to convert these values to estimates based on M_s , it is not correct to apply

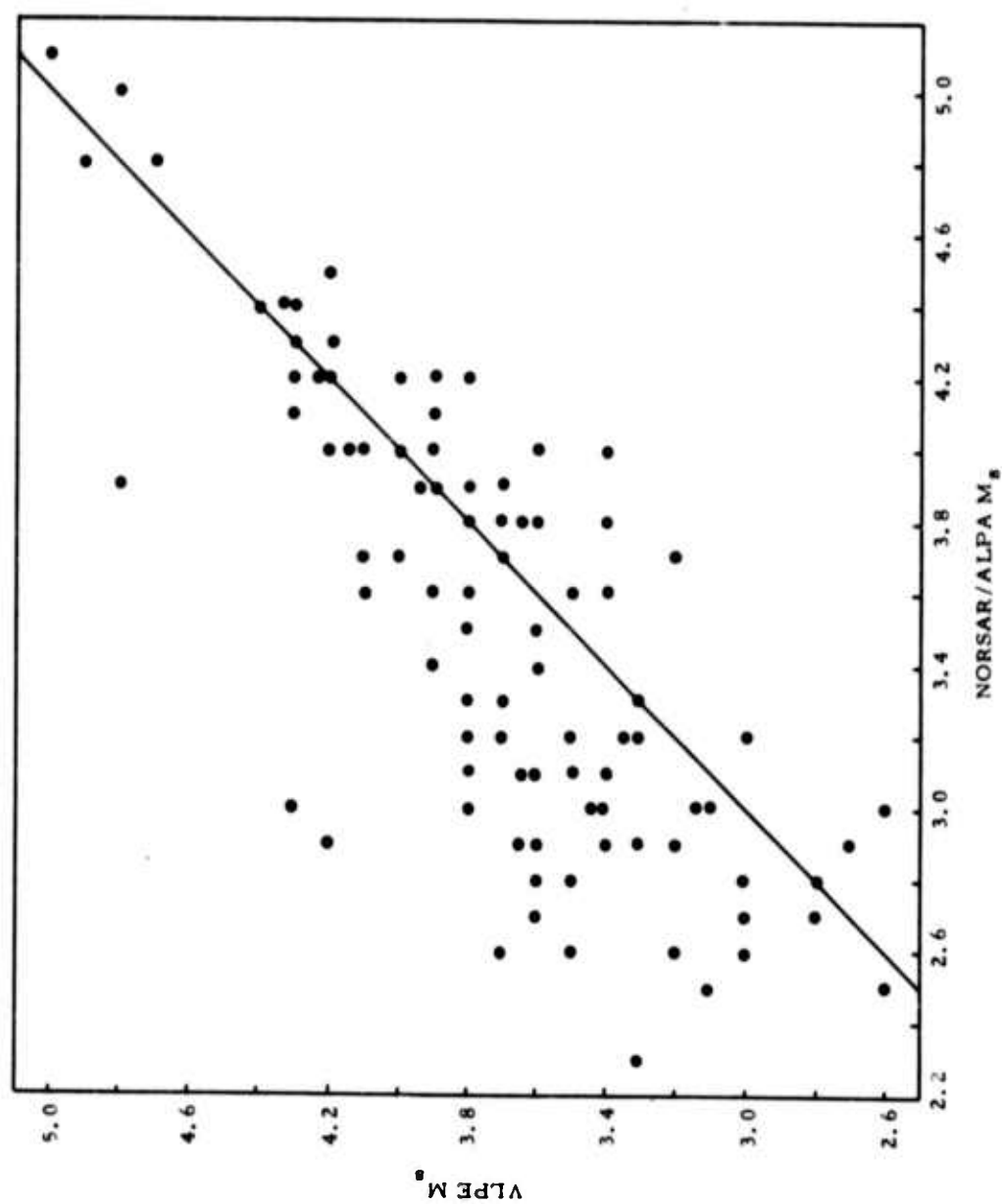


FIGURE IV-1

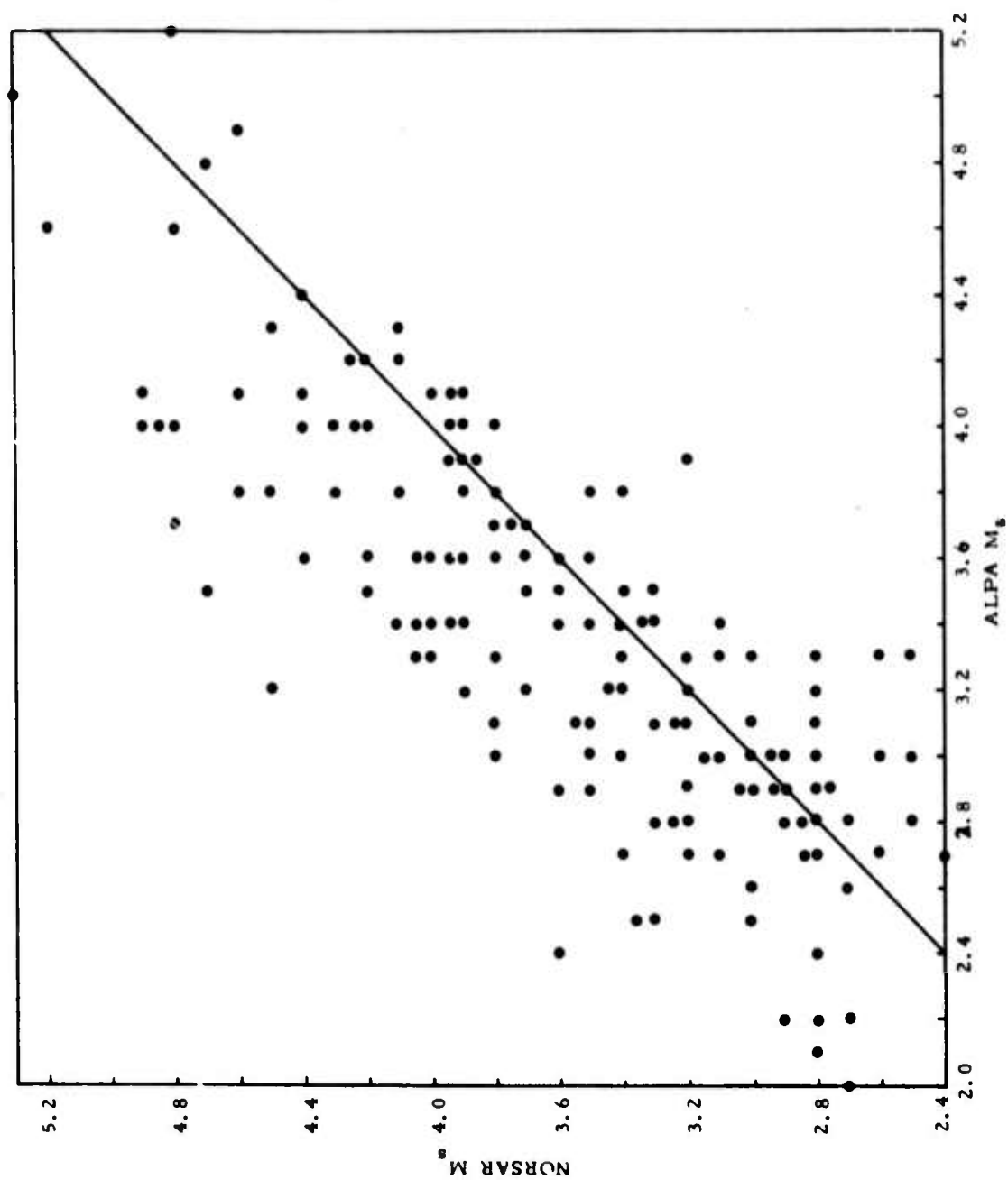


FIGURE IV-2

directly a linear M_s versus m_b relationship; we must also take into account the scattering in this correspondence. This has been pointed out by Harley and Heiting (Special Report No. 1, 1972), and independently by Lacoss (1971).

It is easily seen that the estimate of the 50 percent detection threshold μ is independent of this scattering effect, while the variance estimate σ^2 in (1) must be modified. Specifically, as pointed out by Lacoss (1971), if the variance in the M_s versus m_b relationship is σ_r^2 and the estimate of σ^2 based on m_b values is σ_m^2 , then the corresponding estimate σ_M^2 for a detection curve based on M_s values will be

$$(2) \quad \sigma_M^2 = \sigma_m^2 - \sigma_r^2$$

In practical situations one must be careful when applying (2) since σ_r and σ_m sometimes will be almost equal, and the resulting σ_M value may thus be dominated by possible errors in the other two estimates.

2. VLPE Single Station Detection Capability

Maximum likelihood detection threshold estimation based on body-wave magnitudes was performed for each of 11 single VLPE stations. For each station, all events were included for which a decision detection versus no detection could be made. We deleted events occurring during any period of malfunctioning hardware, and we did not consider presumed explosions or events where interfering signals were present.

The results are presented in Figures IV-3 through IV-13. Fifty-percent detection estimates are given with reasonably good confidence ($\sigma < 0.1 m_b$ units and more than 100 detection/no detection decisions) for the first nine stations, while for MAT and ZLP we obtained poor detection estimates due to the small number of detection/no detection decisions available.

The single station detectability estimates are summarized in

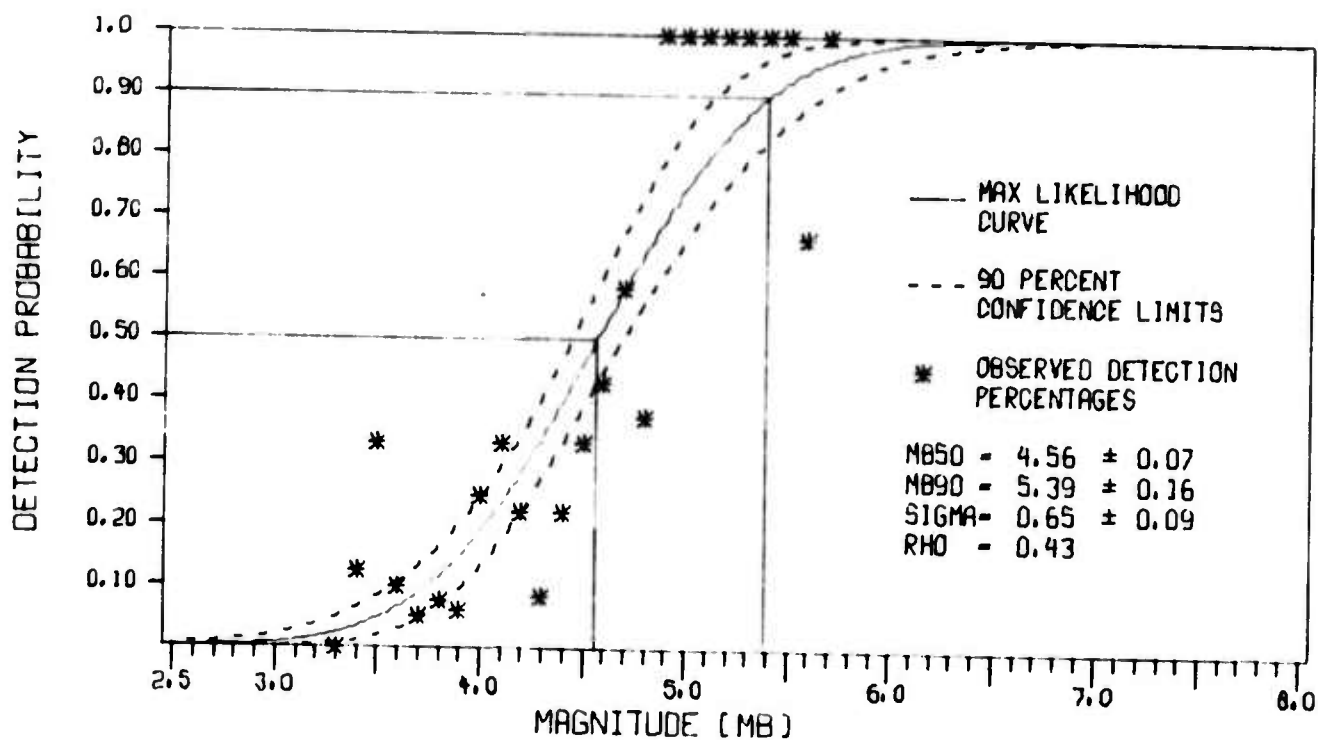
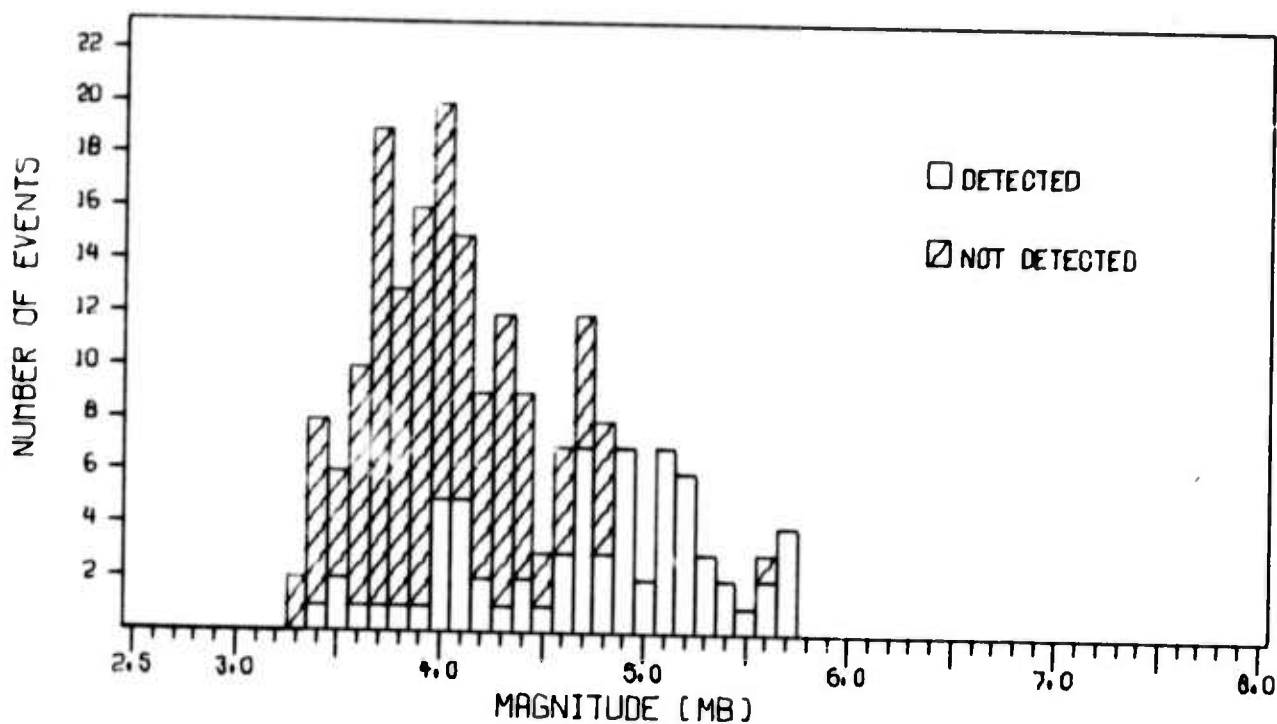


FIGURE IV-3
DETECTION STATISTICS FOR VLPE STATION 1 (CTA)
IV-6

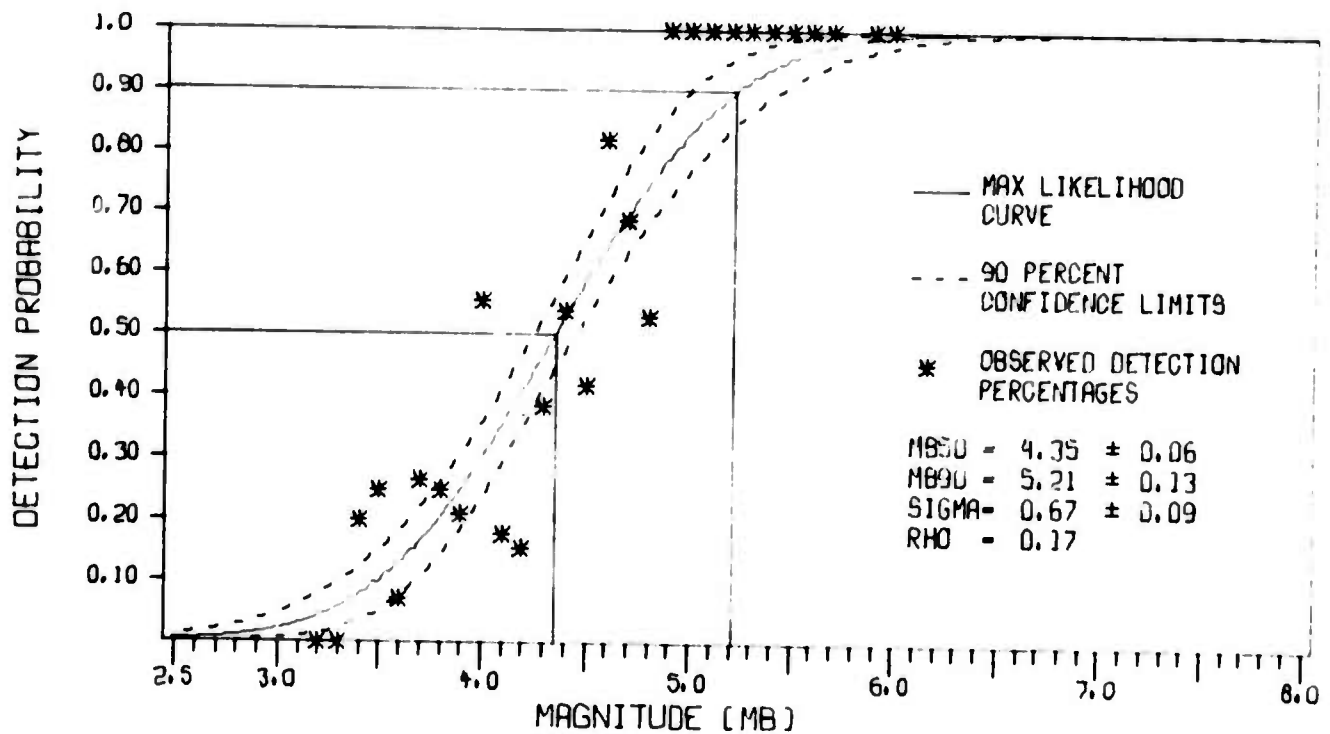
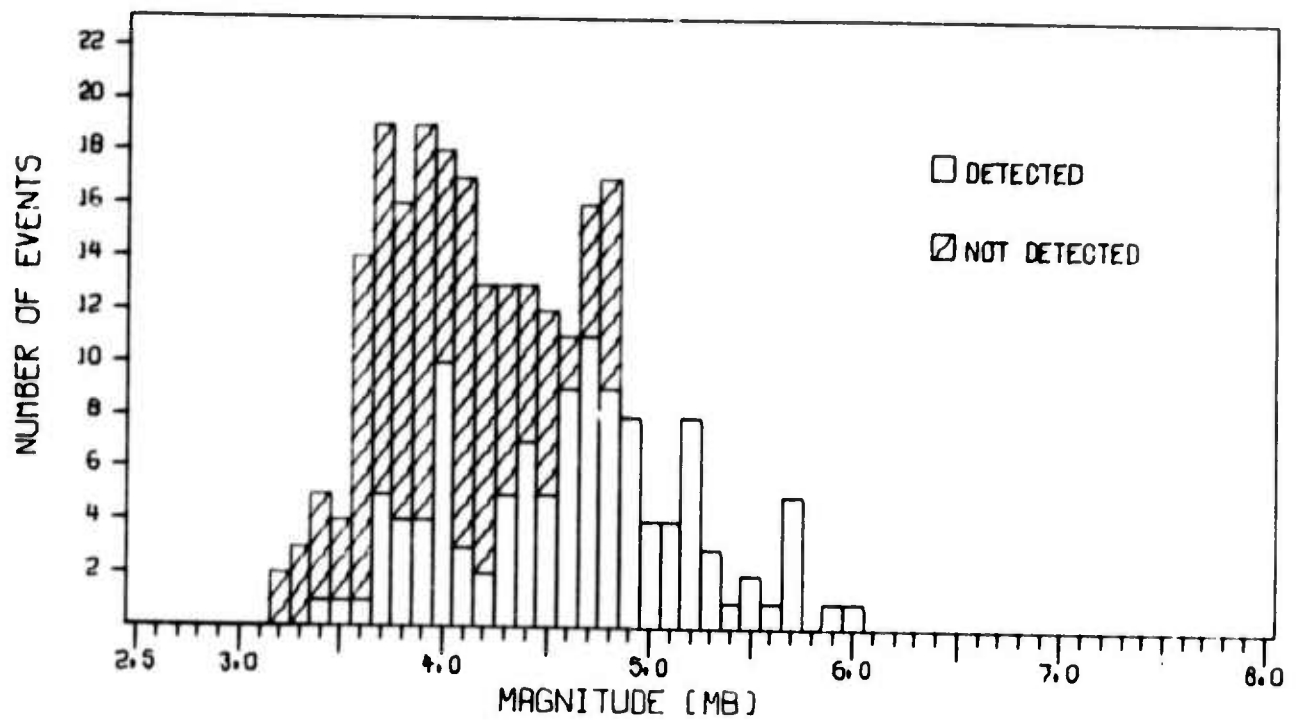


FIGURE IV-4
DETECTION STATISTICS FOR VLPE STATION 2 (CHG)

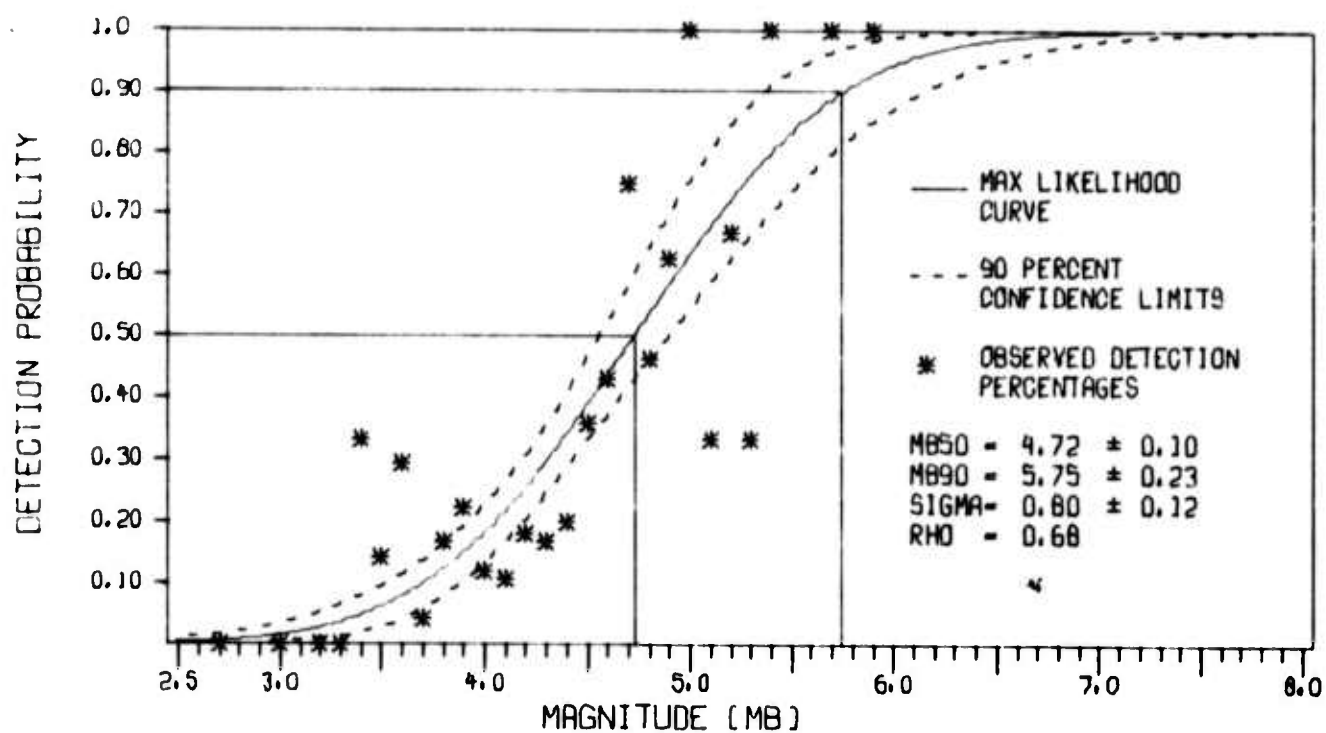
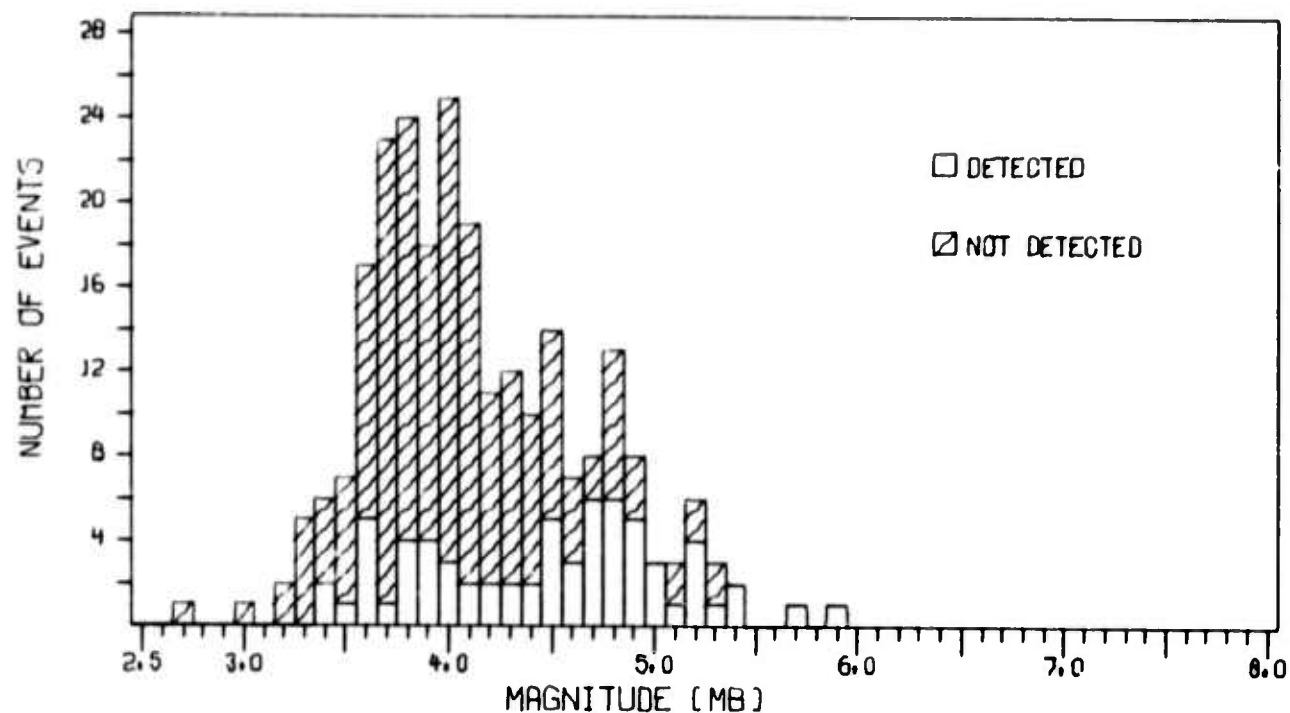


FIGURE IV-5
 DETECTION STATISTICS FOR VLPE STATION 3 (FBK)

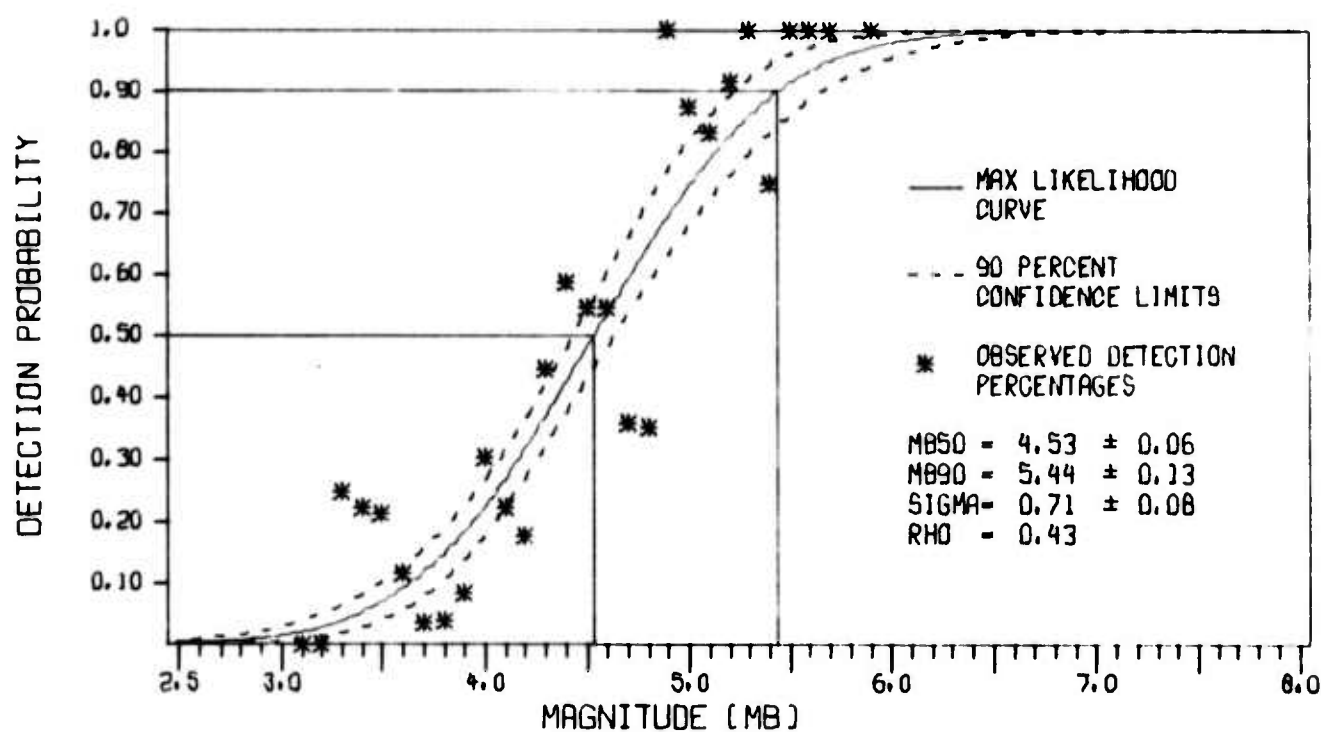
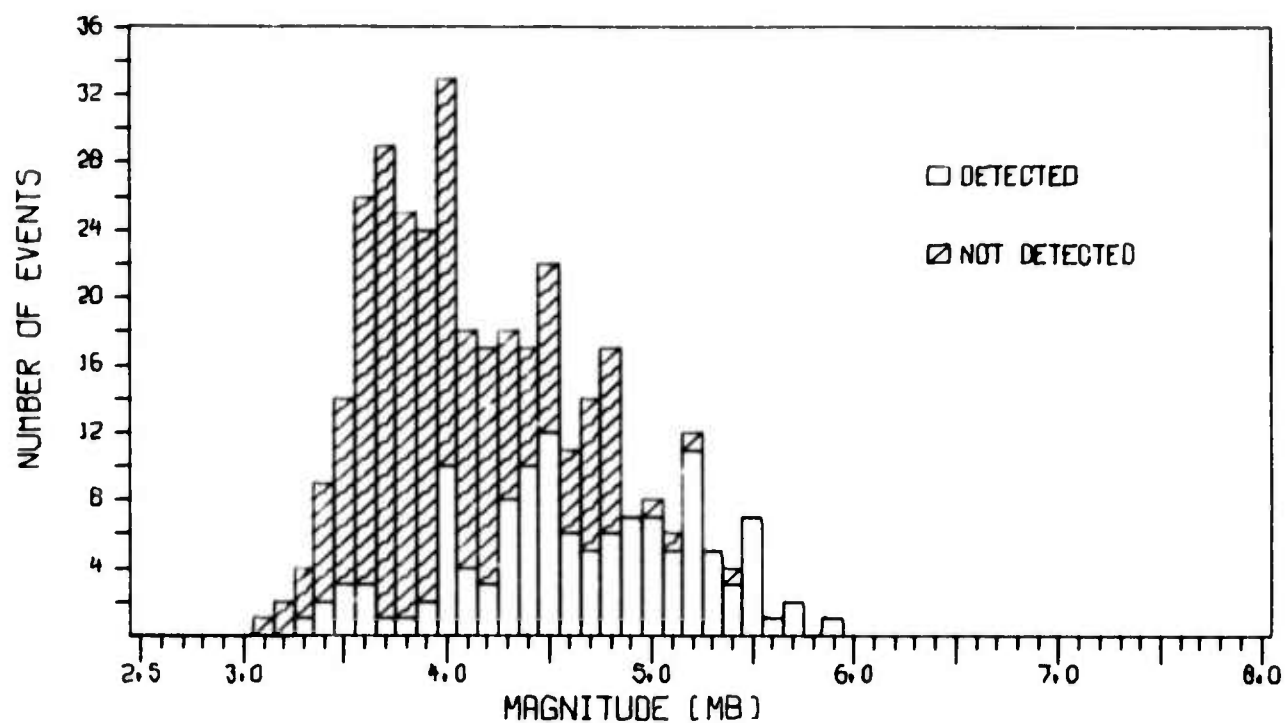


FIGURE IV-6
 DETECTION STATISTICS FOR VLPE STATION 4 (TLO)

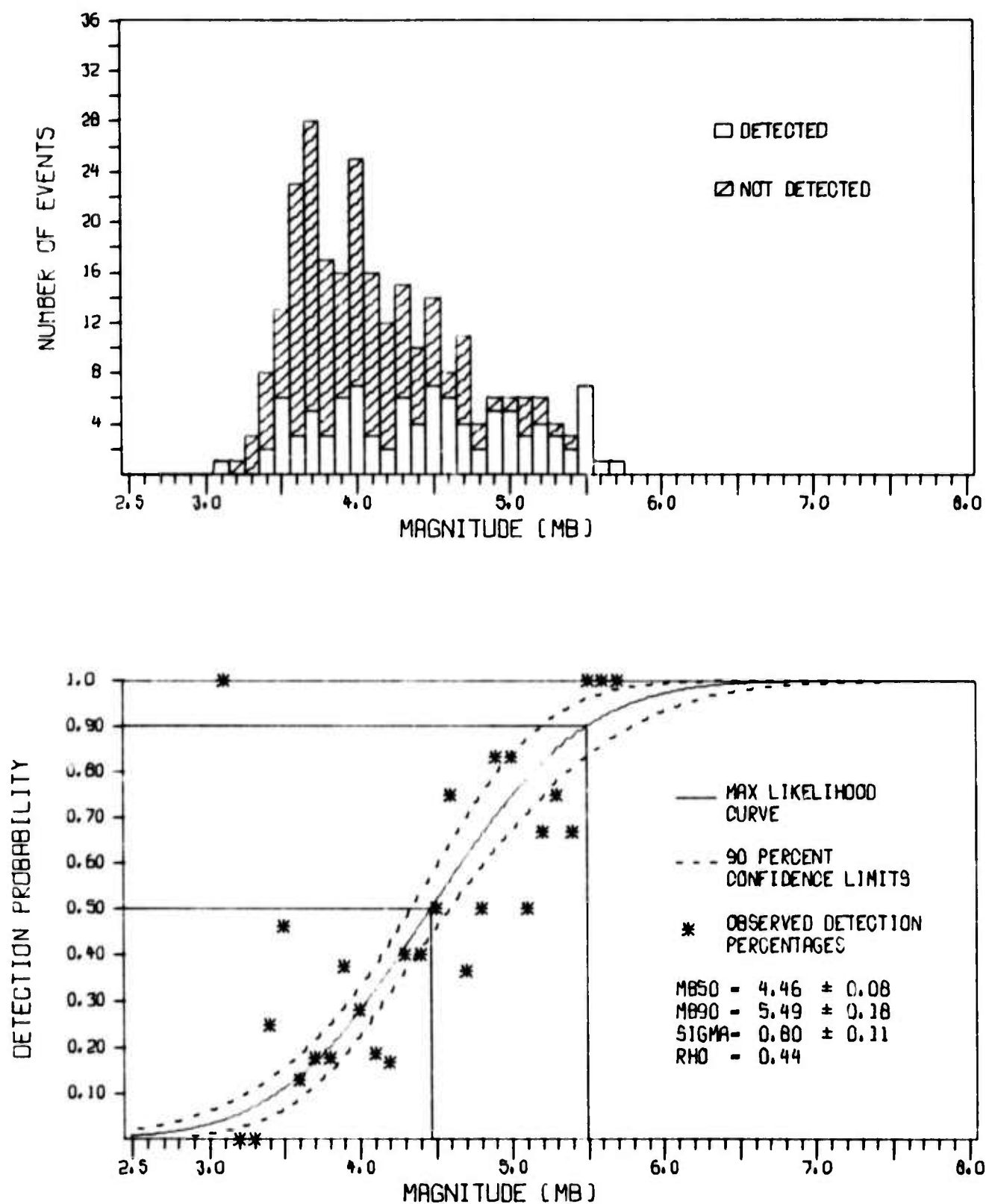


FIGURE IV-7
DETECTION STATISTICS FOR VLPE STATION 5 (EIL)

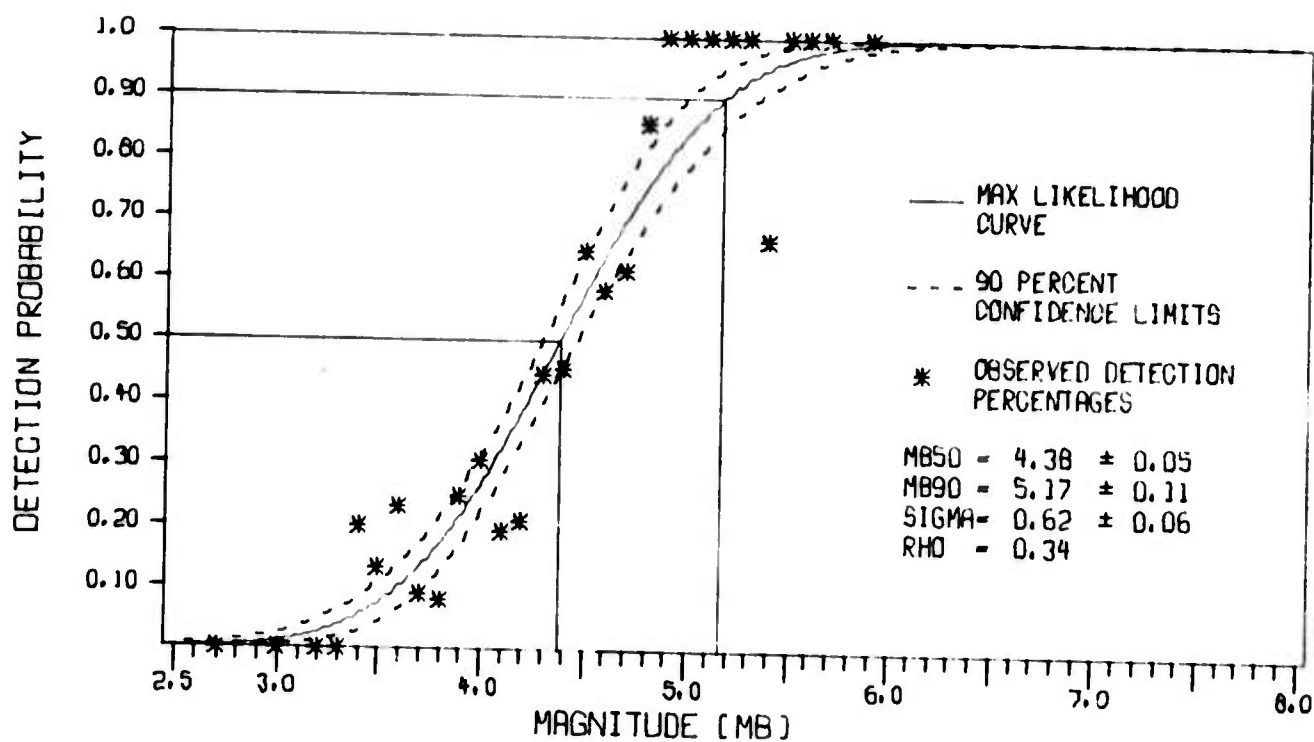
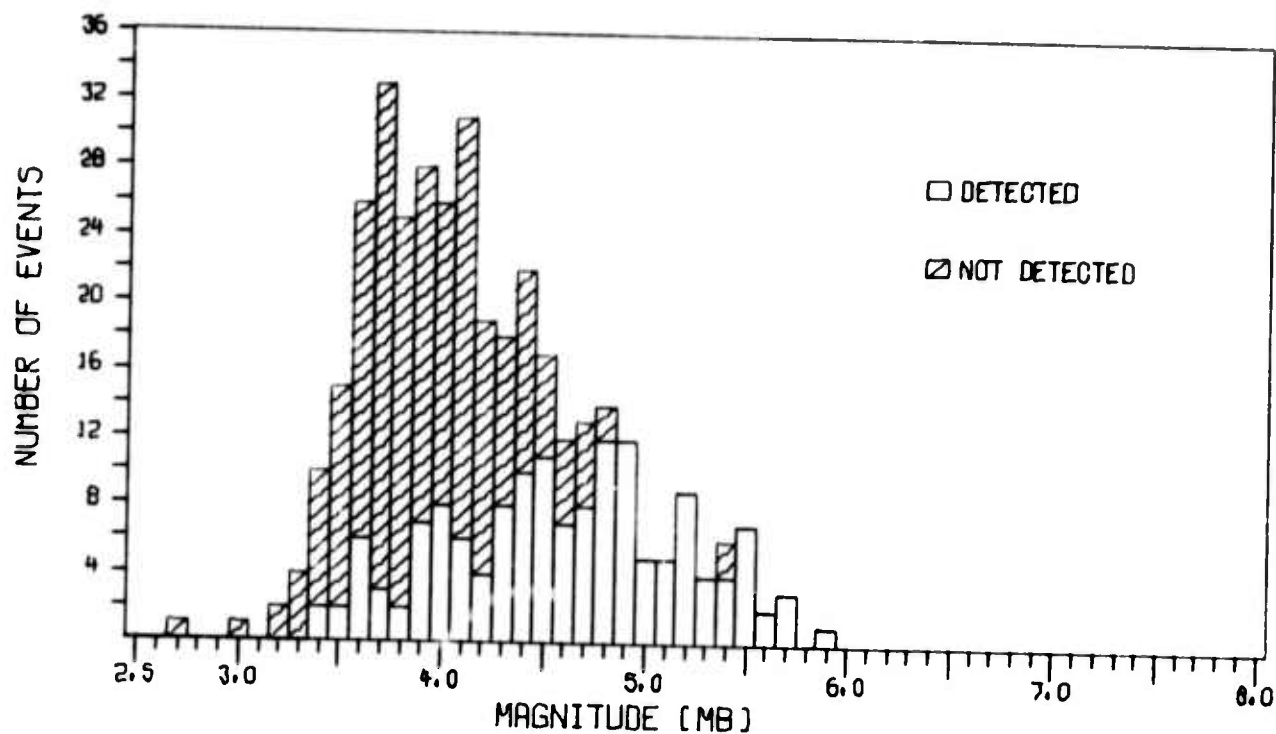


FIGURE IV-8
DETECTION STATISTICS FOR VLPE STATION 6 (KON)

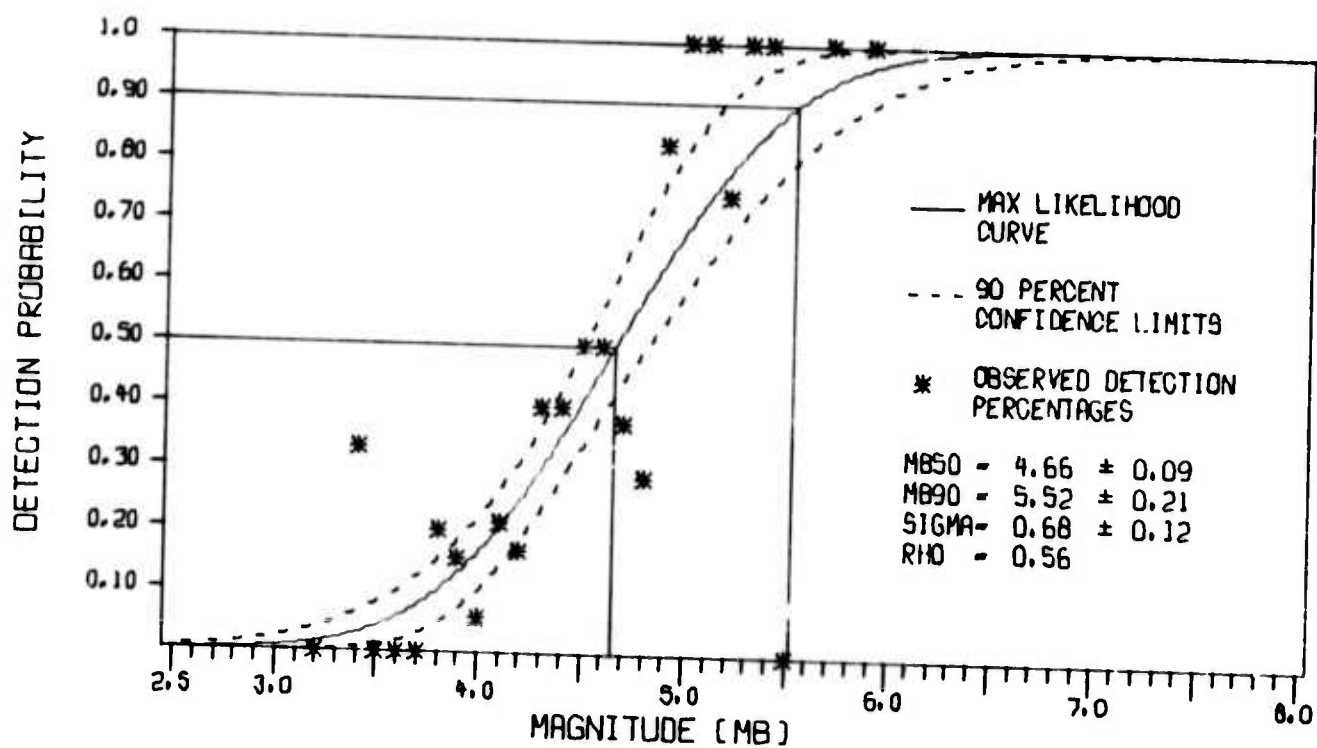
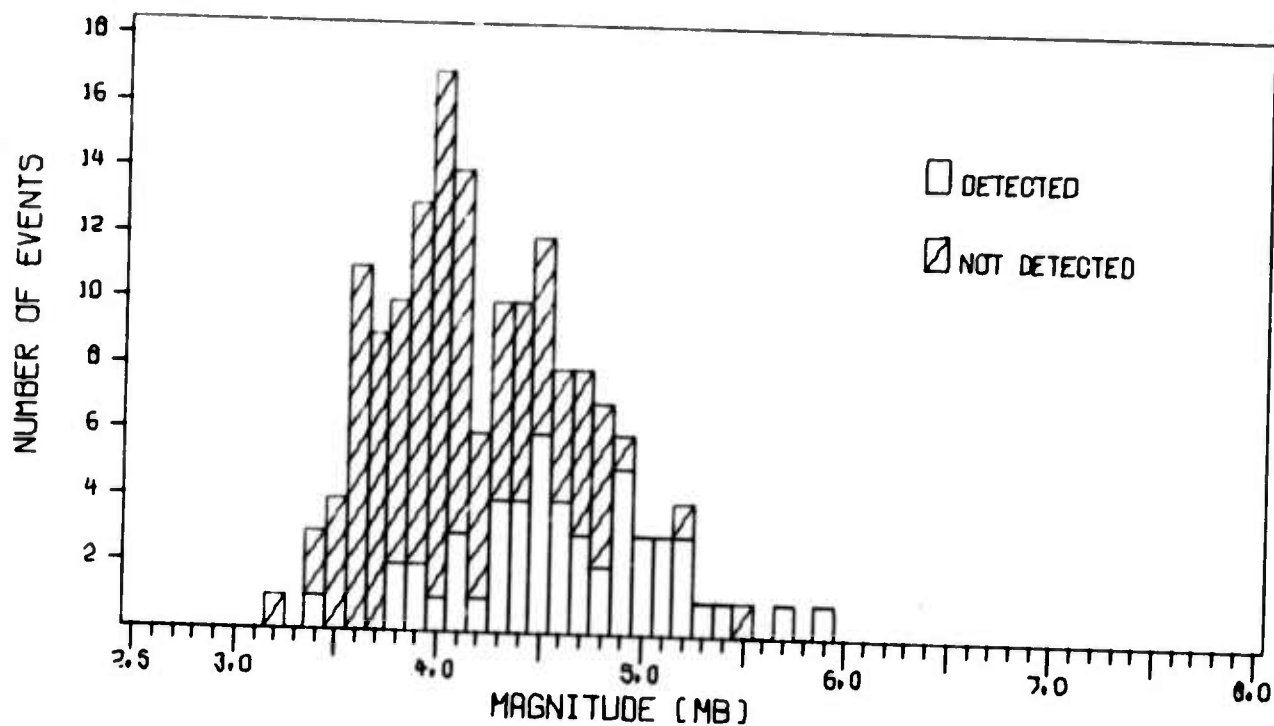


FIGURE IV-9
 DETECTION STATISTICS FOR VLPE STATION 7 (OGD)

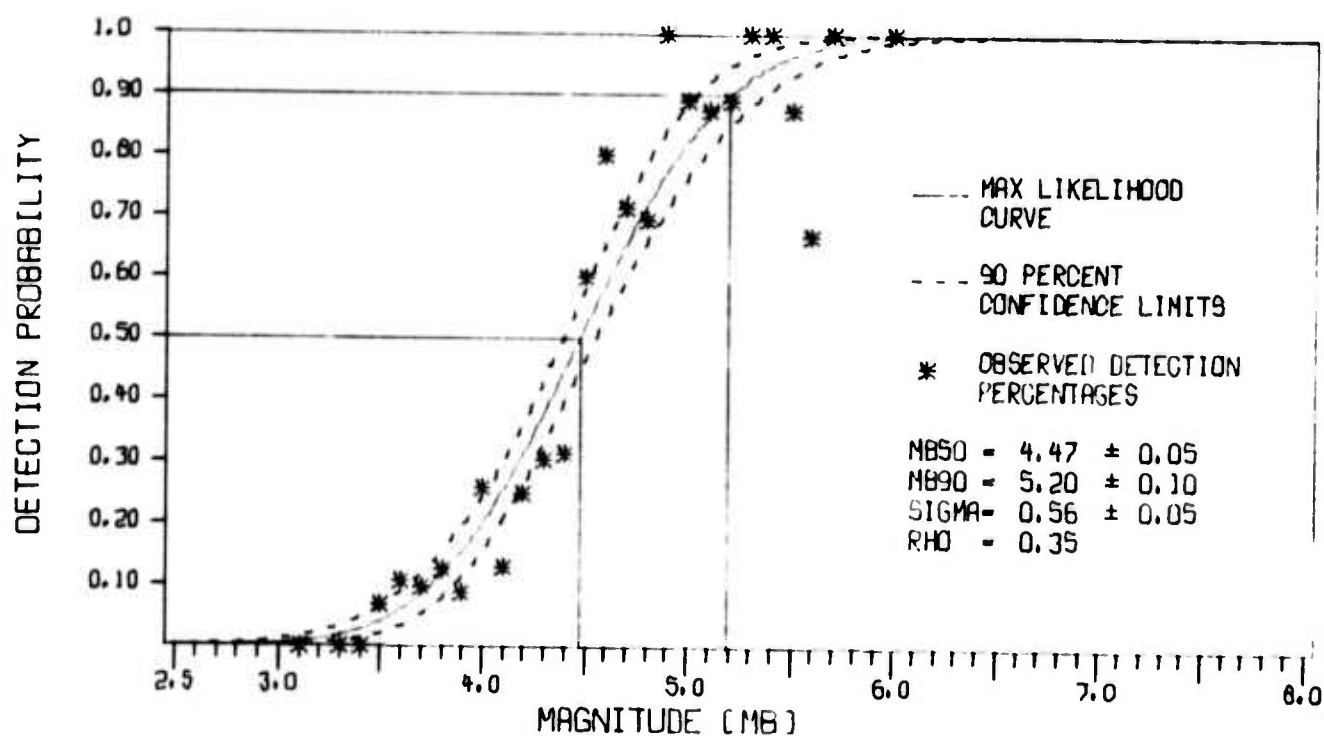
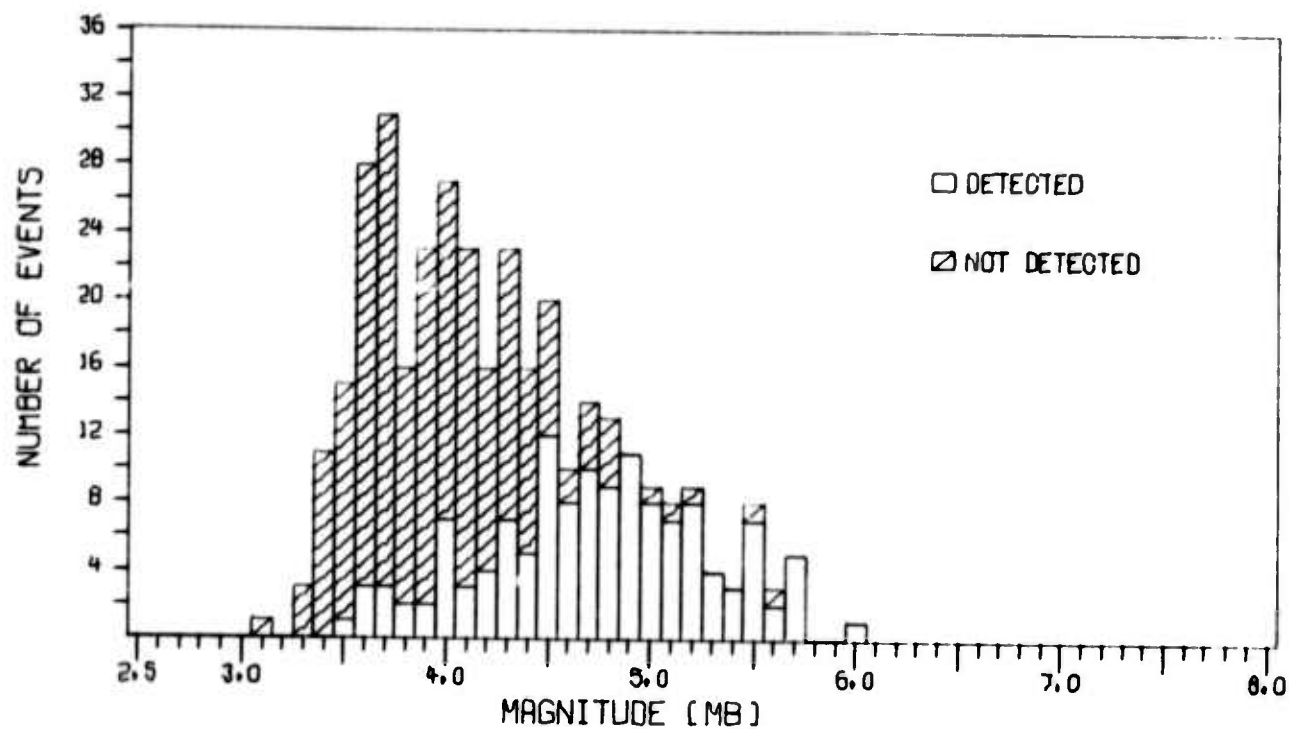


FIGURE IV-10
DETECTION STATISTICS FOR VLPE STATION 8 (KIP)
IV-13

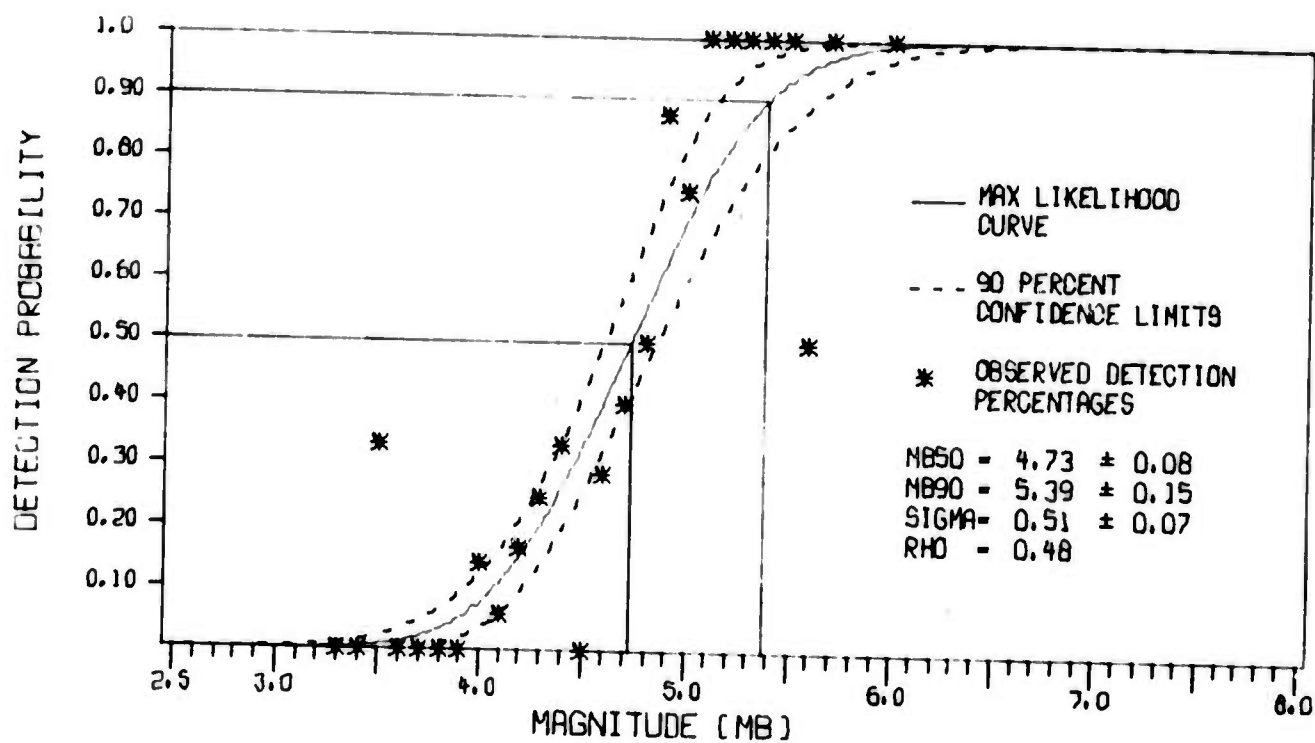
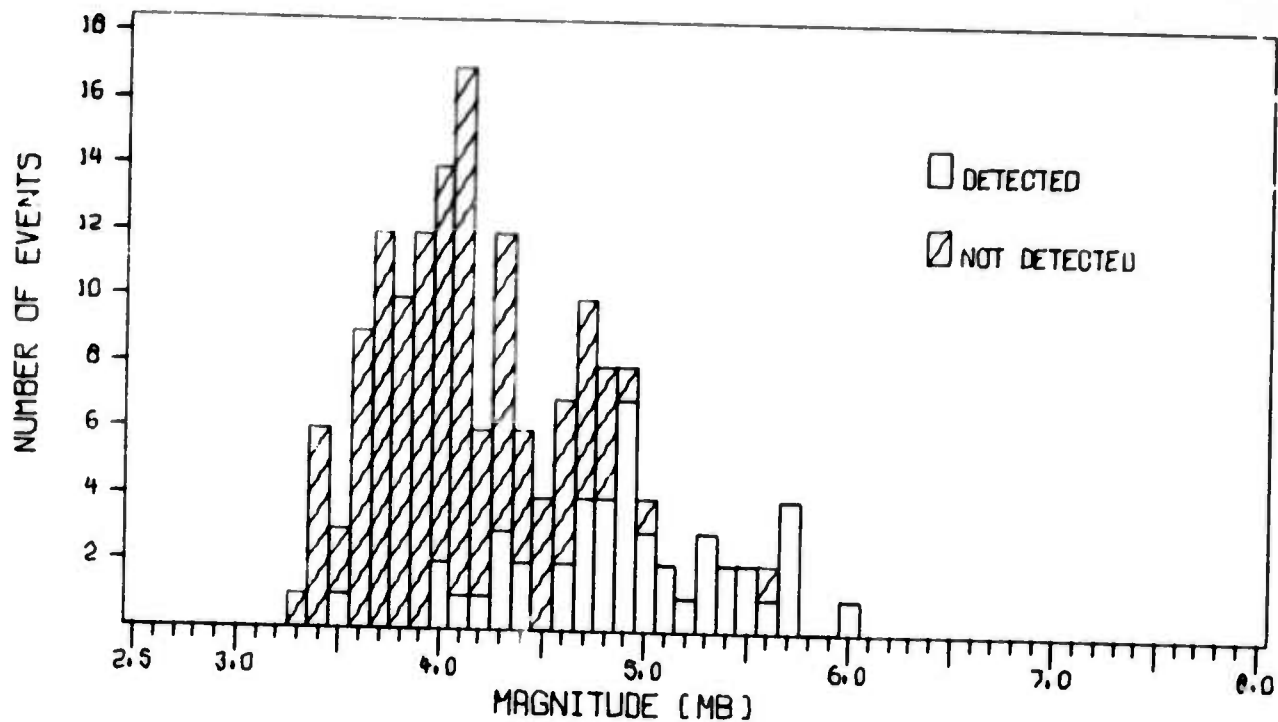


FIGURE IV-11
DETECTION STATISTICS FOR VLPE STATION 9 (ALQ)

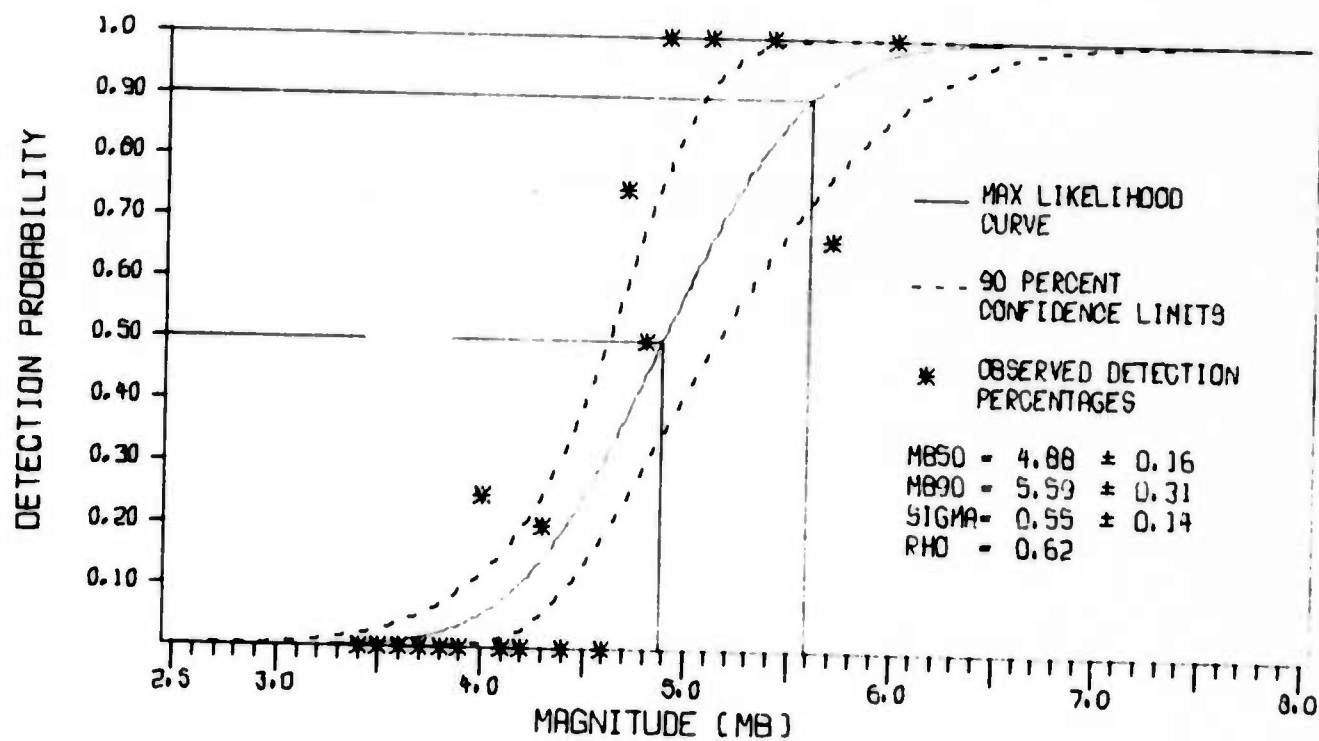
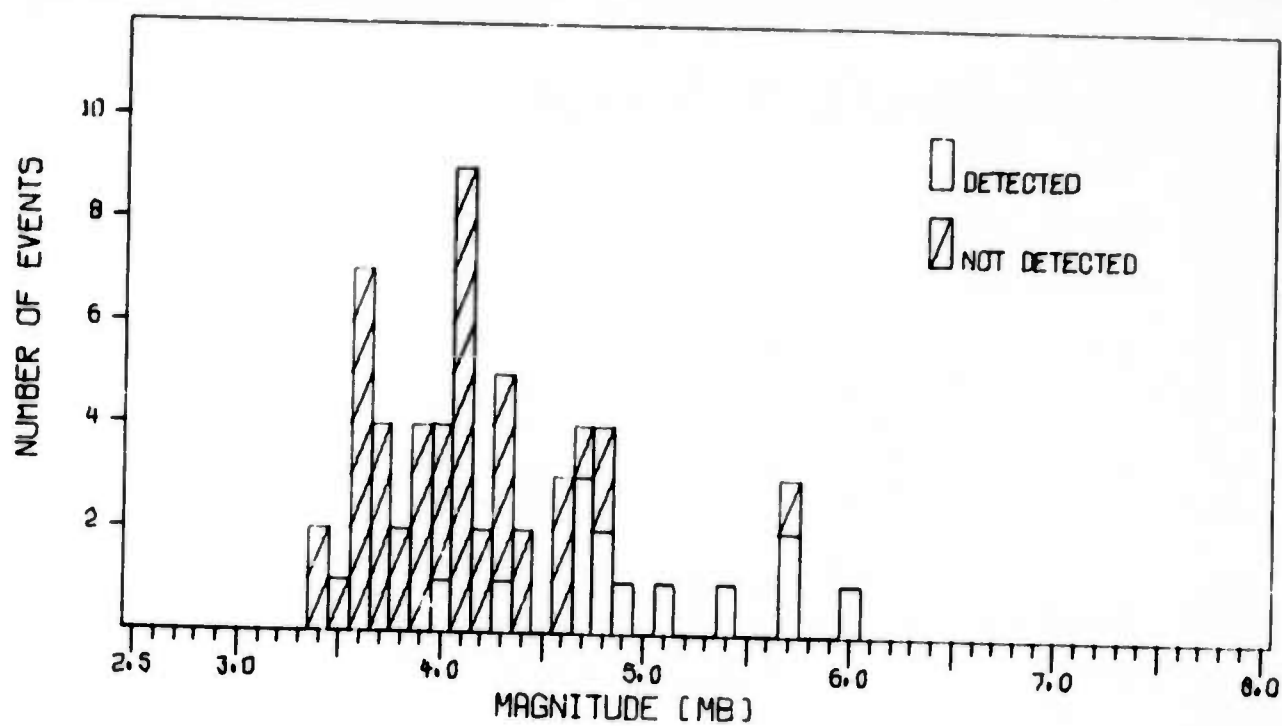


FIGURE IV-12
DETECTION STATISTICS FOR VLPE STATION 10 (ZLP)

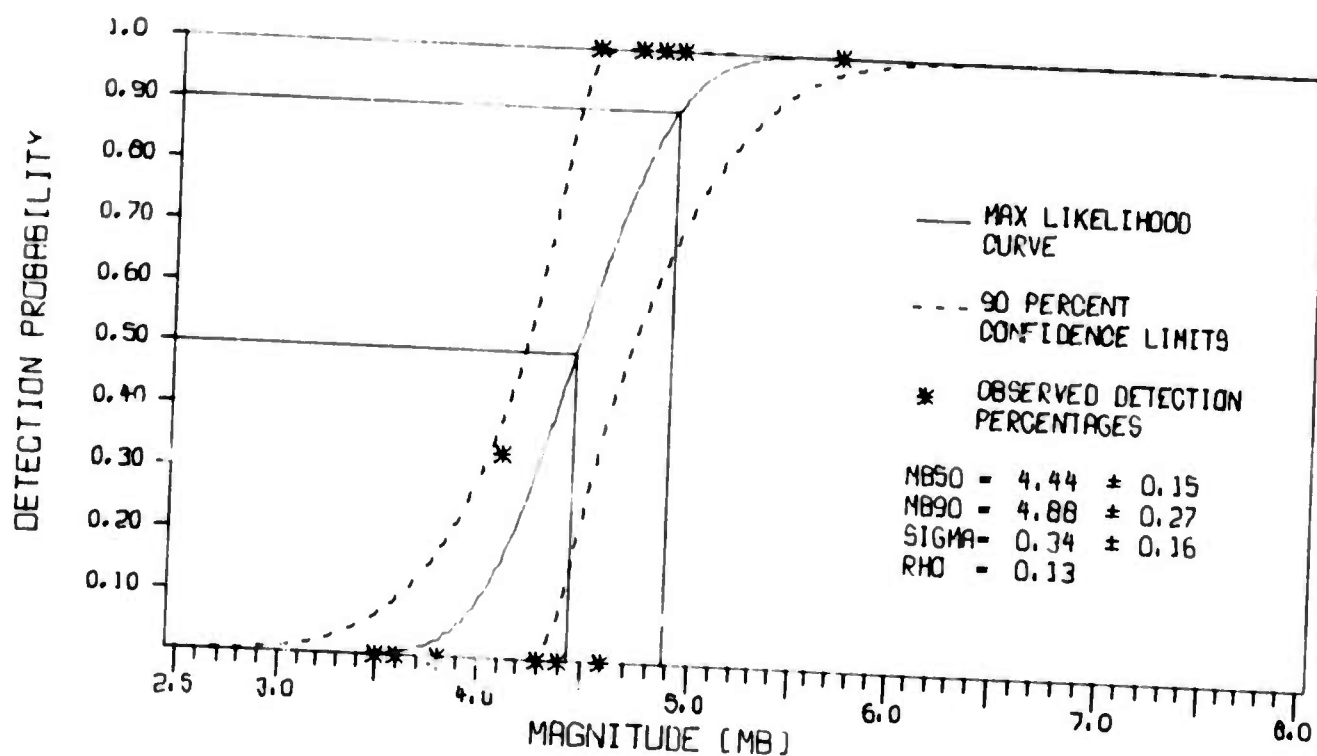
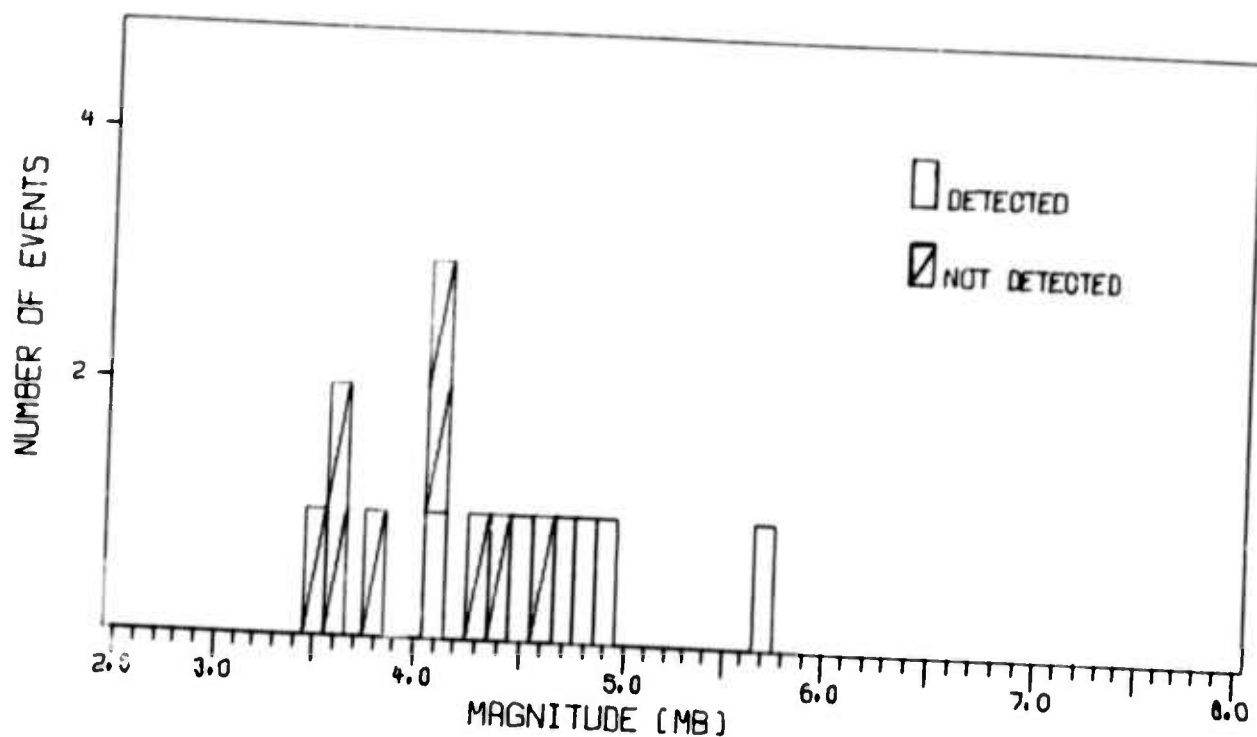


FIGURE IV-13
 DETECTION STATISTICS FOR VLPE STATION II (MAT)

Table IV-1. Separate estimates were computed for all events within 50 degrees epicentral distance as well as for events of greater distance than 50 degrees since the distribution of station-events versus distance shows two distinct groupings (Lambert and Becker, 1973). It is seen that the difference in 50 percent detectability for these two subsets ranges from 0.2 to 0.5 m_b units. The best stations are CHG and KON (m_b of 4.35 and 4.38) and the average m_b of all stations is 4.56.

Table IV-1 also gives the detection thresholds in terms of M_s corresponding to our m_b values. The following relationship was used for this conversion and will be discussed in greater detail in the next section.

$$(3) \quad M_s = 1.20 m_b - 1.74 \pm 0.5$$

Thus, we obtained the value $\sigma_r = 0.5$ for use in Equation (2). Since the average estimate of σ_m as defined in (2) was 0.63 for the 11 single stations and we found a typical value $\sigma_M = 0.4$ for the detection curve based on M_s values, this value was used throughout to estimate 90 percent M_s thresholds.

3. VLPE Network Detection Capabilities

Detection statistics were computed for each of the three VLPE networks defined above and in Section II-B. The results are presented in Figures IV-14 through IV-19. Only those events were included for which at least one station in the network was operational (i.e. events where all channels were malfunctioning or contained mixed signals were deleted). Separate statistics were compiled for all events for which at least two stations were operational for each network and two-station detection was required.

Table IV-2 summarizes the results obtained by the maximum likelihood estimations for the three networks. It is interesting to notice that the networks requiring one operational station are almost equivalent in terms of 50 percent m_b threshold ($m_b \approx 4.2$).

Lambert and Becker (1973) indicated a decrease of 0.3 m_b units in the 90 percent detection levels between winter and summer networks for which one operational station was required. They attributed this difference to the presence of higher noise levels at specific VLPE sites during the winter. For this study, network 1 corresponds to the winter network and network 2 corresponds to the summer network with the addition of the August 1972 event ensemble. We now find only an insignificant decrease in the 90 percent threshold between network 1 and network 2.

In reviewing the histogram for network 2 (Figure IV-16), we find that a total of 3 events, one each at magnitudes (m_b) 5.0, 5.1, and 5.2, were not detected. Lambert and Becker had no missed detections for magnitudes (m_b) 4.9 and greater for the summer network. Thus, the effect upon VLPE network detection thresholds due to possible seasonal variations in noise levels is unresolved.

The 90 percent detection threshold for network 3 (event ensemble for November-December 1972) is less than those of the first two networks. This decrease in the 90 percent threshold may be due to variations in the number of stations and is probably insignificant since the 50 percent thresholds for the three networks are about equal ($m_b \approx 4.2$).

Comparing the networks requiring two operational stations and two stations detecting for a detection decision to the networks requiring one operational station, we expect a significant increase in the 50 percent detection threshold and only a slight increase for the 90 percent detection threshold. Wirth (1971) shows that for two stations and their associated detection probabilities, the exact probability for both stations detecting is the sum of the product of the single station probabilities. His result assumes that the same two stations are operational which is not the case here. Thus, the problem becomes much more complex and we cannot predict exactly the new detection probabilities.

TABLE IV-1
VLPE SINGLE STATION DETECTION THRESHOLDS
IN TERMS OF m_b AND M_s

| Station | Estimate of σ | Estimated 50 Percent m_b Thresholds | | | Corresponding M_s Thresholds | | | | | |
|----------|----------------------------|--|------|------|--------------------------------|----------------|----------------|---------------|----------------|----------------|
| | | All Events | <50 | >50 | 50 Percent | | | 90 Percent | | |
| | | | | | All Events | <50 Degrees | >50 Degrees | All Events | <50 Degrees | >50 Degrees |
| 1 CTA | 0.65 | 4.56 | - | 4.61 | 3.73 | - | 3.79 | 4.23 | - | 4.29 |
| 2 CHG | 0.67 | 4.35 | 4.18 | 4.50 | 3.48 | 3.28 | 3.66 | 3.98 | 3.78 | 4.16 |
| 3 FBK | 0.80 | 4.72 | 4.59 | 4.85 | 3.92 | 3.77 | 4.06 | 4.42 | 4.27 | 4.56 |
| 4 TLO | 0.71 | 4.53 | 4.13 | 4.69 | 3.60 | 3.22 | 3.88 | 4.10 | 3.72 | 4.38 |
| 5 EIL | 0.80 | 4.46 | 4.23 | 4.70 | 3.61 | 3.34 | 3.90 | 4.11 | 3.84 | 4.40 |
| 6 KON | 0.62 | 4.38 | 4.26 | 4.45 | 3.52 | 3.37 | 3.60 | 4.02 | 3.87 | 4.10 |
| 7 OGD | 0.68 | 4.66 | - | 4.66 | 3.85 | - | 3.95 | 4.35 | - | 4.35 |
| 8 KIP | 0.56 | 4.47 | 4.30 | 4.59 | 3.62 | 3.42 | 3.77 | 4.12 | 3.92 | 4.27 |
| 9 ALQ | 0.51 | 4.73 | - | 4.73 | 3.94 | - | 3.94 | 4.44 | - | 4.44 |
| 10 ZLP* | 0.55 | 4.88 | - | 4.88 | 4.12 | - | 4.12 | 4.62 | - | 4.62 |
| 11 MAT* | 0.34 | 4.44 | 4.27 | - | 3.59 | 3.38 | - | 4.09 | 3.88 | - |
| Averages | 0.63 | 4.56 | 4.28 | 4.66 | 3.73 | 3.40 | 3.86 | 4.23 | 3.90 | 4.36 |

*Insufficient data at these sites.

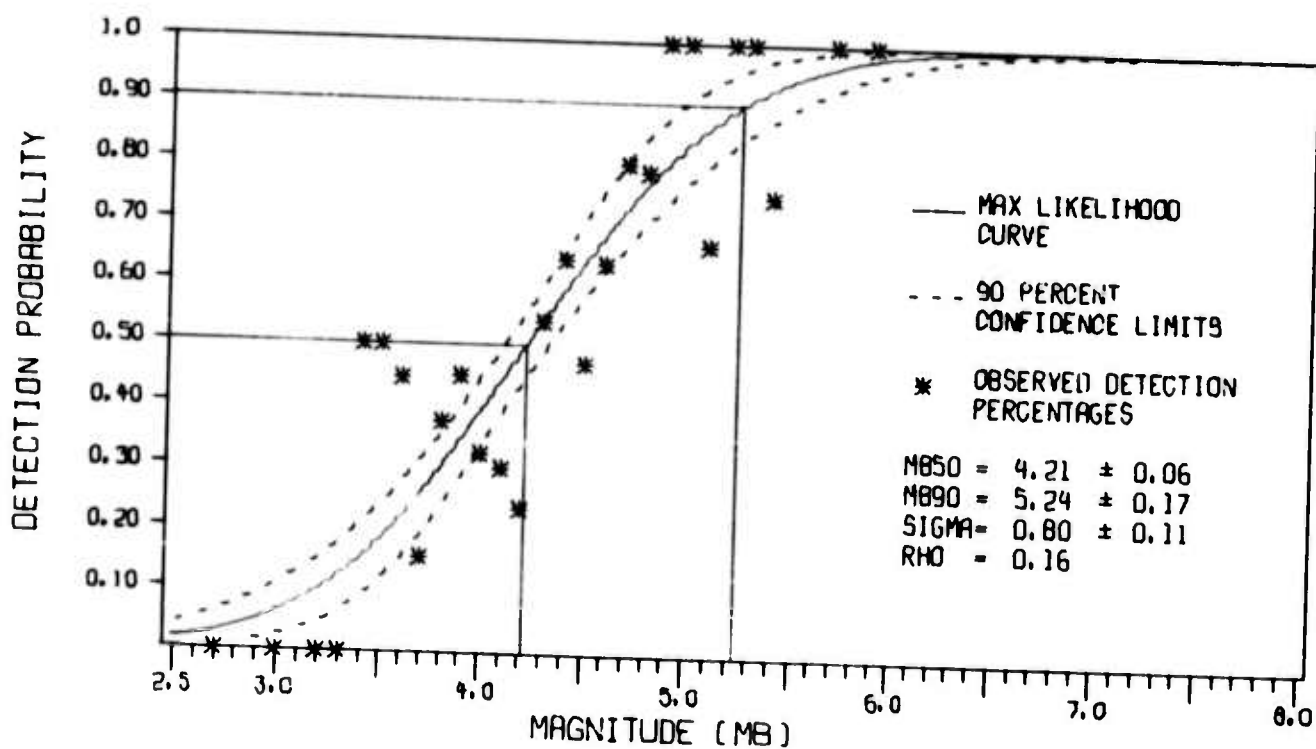
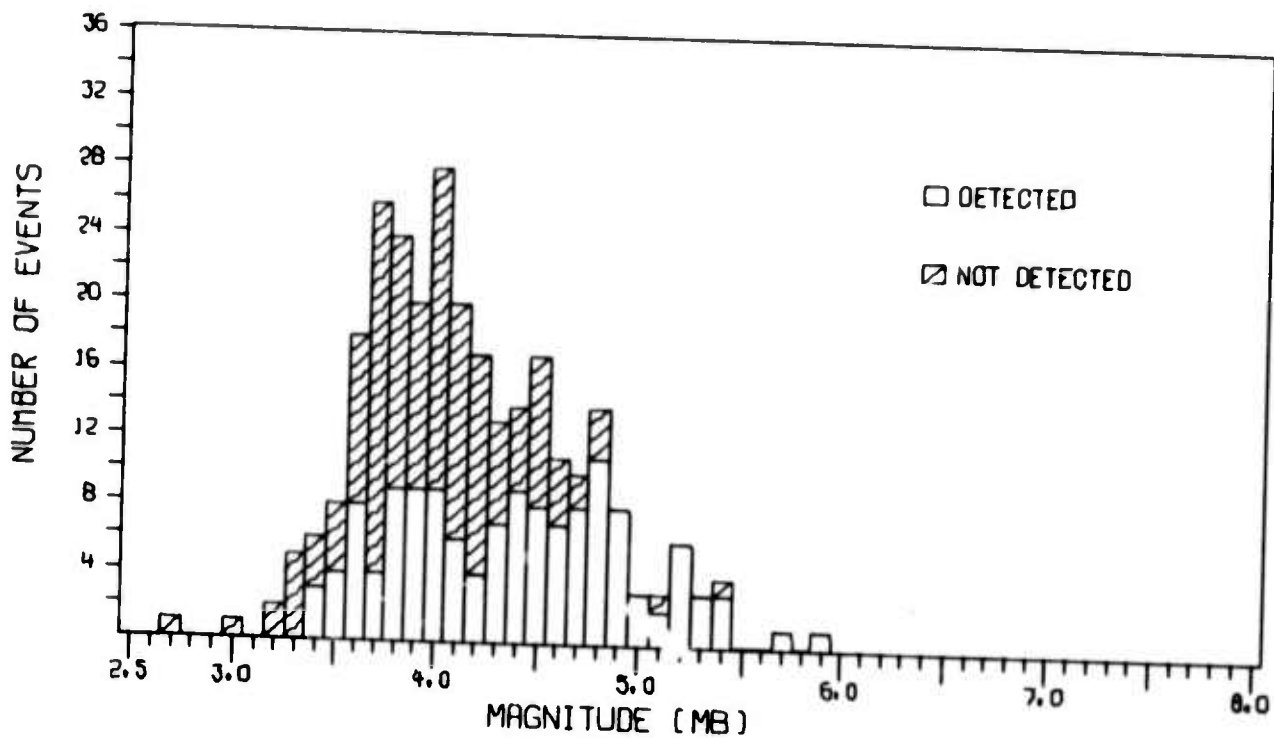


FIGURE IV-14
DETECTION STATISTICS FOR VLPE NETWORK 1
AT LEAST 1 OPERATIONAL STATION

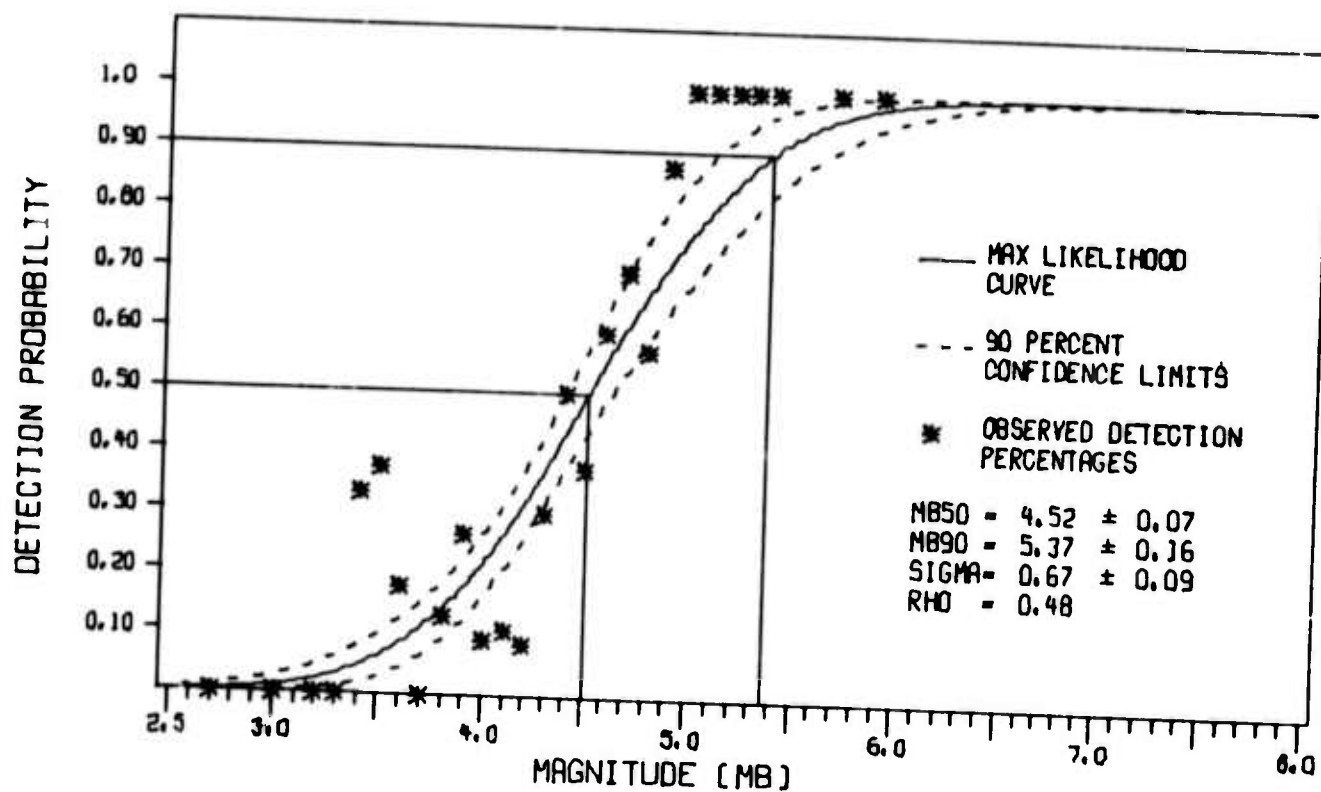
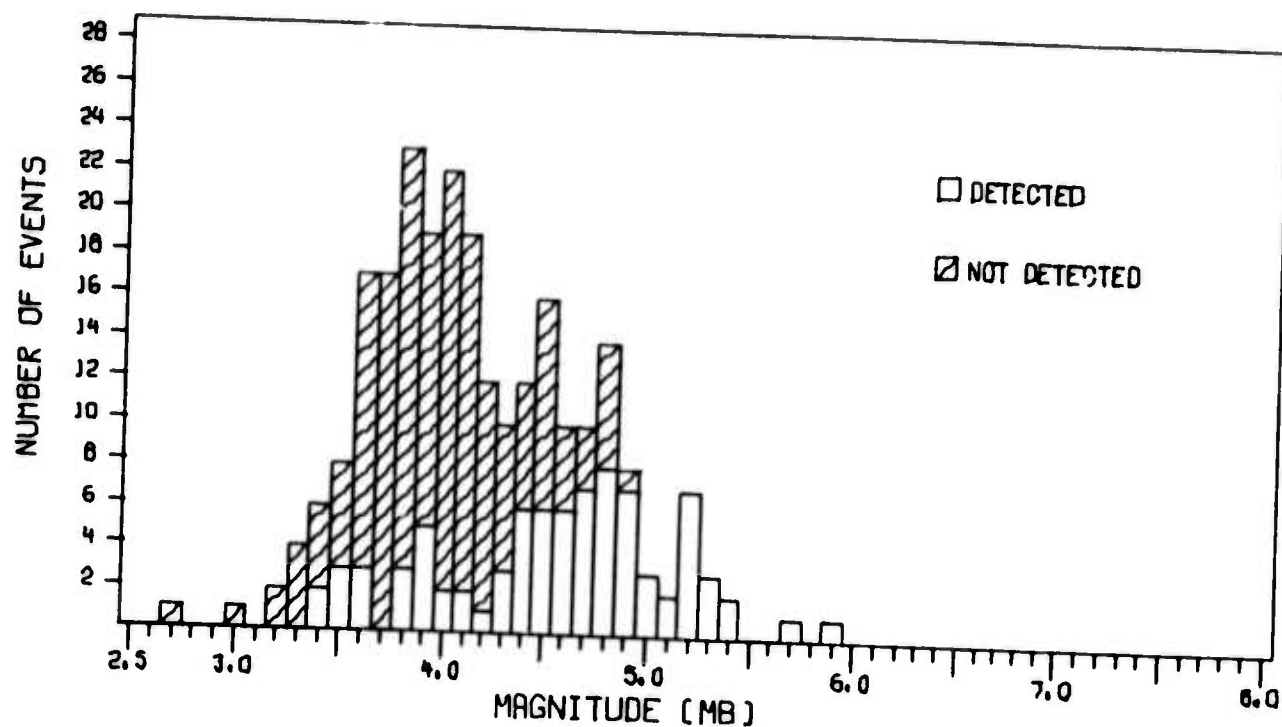


FIGURE VI-15
DETECTION STATISTICS FOR VLPE NETWORK I
AT LEAST 2 OPERATIONAL STATIONS

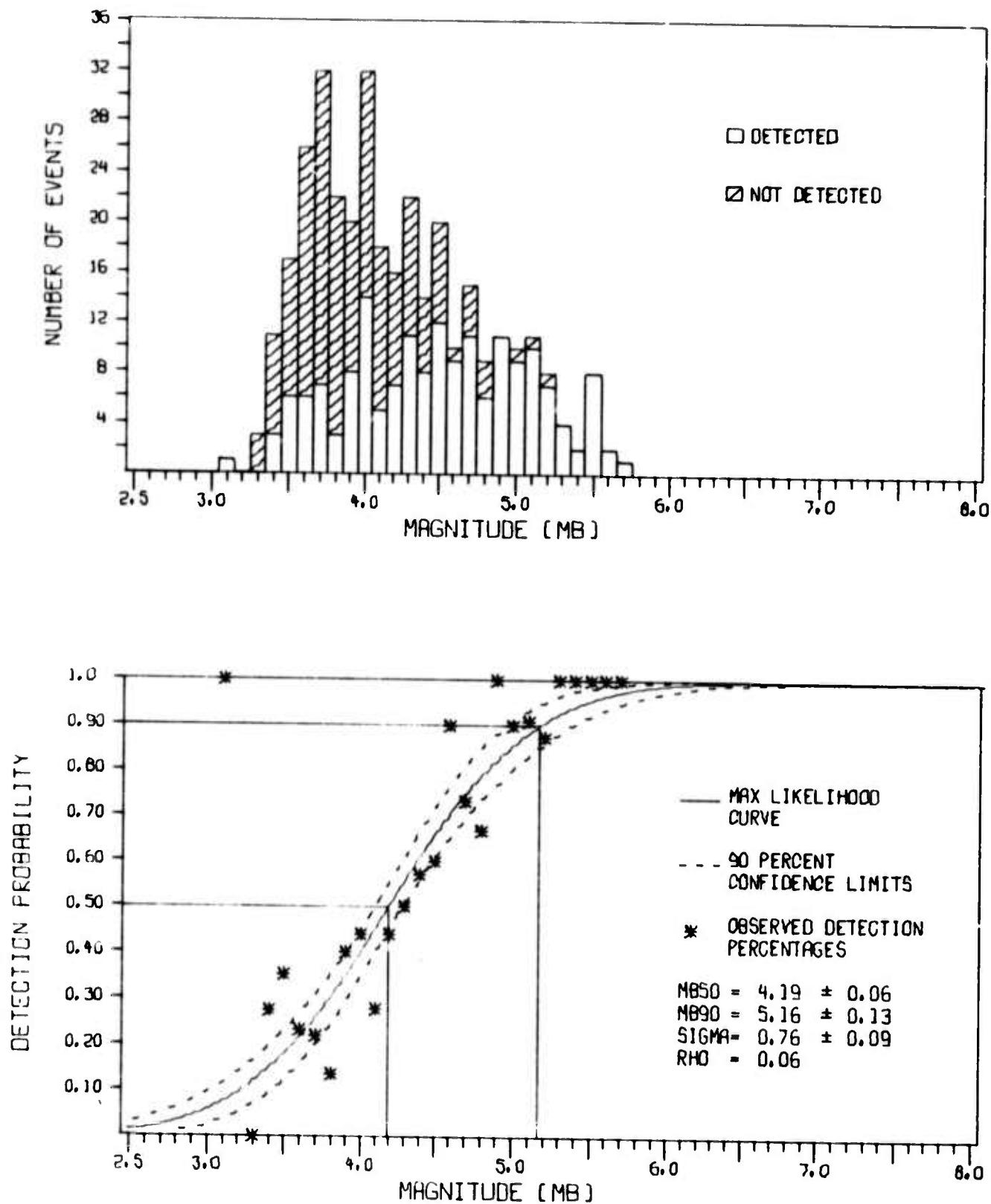


FIGURE IV-16
DETECTION STATISTICS FOR VLPE NETWORK 2
AT LEAST 1 OPERATIONAL STATION

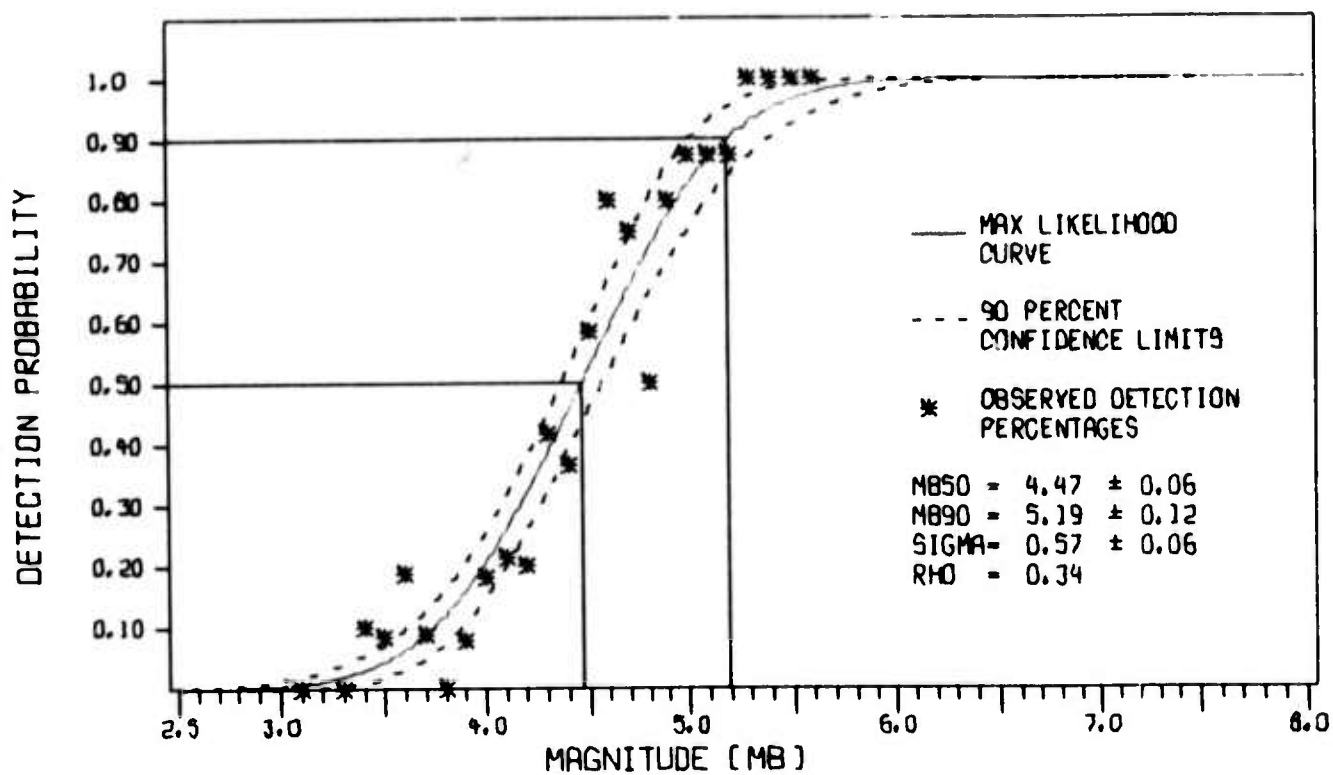
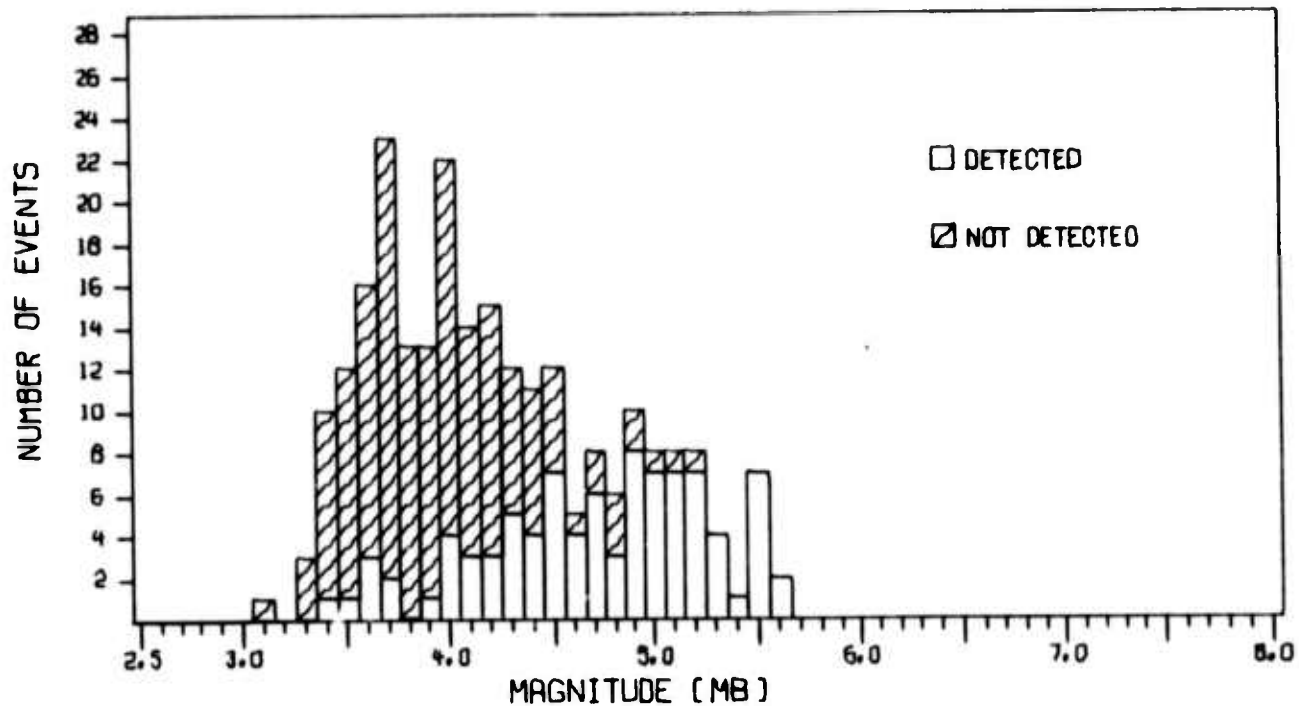


FIGURE IV-17
DETECTION STATISTICS FOR VLPE NETWORK 2
AT LEAST 2 OPERATIONAL STATIONS

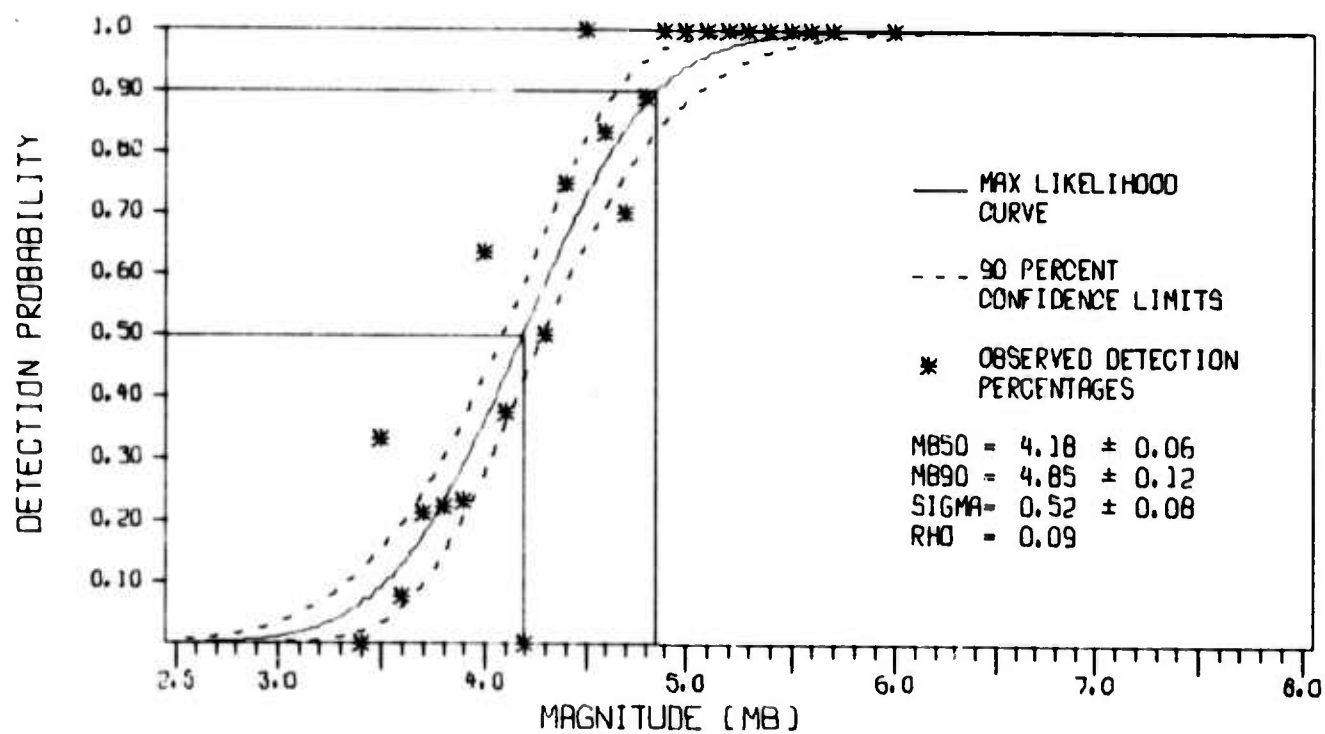
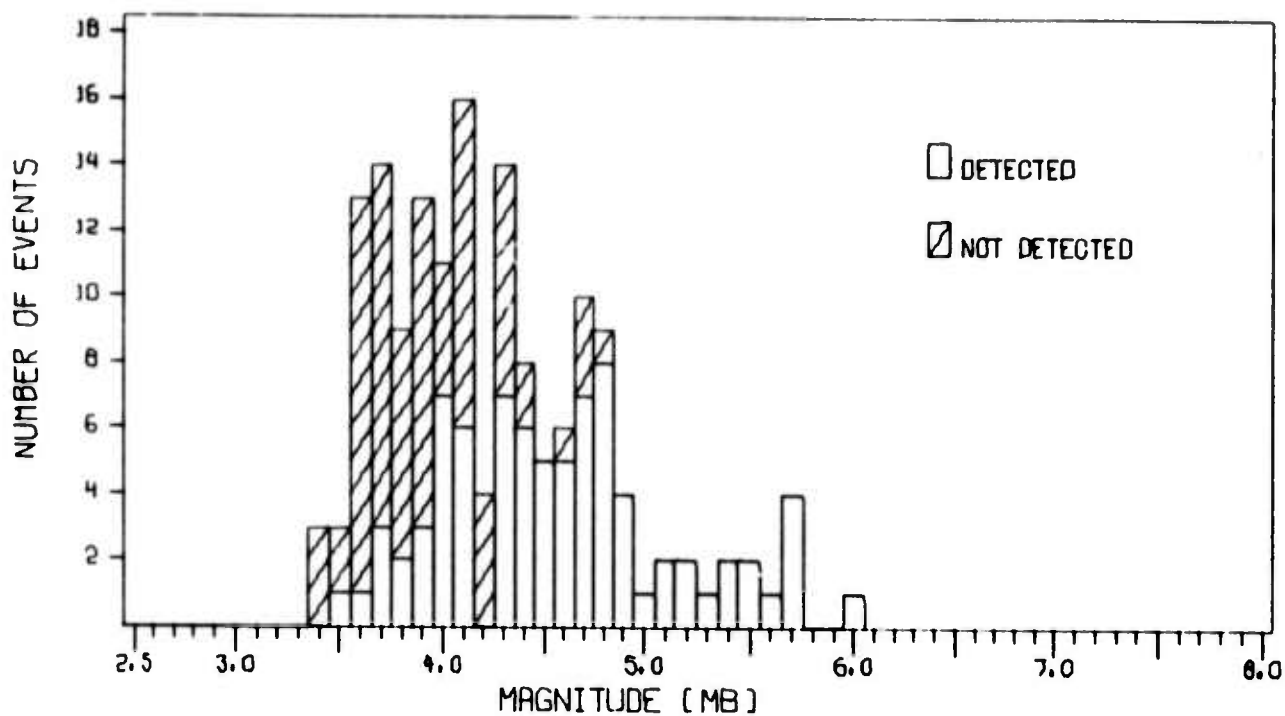


FIGURE IV-18

DETECTION STATISTICS FOR VLPE NETWORK 3
AT LEAST 1 OPERATIONAL STATION

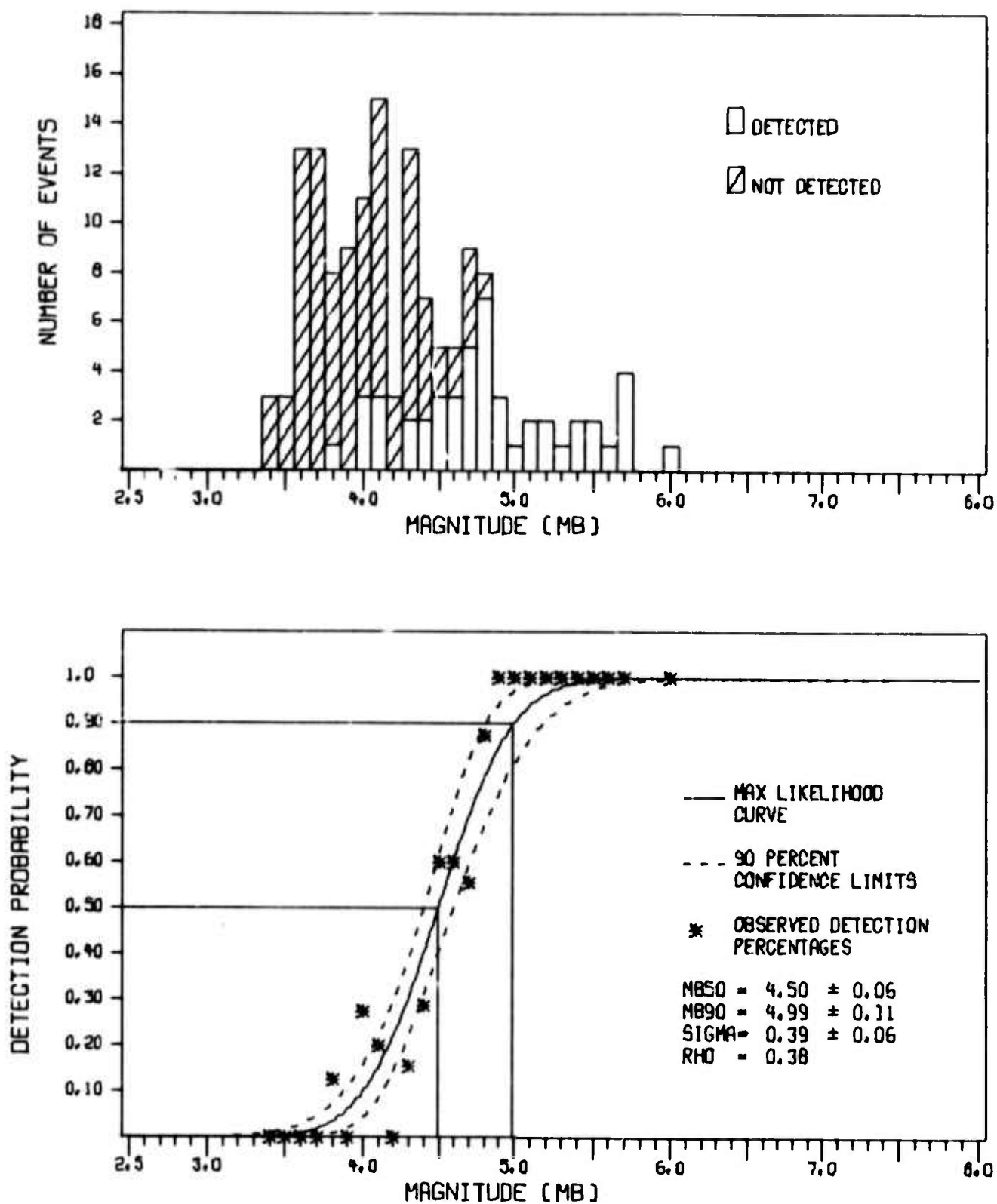


FIGURE IV-19
 DETECTION STATISTICS FOR VLPE NETWORK 3
 AT LEAST 2 OPERATIONAL STATIONS

The results of the maximum likelihood detection estimations for the two station networks do show increases of 0.3 m_b units and 0.1 m_b units for the 50 and 90 percent detection thresholds (Table IV-2). The 0.3 m_b units increase is significant while the 0.1 m_b units increase is small and both increases were as expected.

Table IV-2 also lists estimates of the detection thresholds in terms of M_s values, using the previously defined M_s versus m_b relationship and σ_M values. It should be emphasized, however, that these values are subject to significant uncertainties, and it is expected that more reliable estimates may be obtained in our future studies when direct detection statistics based on M_s values become available.

C. MIXED EVENT PROBABILITIES

Signals are classified as mixed events when one or more dispersed signals arrive adjacent to or overlapping onto either end of the expected signal velocity window. When this situation occurs, all epicenter source reports, location determinations, and magnitudes are reviewed in an attempt to resolve which signal is the expected one. If the problem is resolved in favor of the expected signal, a detection is indicated, but with an additional comment; the presence of mixed event signals. If the problem is not resolved, the signal was recorded as a mixed event signal. This study deals only with the latter classification, mixed event signal. Further, we consider only stations having signals detected, signals not detected, and mixed event signals as operational stations.

We determine the probability of mixed events occurring at VLPE networks based on our observational data. These probabilities are displayed in Table IV-3 and can be read in the following manner:

- Based on 844 events with at least one operational station, the probability is 0.22 that a given event appears as a mixed signal at a given station and 0.75 that the signal is not mixed.
- Similarly, 734 events had at least three stations operational.

TABLE IV-2
VLPE NETWORK DETECTION THRESHOLDS
IN TERMS OF m_b AND M_s

| | At Least 1 Operational Station | | | | At Least 2 Operational Stations | | | |
|-----------|--------------------------------|--------------|--------------|--------------|---------------------------------|--------------|--------------|--------------|
| | Detection Thresholds | | | | Detection Thresholds | | | |
| | 50% m_b | 90% m_b | 50% M_s | 90% M_s | 50% m_b | 90% m_b | 50% M_s | 90% M_s |
| Network 1 | 4.21 | 5.24 | 3.31 | 3.81 | 4.52 | 5.37 | 3.68 | 4.18 |
| Network 2 | 4.19 | 5.16 | 3.29 | 3.79 | 4.47 | 5.20 | 3.62 | 4.12 |
| Network 3 | 4.18 | 4.85 | 3.28 | 3.78 | 4.50 | 4.99 | 3.66 | 4.16 |

TABLE IV-3
NETWORK MIXED EVENT PROBABILITY STATISTICS

| | | Number of Events with i Operational Stations | | | | | |
|---------------------------|---|--|------|------|------|------|------|
| | | 844 | 817 | 734 | 470 | 237 | 40 |
| Number of Mixed Events, N | i | 1 | 2 | 3 | 4 | 5 | 6 |
| | 0 | 0.78 | 0.65 | 0.56 | 0.52 | 0.54 | 0.63 |
| | 1 | 0.22 | 0.24 | 0.26 | 0.23 | 0.20 | 0.10 |
| | 2 | | 0.11 | 0.11 | 0.12 | 0.12 | 0.09 |
| | 3 | | | 0.07 | 0.09 | 0.08 | 0.06 |
| | 4 | | | | 0.04 | 0.05 | 0.10 |
| | 5 | | | | | 0.01 | 0.00 |
| | 6 | | | | | | 0.02 |

Given a network of these stations, the probability that a given event will be seen as a mixed signal at all three is 0.07.

The actual number of mixed events that remain as mixed events for the total network was 49 and the average number of operational stations was 3.8. This translates into 5.8% (0.058 Probability) mixed events remaining with 3.8 operational stations for the total network. These values correspond closely to the appropriate probability numbers in Table IV-3.

The probability values shown under the columns for 5 and 6 operational stations (Table IV-3) clearly begin to misbehave. This is due to the smaller number of events actually having 5 and 6 operational stations per event. However, these values do give some estimate of the VLPE network requirements to further reduce the probability of mixed events occurring at all stations. Obviously, the percentage of mixed events is related to the detection capability of the station, (i. e. the more events a station detects, the greater is the probability of mixed events occurring). Thus the probabilities determined here are valid only for the present VLPE capability. It is also noteworthy that the percentage of mixed events at NORSAR LP is also 22% (Swindell, 1973). Thus, with respect to mixed events in this case, the added detection capability of NORSAR relative to VLPE stations, is offset by the spatial resolution provided by the array.

D. MATCHED FILTER AND THREE COMPONENT ADAPTIVE PROCESSOR PERFORMANCE

1. Discussion

Matched filters (reference waveform and chirp) and the Three Component Adaptive processor (TCA) were applied to a restricted suite of events as recorded at the VLPE stations to evaluate their effectiveness in increasing the signal-to-noise ratios of dispersed seismic signals. Reference waveform and chirp filters were applied to the transverse Love wave and the vertical Rayleigh wave of each test event. The TCA processor makes use of all three instrumental components (Lane, 1973). The goals of this analysis are:

- To obtain a first approximation of potential signal-to-noise ratio gains of reference waveform and chirp matched filters.
- To estimate the effectiveness of matched filters in increasing the surface-wave detection capability of the VLPE stations.
- To compare the relative effectiveness of reference waveform and chirp matched filters.
- To obtain a first estimate of the TCA processor detection capability.

Analysis of data recorded at the Alaskan Long-Period Array (Strauss, 1973) indicated that chirp filters were slightly more effective than reference waveform filters, that matched filters reduced the number of non-detected events by about 20 per cent, and that the greatest change in the detection versus body-wave magnitude plots caused by inclusion of these detections occurred at the 50 percent detection level. Analysis of data recorded at the Norwegian Seismic Array (Laun et al, 1973) indicated that reference waveform filters were slightly more effective than chirp filters, that matched filters reduced the number of non-detected events by about 10 percent, and that inclusion of these detections in the detection versus body-wave magnitude plots caused changes between the 30 percent and 90 percent detection levels.

Matched filter performance was analysed in terms of detection improvement and signal-to-noise ratio improvement over the equivalent bandpass signal-to-noise ratio. Each signal-to-noise ratio was calculated as the ratio of the peak value of the signal to the root-mean-square (RMS) value of the noise as measured in a gate ahead of the signal. The signal-to-noise ratio improvement of a matched filtered trace over the corresponding bandpass trace, expressed in decibels, is:

$$\text{IMPROVEMENT (dB)} = 20 \text{ LOG } \left(\frac{\text{SNR}_{\text{matched filter}}}{\text{SNR}_{\text{Bandpass filter}}} \right)$$

Since the signals are not noise-free, the signal amplitudes are actually signal-plus-noise amplitudes. For this reason, we will hereafter refer to the signal-plus-noise to noise ratio (SNNR).

The performance of the TCA processor was analysed only in terms of detection improvement.

2. Data Base

A suite of 29 earthquakes and 8 presumed explosions was selected for this first evaluation of matched filter performance for the VLPE stations. These events and their associated parameters are listed in Tables IV-4 and IV-5. (The ninth presumed explosion in the list was used as a reference waveform but was otherwise not included in the analysis.) An X under a station number indicates that this station was operating at the time this event occurred; an * indicates that the event as recorded at this station was used as a reference waveform. This suite of earthquakes and presumed explosions were analysed and reported in Special Report No. 6, Extended Array Evaluation Program (Lambert and Becker, 1973). The earthquakes all have epicenters in or near northern Sinkiang (strippld area in Figure IV-20). This region was chosen for its proximity to the eastern Kazakh test area and to minimize regional variations. The general location of the presumed explosions are indicated in Figure IV-20 by solid black spots.

Inspection of Table IV-4 reveals that events 0075 and 0076 have origin times differing by 10 seconds and 0317 and 0318 have origin times differing by 27 seconds. It is believed that these pairs of events are actually single events. In the case of the first pair of events, both were reported by NORSAR with the second event being perhaps picked from a depth phase of the first. In the case of the second pair, one was reported by PDE and the other by NORSAR; the difference in origin times is perhaps due to errors in picking the records. Therefore, these pairs of events will hereafter be considered as single events and will be reported as 0075

TABLE IV-4
EARTHQUAKE EVENT LIST
(PAGE 1 OF 2)

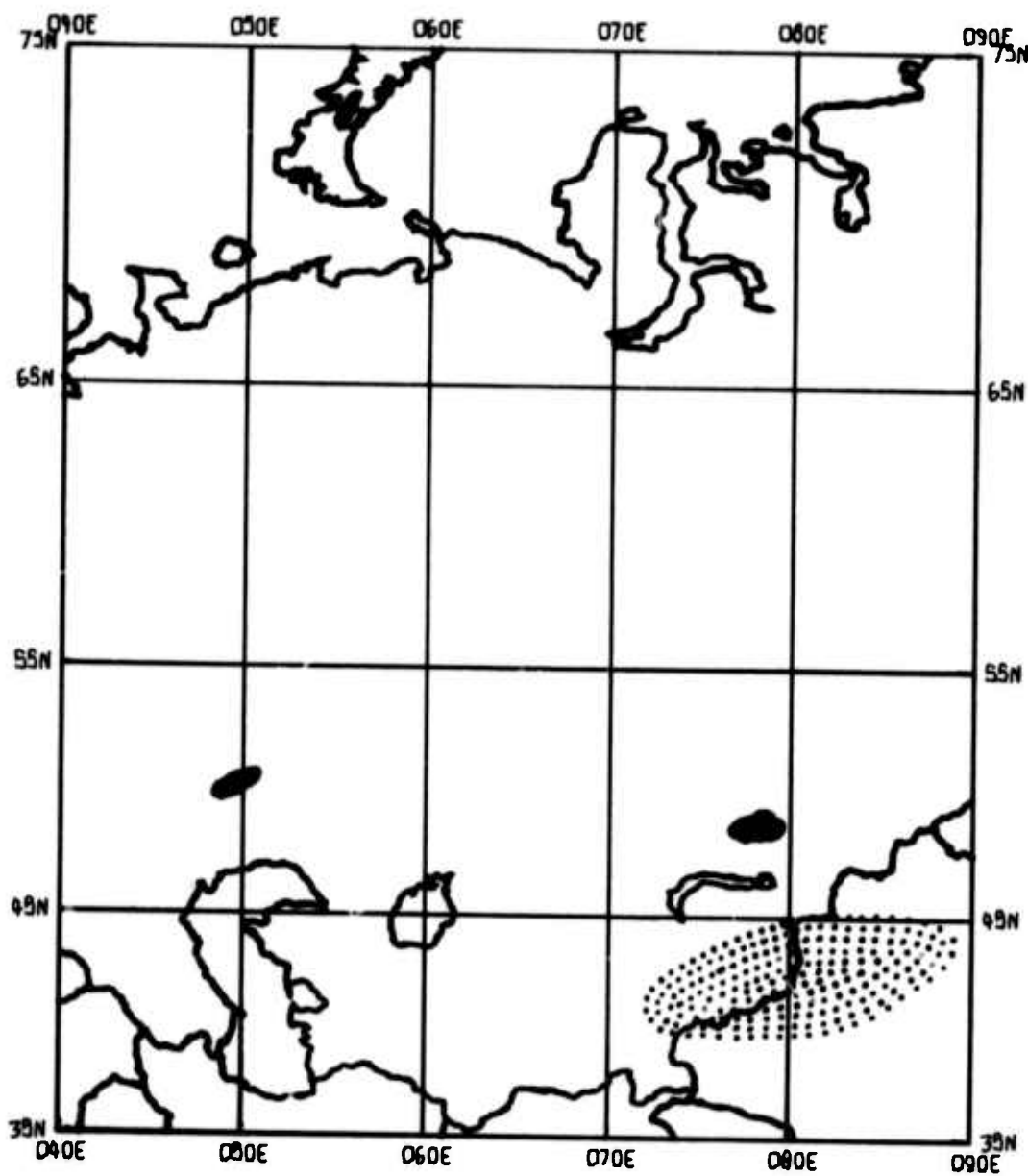
| Event Number | Month | Day | Origin Time | m _b | Lat °N | Long °E | Available Stations | | | | | | | | |
|--------------|-------|-----|-------------|----------------|-----------|------------|--------------------|---|---|---|---|---|---|---|---|
| | | | | | | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 0006 | 01 | 02 | 10.27.35 | 5.2 | 41.8 | 84.5 | | * | X | * | | | X | | |
| 0021 | 01 | 06 | 06.30.36 | 4.7 | 40.7 | 72.4 | | * | X | X | | | X | | |
| 0044 | 01 | 15 | 20.21.50 | 5.4 | 40.3 | 79.0 | | * | * | * | | | * | | |
| 0045 | 01 | 15 | 20.45.22 | 4.6 | 39.3 | 79.9 | | X | X | X | | X | X | | |
| 0075 | 01 | 28 | 20.29.09 | 4.5 | 40.8 | 81.4 | | X | X | X | | X | X | | |
| 0076 | 01 | 28 | 20.29.19 | 4.4 | 43.0 | 78.0 | | X | X | X | | X | X | | |
| 0108 | 02 | 06 | 07.30.11 | 4.7 | 41.6 | 82.2 | | | X | X | | X | X | | |
| 0120 | 02 | 11 | 05.55.46 | 4.9 | 39.9 | 77.4 | | | X | X | | X | | | |
| 0129 | 02 | 16 | 23.19.20 | 4.8 | 41.7 | 80.7 | | | X | | | * | X | | |
| 0225 | 03 | 02 | 19.57.42 | 3.5 | 43.0 | 76.0 | | | X | | | X | X | | |
| 0235 | 03 | 04 | 04.00.09 | 4.5 | 40.0 | 80.0 | | | X | | | | X | | |
| 0236 | 03 | 04 | 08.22.16 | 4.4 | 43.0 | 86.0 | | | X | | | | X | | |
| 0238 | 03 | 04 | 18.24.11 | 5.1 | 39.0 | 75.0 | | | X | | | | X | | |
| 0302 | 03 | 18 | 19.54.18 | 3.2 | 41.0 | 72.0 | | | X | X | | X | | | |
| 0309 | 03 | 20 | 21.47.55 | 3.4 | 40.0 | 80.0 | | | X | X | | X | | | |
| 0317 | 06 | 02 | 04.21.49 | 3.8 | 42.0 | 82.0 | X | | | | X | X | | X | X |
| 0318 | 06 | 02 | 04.22.16 | 3.7 | 42.0 | 82.0 | X | | | | X | X | | X | X |
| 0319 | 06 | 02 | 05.11.13 | 3.5 | 43.0 | 81.0 | X | | | | X | X | | X | X |

TABLE IV-4
EARTHQUAKE EVENT LIST
(PAGE 2 OF 2)

| Event Number | Month | Day | Origin Time | m _b | Lat °N | Long °E | Available Stations | | | | | | | | |
|--------------|-------|-----|-------------|----------------|-----------|------------|--------------------|---|---|---|---|---|---|---|---|
| | | | | | | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 0320 | 06 | 02 | 06.30.49 | 3.9 | 42.0 | 81.0 | X | | | | X | X | | X | X |
| 0384 | 06 | 18 | 09.18.49 | 4.3 | 40.0 | 73.0 | | | | | | | X | X | X |
| 0449 | 07 | 05 | 01.09.53 | 4.6 | 44.6 | 81.1 | | | | * | X | | | | |
| 0450 | 07 | 05 | 02.41.54 | 3.5 | 44.0 | 86.0 | | | | X | X | | | X | |
| 0451 | 07 | 05 | 04.09.49 | 4.3 | 43.6 | 87.9 | | | | X | X | | | X | |
| 0470 | 07 | 10 | 19.03.33 | 4.7 | 43.4 | 88.6 | X | | | X | X | X | | X | |
| 0491 | 07 | 15 | 00.35.52 | 3.8 | 43.0 | 78.0 | X | | | X | X | | | X | X |
| 0510 | 07 | 18 | 03.27.07 | 4.0 | 39.0 | 77.0 | X | | | X | X | | | X | |
| 0536 | 07 | 28 | 05.50.29 | 4.3 | 42.0 | 81.0 | X | | | | X | | | | |
| 0604 | 08 | 09 | 16.28.14 | 4.5 | 41.0 | 72.0 | | | | X | X | | | X | |
| 0662 | 08 | 22 | 16.34.56 | 4.6 | 40.0 | 79.0 | X | | | X | X | | | X | |

TABLE IV-5
PRESUMED EXPLOSION EVENT LIST

| Event Number | Month | Day | Origin Time | m _b | Lat °N | Long °E | Available Stations | | | | | | | | |
|--------------|-------|-----|-------------|----------------|-----------|------------|--------------------|---|---|---|---|---|---|---|---|
| | | | | | | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 0116 | 02 | 10 | 05.02.57 | 5.5 | 50.0 | 78.9 | | | X | X | | X | | | |
| 0260 | 03 | 10 | 04.56.57 | 5.5 | 50.0 | 78.0 | | | X | | | X | | | |
| 0339 | 06 | 07 | 01.27.57 | 5.5 | 49.8 | 78.2 | | | | | X | X | | | |
| 0456 | 07 | 06 | 01.02.58 | 4.4 | 49.7 | 78.2 | | | | | X | X | | X | |
| 0626 | 08 | 16 | 03.16.57 | 5.2 | 49.8 | 78.1 | | | | X | X | | | X | |
| 0652 | 08 | 20 | 02.59.58 | 5.7 | 49.5 | 48.2 | | | | X | X | | | X | |
| 0672 | 08 | 26 | 03.46.57 | 5.5 | 50.0 | 77.8 | | | | X | X | | | X | |
| 0679 | 08 | 28 | 05.59.56 | 6.3 | 73.3 | 55.1 | | X | | X | | | | X | |
| 0797 | 12 | 10 | 04.26.58 | 5.7 | 49.8 | 78.1 | | * | | | | | | * | |



MILLER MODIFIED MERCATOR PROJECTION
MAP SCALE: 1,000 IN./ 10 DEG. LONGITUDE

FIGURE IV-20
LOCATION OF AREAS OF INTEREST

and 0317, respectively. This results in a revised data base of 27 events and 8 presumed explosions.

Each earthquake or presumed explosion as recorded at a given station will be considered to be an individual event and will hereafter be referred to as a station-event. There are, therefore, a total of 98 station-events derived from the 27 earthquakes and 31 station-events derived from the 8 presumed explosions.

The data base used for the TCA processor did not include all of the station-events used in the matched filter analysis, since some of the station-events could not be handled by this method due to malfunctioning components. A total of 78 station-events were TCA-processed.

3. Matched Filter Application

a. Reference Waveform Filters

A subset of 11 reference waveform station-events (9 earthquake, 2 presumed explosion) was selected for this evaluation of reference waveform matched filtering. These station-events are indicated in Tables IV-4 and IV-5 by an asterisk under the appropriate station number. The selection criteria were: good SNNR and shallow (less than 60 km) focus. The length of the reference waveforms was chosen in the following manner: for events at large epicentral distances, the length was selected to include possible multipath energy, since small changes in event epicenter location would not be expected to significantly change the multipath structure. This situation is reversed for events at small epicentral distances; for such events, small changes in event epicenter location could significantly change the multipath effects, if any. Therefore, the lengths of reference waveforms having small epicentral distances were chosen so as to exclude any possible multipath energy.

The major problem encountered in this form of matched filtering

was obtaining satisfactory reference waveforms. Due to the limited number of suitable events available, reference waveforms could be generated only for earthquakes recorded at stations 2, 3, 4, 6, and 7 and for presumed explosions recorded at stations 2 and 8. Also, it was desirable to have more than one reference waveform for application to events from a given region as recorded at a given station, since succeeding events from a region may have different source mechanisms, resulting in a poor match between reference waveform and test event. Due again to the limited size of the data base, it was possible to generate more than one reference waveform for stations 2 and 4 only (3 reference waveforms each). These difficulties will be alleviated in future work with the expansion of the data base.

b. Chirp Match Filters

Linear chirp filters were applied to all the station-events listed in Table IV- 4 and 5. These chirp filters were specified and applied in the frequency domain, using a chirp bandpass of 0.023 to 0.59 Hz. After application of these filters, the data were inverse-transformed to obtain time domain chirp filter outputs.

The chirp filter response function is:

$$G(K) = \begin{cases} e^{i2\pi(C/N)(K-K_0)^2} & \text{if } K_L \leq K \leq K_H \\ 0 & \text{if } 0 \leq K \leq (K_L - K_H) \leq K \leq N/2 \end{cases}$$

$$G(-K) = G(K)^*$$

where

K is the discrete Fourier transform frequency index.

K_L and K_H are the lowest and highest frequencies in the passband.

K_0 is the frequency index at which zero phase shift occurs.

N is the number of transform points.

C is a parameter which controls the length of the corresponding time-domain waveform.

This yields a dispersive time-domain waveform with a linear group delay and essentially flat amplitude at all periods in the band corresponding to $K_L \leq K \leq K_H$ (Harley, 1971).

A minimum of five chirps were applied to each station-event. Their lengths were centered about the assumed optimum length (based on station-event separation) and differed by increments of ± 100 seconds. The SNNR improvement for the station-event pair was then measured from the best, in terms of amplitude and shape, of the chirp responses. In each case, sufficient chirps were applied to ensure that the best chirp response was in fact found.

c. The Three Component Adaptive Processor (TCA)

The TCA processor forms a single channel filter in the frequency domain which passes energy having some of the characteristics of Love and Rayleigh waves. The filter is adaptive, since the data is segmented with a new filter designed for each segment. The filter weights depend on the signal behavior during the segment, rather than on the signal behavior for some fixed time before or after the output point.

The advantage of the TCA processor lies in the fact that it changes its filter weights to pass properly polarized energy. The output of the TCA processor is a filtered seismogram, not a new quantity.

To pass Rayleigh wave energy, the processor looks for signals which are 90° out of phase on the radial and vertical components. The Fourier transform of a segment of data is taken and the phase angle between radial and vertical components calculated at each frequency. (This angle will be $\frac{\pi}{2}$ for fundamental Rayleigh waves.) Some power of the sine of this phase angle constitutes the frequency domain filter weight for the corresponding frequency.

The Love wave filter calculates the angle, in space, between

the transverse direction and the direction of particle motion at each frequency. (This angle will be zero for pure Love wave energy.) Some power of the cosine of this angle is the filter weight. This filter is strictly a polarization filter for transverse waves (Lane, 1973).

4. SNNR Gains - Reference Waveform and Chirp Filters

Reference waveform filters were applied to 54 earthquake station-events and 10 presumed explosion station-events. Table IV-6 presents the results of the filter application. The amount of data available is too small to make meaningful statements about the behavior of individual reference waveform filters. Therefore, only the overall average SNNR improvements for the Reference waveform filter will be considered here. These average improvements are:

| | SNNR IMPROVEMENT (dB) | |
|--------------------|-----------------------|------|
| | RAYLEIGH | LOVE |
| EARTHQUAKE | 3.5 | 0.1 |
| PRESUMED EXPLOSION | 3.8 | -2.7 |

Unger (1973) shows an average optimum reference waveform filter gain of 4.0 to 8.0 dB for ALPA and events from Central Asia. However, we did not process these events in a similar exhaustive manner to obtain optimum gains. Further, these average values do not include the SNNR improvements derived from the match of a reference waveform with the event itself, since inclusion of these values would have given a high bias to the averages. The low SNNR (0.1 dB) improvement for earthquake Love waves is primarily due to poor quality (low SNNR) reference waveforms available from the VLPE. No or low amplitude Love waves would normally be expected from explosions, depending upon the amount of tectonic strain release accompanying the explosion, but the large negative gain shown above is again indicative of the poor quality of the reference waveforms available.

TABLE IV-6
RESULTS OF REFERENCE WAVEFORM FILTERING
(PAGE 1 OF 4)

| EVENT | STA | RWF | mb | RWF/TEST EV SEP | DETECTION | | | | SNNR IMPROVEMENT (dB) | | TYPE |
|-------|-----|-----|-----|--------------------|-----------|----|-----|----|-----------------------------|------|------|
| | | | | | BP | | RWF | | LR | LQ | |
| | | | | | LR | LQ | LR | LQ | | | |
| 6 | 2 | 6 | 5.2 | 0 | 1 | 1 | 1 | 1 | 7.7 | 3.2 | C |
| 6 | 4 | 6 | 5.2 | 0 | 1 | 1 | 1 | 1 | 7.4 | 2.8 | F |
| 21 | 2 | 6 | 4.7 | 1255 | 1 | 1 | 1 | 1 | 3.0 | -2.9 | F |
| 21 | 4 | 6 | 4.7 | 1255 | 2 | 2 | 2 | 2 | --- | --- | F |
| 44 | 2 | 6 | 5.4 | 744 | 1 | 1 | 1 | 1 | 2.3 | 3.3 | F |
| 44 | 4 | 6 | 5.4 | 744 | 1 | 1 | 1 | 1 | 5.5 | 5.0 | F |
| 45 | 2 | 6 | 4.6 | 731 | 1 | 3 | 1 | 3 | --- | --- | F |
| 45 | 4 | 6 | 4.6 | 731 | 1 | 3 | 1 | 3 | --- | --- | F |
| 75 | 2 | 6 | 4.5 | 537 | 2 | 2 | 2 | 2 | --- | --- | F |
| 75 | 4 | 6 | 4.5 | 537 | 2 | 2 | 2 | 2 | --- | --- | F |
| 108 | 4 | 6 | 4.7 | 440 | 2 | 2 | 1 | 2 | --- | --- | F |
| 302 | 4 | 6 | 3.2 | 1279 | 2 | 2 | 2 | 2 | --- | --- | F |
| 309 | 4 | 6 | 3.4 | 683 | 2 | 2 | 2 | 2 | --- | --- | F |
| 449 | 4 | 6 | 4.6 | 537 | 1 | 1 | 1 | 1 | 3.9 | 1.3 | F |
| 450 | 4 | 6 | 3.5 | 170 | 2 | 2 | 2 | 2 | --- | --- | F |
| 451 | 4 | 6 | 4.3 | 101 | 2 | 2 | 2 | 2 | --- | --- | F |
| 491 | 4 | 6 | 3.8 | 757 | 2 | 2 | 1 | 2 | --- | --- | F |
| 604 | 4 | 6 | 4.5 | 1279 | 1 | 3 | 3 | 3 | --- | --- | F |
| 6 | 2 | 21 | 5.2 | 1255 | 1 | 1 | 1 | 1 | 0.6 | 3.3 | F |
| 21 | 2 | 21 | 4.7 | 0 | 1 | 1 | 1 | 1 | 12.3 | 9.0 | F |
| 44 | 2 | 21 | 5.4 | 559 | 1 | 1 | 1 | 1 | 4.5 | -3.7 | F |
| 45 | 2 | 21 | 4.6 | 657 | 3 | 3 | 3 | 3 | --- | --- | F |
| 75 | 2 | 21 | 4.5 | 757 | 2 | 2 | 2 | 2 | --- | --- | F |
| 6 | 2 | 44 | 5.2 | 744 | 1 | 1 | 1 | 1 | 2.7 | -2.8 | F |
| 6 | 3 | 44 | 5.2 | 744 | 2 | 2 | 2 | 2 | --- | --- | F |
| 6 | 4 | 44 | 5.2 | 744 | 1 | 1 | 1 | 1 | 3.2 | 0.4 | F |
| 6 | 7 | 44 | 5.2 | 744 | 2 | 2 | 6 | 2 | --- | --- | F |

TABLE IV-6
RESULTS OF REFERENCE WAVEFORM FILTERING
(PAGE 2 OF 4)

| EVENT | STA | RWF | m _b | RWF/TEST EV SEP | DETECTION | | | | SNNR IMPROVEMENT (dB) | | TYPE |
|-------|-----|-----|----------------|--------------------|-----------|----|-----|----|-----------------------------|------|------|
| | | | | | BP | | RWF | | LR | LQ | |
| | | | | | LR | LQ | LR | LQ | | | |
| 21 | 2 | 44 | 4.7 | 559 | 1 | 1 | 1 | 1 | 2.6 | -6.6 | F |
| 21 | 3 | 44 | 4.7 | 559 | 2 | 2 | 1 | 2 | --- | --- | F |
| 21 | 4 | 44 | 4.7 | 559 | 2 | 2 | 6 | 2 | --- | --- | F |
| 21 | 7 | 44 | 4.7 | 559 | 2 | 2 | 6 | 2 | --- | --- | F |
| 44 | 2 | 44 | 5.4 | 0 | 1 | 1 | 1 | 1 | 11.0 | 11.5 | F |
| 44 | 3 | 44 | 5.4 | 0 | 1 | 1 | 1 | 1 | 8.6 | 12.2 | F |
| 44 | 4 | 44 | 5.4 | 0 | 1 | 1 | 1 | 1 | 11.3 | 9.0 | F |
| 44 | 7 | 44 | 5.4 | 0 | 1 | 1 | 1 | 1 | 12.2 | 11.4 | F |
| 45 | 2 | 44 | 4.6 | 135 | 3 | 3 | 3 | 6 | --- | --- | F |
| 45 | 3 | 44 | 4.6 | 135 | 3 | 3 | 6 | 6 | --- | --- | F |
| 45 | 4 | 44 | 4.6 | 135 | 3 | 3 | 6 | 3 | --- | --- | F |
| 45 | 7 | 44 | 4.6 | 135 | 3 | 3 | 3 | 5 | --- | --- | F |
| 75 | 2 | 44 | 4.5 | 210 | 2 | 2 | 1 | 1 | --- | --- | F |
| 75 | 3 | 44 | 4.5 | 210 | 2 | 2 | 2 | 2 | --- | --- | F |
| 75 | 4 | 44 | 4.5 | 210 | 2 | 2 | 2 | 2 | --- | --- | F |
| 75 | 7 | 44 | 4.5 | 210 | 2 | 2 | 2 | 2 | --- | --- | F |
| 108 | 3 | 44 | 4.7 | 305 | 2 | 2 | 2 | 6 | --- | --- | F |
| 108 | 4 | 44 | 4.7 | 305 | 2 | 2 | 2 | 2 | --- | --- | F |
| 108 | 7 | 44 | 4.7 | 305 | 2 | 2 | 6 | 6 | --- | --- | F |
| 120 | 3 | 44 | 4.9 | 143 | 1 | 1 | 1 | 1 | 6.9 | -1.8 | F |
| 120 | 4 | 44 | 4.9 | 143 | 5 | 5 | - | - | --- | --- | F |
| 129 | 3 | 44 | 4.8 | 211 | 1 | 1 | 1 | 1 | 7.5 | 0.6 | F |
| 129 | 7 | 44 | 4.8 | 211 | 3 | 3 | 3 | 3 | --- | --- | F |
| 225 | 3 | 44 | 3.5 | 390 | 3 | 3 | 3 | 3 | --- | --- | F |
| 225 | 7 | 44 | 3.5 | 390 | 3 | 3 | 3 | 3 | --- | --- | F |
| 235 | 3 | 44 | 4.5 | 91 | 1 | 1 | 1 | 1 | --- | --- | F |
| 235 | 7 | 44 | 4.5 | 91 | 3 | 3 | 6 | 3 | --- | --- | F |

TABLE IV-6
RESULTS OF REFERENCE WAVEFORM FILTERING
(PAGE 3 OF 4)

| EVENT | STA | RWF | m _b | RWF/TEST EV SEP | DETECTION | | | | SNNR IMPROVEMENT (dB) | | TYPE |
|-------|-----|-----|----------------|--------------------|-----------|----|-----|----|-----------------------------|------|------|
| | | | | | BP | | RWF | | LR | LQ | |
| | | | | | LR | LQ | LR | LQ | | | |
| 236 | 3 | 44 | 4.4 | 654 | 2 | 2 | 2 | 6 | --- | --- | F |
| 238 | 3 | 44 | 5.1 | 371 | 2 | 2 | 1 | 1 | --- | --- | F |
| 238 | 7 | 44 | 5.1 | 371 | 3 | 3 | 1 | 3 | --- | --- | F |
| 302 | 3 | 44 | 3.2 | 595 | 2 | 2 | 2 | 2 | --- | --- | F |
| 302 | 4 | 44 | 3.2 | 595 | 2 | 2 | 2 | 2 | --- | --- | F |
| 309 | 3 | 44 | 3.4 | 91 | 2 | 2 | 2 | 2 | --- | --- | F |
| 309 | 4 | 44 | 3.4 | 91 | 2 | 2 | 2 | 2 | --- | --- | F |
| 449 | 4 | 44 | 4.6 | 508 | 1 | 1 | 1 | 1 | 0.6 | 0.5 | F |
| 450 | 4 | 44 | 3.5 | 708 | 2 | 2 | 2 | 2 | --- | --- | F |
| 451 | 4 | 44 | 4.3 | 821 | 2 | 2 | 2 | 2 | --- | --- | F |
| 470 | 4 | 44 | 4.7 | 865 | 5 | 5 | - | - | --- | --- | F |
| 491 | 4 | 44 | 3.8 | 311 | 2 | 2 | 2 | 2 | --- | --- | F |
| 510 | 4 | 44 | 4.0 | 224 | 5 | 5 | - | - | --- | --- | F |
| 604 | 4 | 44 | 4.5 | 595 | 3 | 3 | 3 | 3 | --- | --- | F |
| 662 | 4 | 44 | 4.6 | 33 | 5 | 5 | - | - | --- | --- | F |
| 45 | 6 | 129 | 4.6 | 275 | 3 | 3 | 3 | 3 | --- | --- | F |
| 75 | 6 | 129 | 4.5 | 116 | 3 | 3 | 3 | 3 | --- | --- | F |
| 108 | 6 | 129 | 4.7 | 125 | 2 | 1 | 2 | 1 | --- | 1.0 | F |
| 120 | 6 | 129 | 4.9 | 342 | 1 | 1 | 1 | 1 | 0.8 | -0.2 | F |
| 129 | 6 | 129 | 4.8 | 0 | 1 | 1 | 1 | 1 | 6.6 | 0.7 | F |
| 225 | 6 | 129 | 3.5 | 412 | 2 | 2 | 2 | 2 | --- | --- | F |
| 302 | 6 | 129 | 3.2 | 729 | - | 2 | 2 | 2 | --- | --- | F |
| 309 | 6 | 129 | 3.4 | 198 | 2 | 2 | 2 | 2 | --- | --- | F |
| 317 | 6 | 129 | 3.8 | 113 | 2 | 2 | 2 | 2 | --- | --- | F |
| 319 | 6 | 129 | 3.5 | 146 | 2 | 2 | 2 | 2 | --- | --- | F |
| 320 | 6 | 129 | 3.9 | 41 | 2 | 1 | 2 | 1 | --- | -3.3 | F |
| 470 | 6 | 129 | 4.7 | 673 | 3 | 3 | 3 | 3 | --- | --- | F |

TABLE IV-6
RESULTS OF REFERENCE WAVEFORM FILTERING
(PAGE 4 OF 4)

| EVENT | STA | RWF | mb | RWF/TEST EV SEP | DETECTION | | | | SNNR IMPROVEMENT (dB) | | TYPE |
|-------|-----|-----|-----|--------------------|-----------|----|-----|----|-----------------------------|------|------|
| | | | | | BP | | RWF | | LR | LQ | |
| | | | | | LR | LQ | LR | LQ | | | |
| 6 | 4 | 449 | 5.2 | 537 | 1 | 1 | 1 | 1 | 3.7 | 1.4 | F |
| 21 | 4 | 449 | 4.7 | 932 | 2 | 2 | 2 | 2 | --- | --- | F |
| 44 | 4 | 449 | 5.4 | 508 | 1 | 1 | 1 | 1 | 4.7 | 5.0 | F |
| 45 | 4 | 449 | 4.6 | 597 | 3 | 3 | 3 | 3 | --- | --- | F |
| 108 | 4 | 449 | 4.7 | 345 | 2 | 2 | 2 | 2 | --- | --- | F |
| 120 | 4 | 449 | 4.9 | 604 | 5 | 5 | - | - | --- | --- | F |
| 302 | 4 | 449 | 3.2 | 842 | 2 | 2 | 2 | 2 | --- | --- | F |
| 309 | 4 | 449 | 3.4 | 519 | 2 | 2 | 2 | 2 | --- | --- | F |
| 449 | 4 | 449 | 4.6 | 0 | 1 | 1 | 1 | 1 | 9.2 | 1.9 | F |
| 450 | 4 | 449 | 3.5 | 395 | 2 | 2 | 2 | 2 | --- | --- | F |
| 451 | 4 | 449 | 4.3 | 554 | 2 | 2 | 2 | 2 | --- | --- | F |
| 470 | 4 | 449 | 4.7 | 614 | 5 | 5 | - | - | --- | --- | F |
| 491 | 4 | 449 | 3.8 | 306 | 2 | 2 | 2 | 1 | --- | --- | F |
| 510 | 4 | 449 | 4.0 | 709 | 5 | 5 | - | - | --- | --- | F |
| 604 | 4 | 449 | 4.5 | 842 | 2 | 2 | 6 | 6 | --- | --- | F |
| 662 | 4 | 449 | 4.6 | 539 | 5 | 5 | - | - | --- | --- | F |
| 339 | 8 | 797 | 5.5 | 7 | 5 | 5 | - | - | --- | --- | X |
| 456 | 8 | 797 | 4.4 | 13 | 3 | 3 | 3 | 3 | --- | --- | X |
| 626 | 8 | 797 | 5.2 | 0 | 3 | 3 | 3 | 3 | --- | --- | X |
| 652 | 8 | 797 | 5.7 | 3330 | 1 | 1 | 1 | 1 | 1.9 | -2.3 | X |
| 672 | 2 | 797 | 5.5 | 31 | 2 | 2 | 6 | 1 | --- | --- | X |
| 672 | 8 | 797 | 5.5 | 31 | 3 | 3 | 3 | 3 | --- | --- | X |
| 679 | 2 | 797 | 6.3 | 2837 | 1 | 1 | 1 | 1 | 1.3 | 0.7 | X |
| 679 | 8 | 797 | 6.3 | 2837 | 1 | 1 | 1 | 1 | 8.1 | -6.4 | X |
| 797 | 2 | 797 | 5.7 | 0 | 1 | 1 | 1 | 1 | 8.9 | 4.8 | X |
| 797 | 8 | 797 | 5.7 | 0 | 1 | 1 | 1 | 1 | 10.4 | 1.1 | X |

The effect of distance between reference waveform event and the test event on the SNNR improvement is shown in Figure IV-21, where SNNR improvement in dB is plotted against reference waveform-test event separation. We expect the SNNR improvement to decrease with increasing separation between reference waveform and test event. A general trend of -3dB per 1000 km was observed for ALPA data (Strauss, 1973). A least-means-square-error straight-line fitted to these data and the 95% confidence limits are shown in Figure IV-21. A slope of -3dB per 1000 km was obtained and corresponds to that for ALPA data.

Chirp filters were applied to 84 earthquake station-events and 24 presumed explosion station-events. Table IV-7 presents the results of the application of these chirp filters. The overall average SNNR improvements for the chirp filters are:

| | IMPROVEMENT (dB) | |
|--------------------|------------------|------|
| | RAYLEIGH | LOVE |
| EARTHQUAKE | 3.5 | 2.6 |
| PRESUMED EXPLOSION | 3.7 | 3.5 |

Thus, for chirp filters, the Rayleigh wave SNNR improvements were slightly better than the Love wave SNNR improvements for earthquake data and about the same for presumed explosion data.

The chirp length data is summarized in Figures IV-22 and IV-23 for the transverse and vertical components respectively. The chirp lengths plotted are those chirp lengths which give the best improvements. The corresponding distances are great circle distances in kilometers between event epicenter and station. The chirp lengths applied to presumed explosions are indicated by open circles while those applied to earthquakes are indicated by dots. A least-mean-square-error fit was made for the data points of each plot.

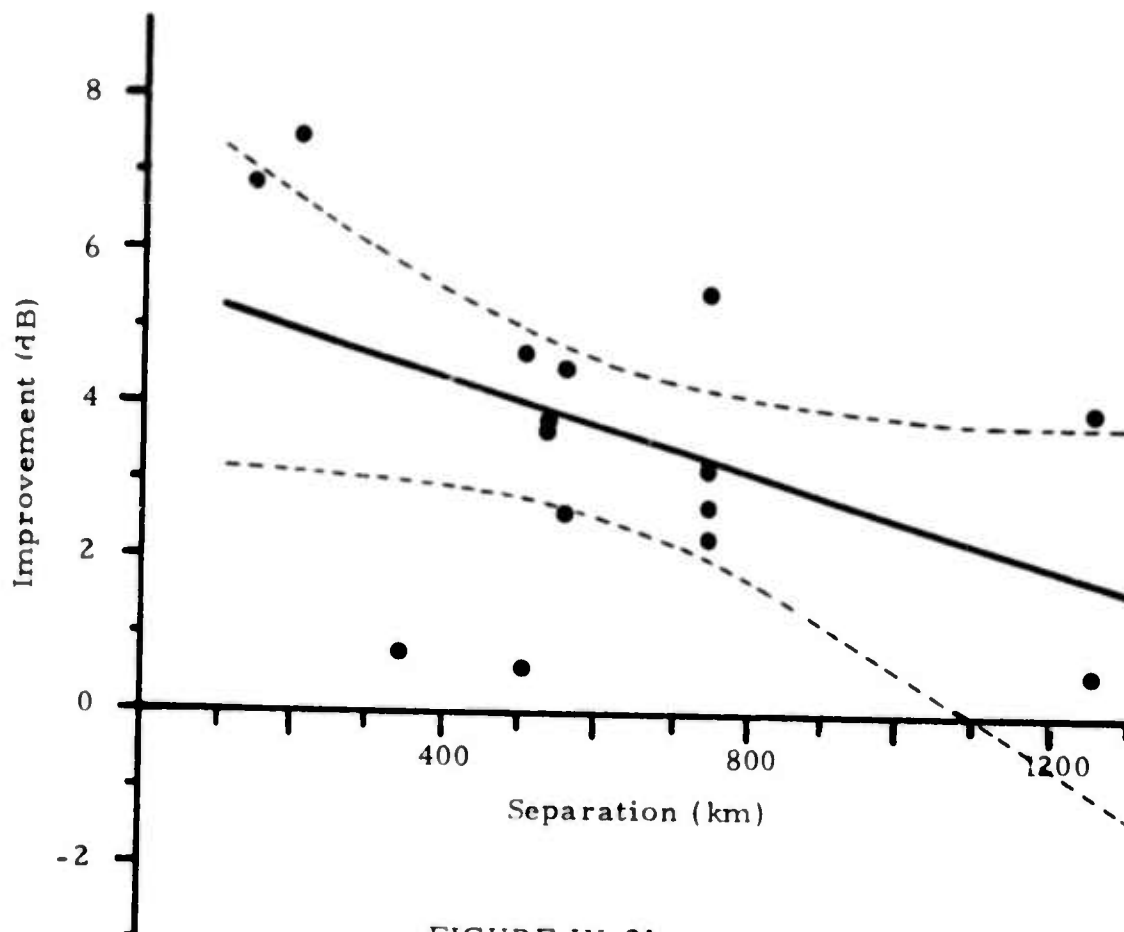


FIGURE IV-21
REFERENCE WAVEFORM FILTER IMPROVEMENT VERSUS
REFERENCE WAVEFORM/TEST EVENT SEPARATION
(VERTICAL COMPONENT)

TABLE IV-7
RESULTS OF CHIRP FILTERING
(PAGE 1 OF 5)

| (PAGE 1 OF 5) | | | | | | | | | | | | |
|---------------|-----|----------------|-------|-----------|----|-------|----|-------------|-----|---------|------|------|
| EVENT | STA | m _b | DELTA | DETECTION | | | | SNNR | | OPTIMUM | | TYPE |
| | | | | BP | | CHIRP | | IMPROVEMENT | | CHIRP | | |
| | | | | LR | LQ | LR | LQ | LR | LQ | LR | LQ | |
| 5 | 2 | 5.2 | 2091 | 1 | 1 | 1 | 1 | 0.9 | 0.6 | 100 | 100 | F |
| 6 | 2 | 5.2 | 7106 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 6 | 4 | 5.2 | 7216 | 1 | 1 | 1 | 1 | 3.7 | 2.5 | 300 | 200 | F |
| 6 | 7 | 5.2 | 10496 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 21 | 2 | 4.7 | 3504 | 1 | 1 | 1 | 1 | 3.6 | 1.7 | 300 | 400 | F |
| 21 | 3 | 4.7 | 7746 | 2 | 2 | 1 | 1 | --- | --- | 400 | --- | F |
| 21 | 4 | 4.7 | 6251 | 2 | 2 | 1 | 1 | --- | --- | 500 | --- | F |
| 21 | 7 | 4.7 | 10315 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 44 | 2 | 5.4 | 3160 | 1 | 1 | 1 | 1 | 1.7 | 0.9 | 300 | 500 | F |
| 44 | 2 | 5.4 | 7568 | 1 | 1 | 1 | 1 | 3.1 | 5.5 | 700 | 1100 | F |
| 44 | 4 | 5.4 | 6653 | 1 | 1 | 1 | 1 | 5.2 | 2.2 | 1000 | 400 | F |
| 44 | 7 | 5.4 | 10463 | 1 | 1 | 1 | 1 | 7.1 | 7.4 | 500 | 300 | F |
| 45 | 2 | 4.6 | 2020 | 3 | 3 | 2 | 6 | --- | --- | --- | 300 | F |
| 45 | 3 | 4.6 | 7692 | 2 | 3 | 3 | 3 | --- | --- | --- | --- | F |
| 45 | 4 | 4.6 | 5885 | 3 | 3 | 6 | 6 | --- | --- | 500 | 500 | F |
| 45 | 6 | 4.6 | 5247 | 3 | 3 | 1 | 1 | --- | --- | 1300 | 1200 | F |
| 45 | 7 | 4.6 | 10695 | 3 | 3 | 3 | 6 | --- | --- | --- | 200 | F |
| 75 | 2 | 4.5 | 2959 | 2 | 2 | 1 | 6 | --- | --- | 100 | 100 | F |
| 75 | 3 | 4.5 | 7492 | 2 | 2 | 1 | 2 | --- | --- | 700 | --- | F |
| 75 | 4 | 4.5 | 6012 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 75 | 6 | 4.5 | 5204 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | F |
| 75 | 7 | 4.5 | 10577 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 108 | 2 | 4.7 | 7385 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 108 | 4 | 4.7 | 6926 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 108 | 6 | 4.7 | 5181 | 2 | 1 | 2 | 1 | --- | --- | --- | --- | F |
| 108 | 7 | 4.7 | 10513 | 2 | 2 | 2 | 2 | --- | 3.9 | --- | 1300 | F |
| 120 | 2 | 4.9 | 7700 | 1 | 1 | 1 | 1 | 4.5 | 2.6 | 700 | 700 | F |

TABLE IV-7
RESULTS OF CHIRP FILTERING
(PAGE 2 OF 5)

| EVENT | STA | m _b | DELTA | DETECTION | | | | SNNR | | IMPROVEMENT | | OPTIMUM CHIRP LENGTH | | TYPE |
|-------|-----|----------------|-------|-----------|----|-------|----|------|-----|-------------|------|----------------------|------|------|
| | | | | BP | | CHIRP | | (dB) | | LR | | LQ | | |
| | | | | LR | LQ | LR | LQ | LR | LQ | LR | LQ | LR | LQ | |
| 120 | 4 | 4.9 | 6663 | 5 | 5 | - | - | --- | --- | --- | --- | --- | --- | F |
| 120 | 6 | 4.9 | 5057 | 1 | 1 | 1 | 1 | 2.0 | 1.8 | 1100 | 1100 | 1100 | 1100 | F |
| 129 | 3 | 4.8 | 7419 | 1 | 1 | 1 | 1 | 5.7 | 5.0 | 1000 | 1000 | 1000 | 1000 | F |
| 129 | 6 | 4.8 | 5090 | 1 | 1 | 1 | 1 | 3.5 | 0.4 | 1200 | 1200 | 1200 | 1200 | F |
| 129 | 7 | 4.8 | 10464 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | --- | --- | F |
| 225 | 3 | 3.5 | 7411 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | --- | --- | F |
| 225 | 6 | 3.5 | 4723 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | --- | --- | F |
| 225 | 7 | 3.5 | 10196 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | --- | --- | F |
| 235 | 3 | 4.5 | 7616 | 1 | 1 | 1 | 1 | --- | --- | --- | --- | --- | --- | F |
| 235 | 7 | 4.5 | 10624 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | --- | --- | F |
| 236 | 3 | 4.4 | 7126 | 2 | 2 | 1 | 2 | --- | --- | 700 | --- | --- | --- | F |
| 236 | 7 | 4.4 | 10449 | 5 | 5 | - | - | --- | --- | --- | --- | --- | --- | F |
| 238 | - | 5.1 | 7859 | 2 | 2 | 1 | 4 | --- | --- | 900 | 1000 | 1000 | --- | F |
| 238 | 7 | 5.1 | 10576 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | --- | --- | F |
| 202 | 3 | 3.2 | 7724 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | --- | --- | F |
| 202 | 4 | 3.2 | 6206 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | --- | --- | F |
| 202 | 6 | 3.2 | 4663 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | --- | --- | F |
| 309 | 3 | 3.4 | 7516 | 2 | 2 | 2 | 6 | --- | --- | 1000 | --- | --- | --- | F |
| 200 | 4 | 3.4 | 6855 | 2 | 2 | 1 | 6 | --- | --- | 500 | 900 | 900 | --- | F |
| 209 | 6 | 3.4 | 5193 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | --- | --- | F |
| 217 | 1 | 3.8 | 9523 | 2 | 2 | 2 | 2 | --- | --- | 1000 | --- | --- | --- | F |
| 217 | 5 | 3.8 | 4443 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | --- | --- | F |
| 217 | 6 | 3.8 | 5137 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | --- | --- | F |
| 217 | 8 | 3.8 | 10634 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | --- | --- | F |
| 217 | 9 | 3.8 | 11394 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | --- | --- | F |
| 219 | 1 | 3.5 | 9451 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | --- | --- | F |
| 219 | 5 | 3.5 | 4369 | 5 | 5 | - | - | --- | --- | --- | --- | --- | --- | F |

TABLE IV-7
RESULTS OF CHIRP FILTERING
(PAGE 3 OF 5)

(PAGE 3 OF 5)

| EVENT | STA | mb | DELTA | DETECTION | | | | SNNR IMPROVEMENT | | OPTIMUM CHIRP | | TYPE |
|-------|-----|-----|-------|-----------|----|-------|----|------------------|------|---------------|------|------|
| | | | | BP | | CHIRP | | (dB) | | LENGTH | | |
| | | | | LR | LQ | LR | LQ | LR | LQ | LR | LQ | |
| 318 | 6 | 3.5 | 5000 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 319 | 8 | 3.5 | 10636 | 5 | 5 | - | - | --- | --- | --- | --- | F |
| 319 | 6 | 3.5 | 11204 | 5 | 5 | - | - | --- | --- | --- | --- | F |
| 320 | 1 | 3.0 | 9593 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 320 | 5 | 3.0 | 4360 | 5 | 5 | - | - | --- | --- | --- | --- | F |
| 320 | 4 | 3.0 | 5082 | 2 | 1 | 1 | 1 | --- | -2.0 | 1200 | 500 | F |
| 320 | 8 | 3.0 | 10702 | 5 | 5 | - | - | --- | --- | --- | --- | F |
| 320 | 6 | 3.0 | 11406 | 5 | 5 | - | - | --- | --- | --- | --- | F |
| 384 | 7 | 4.3 | 10407 | 1 | 1 | 1 | 1 | 2.4 | 3.4 | 200 | 200 | F |
| 384 | 8 | 4.3 | 11361 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 384 | 6 | 4.3 | 11661 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | F |
| 449 | 4 | 4.6 | 6686 | 1 | 1 | 1 | 1 | 6.7 | 1.8 | 900 | 400 | F |
| 449 | 5 | 4.6 | 4393 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | F |
| 449 | 8 | 4.6 | 10523 | 1 | 2 | 1 | 2 | -1.0 | --- | 1200 | --- | F |
| 450 | 4 | 3.5 | 7057 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 450 | 5 | 3.5 | 4776 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 450 | 8 | 3.5 | 10242 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 451 | 4 | 4.3 | 7210 | 2 | 2 | 1 | 2 | --- | --- | 1000 | --- | F |
| 451 | 5 | 4.3 | 4928 | 2 | 2 | 1 | 2 | --- | --- | 500 | --- | F |
| 451 | 8 | 4.3 | 10139 | 1 | 1 | 1 | 1 | 7.0 | 6.0 | 700 | 700 | F |
| 470 | 1 | 4.7 | 9166 | 1 | 1 | 1 | 1 | 6.4 | -1.1 | 800 | 1300 | F |
| 470 | 4 | 4.7 | 7269 | 5 | 5 | - | - | --- | --- | --- | --- | F |
| 470 | 5 | 4.7 | 4084 | 3 | 3 | 1 | 3 | --- | --- | 200 | --- | F |
| 470 | 8 | 4.7 | 5379 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | F |
| 470 | 4 | 4.7 | 10101 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | F |
| 491 | 1 | 3.8 | 9861 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 491 | 4 | 3.8 | 6549 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |

TABLE IV-7
RESULTS OF CHIRP FILTERING
(PAGE 4 OF 5)

(PAGE 4 OF 5)

| EVENT | STA | m _b | DELTA | DETECTION | | | | SNNR IMPROVEMENT | | OPTIMUM CHIRP | | TYPE |
|-------|-----|----------------|-------|-----------|----|-------|----|------------------|-----|---------------|-----|------|
| | | | | BP | | CHIRP | | (dB) | | LENGTH | | |
| | | | | LR | LQ | LR | LQ | LR | LQ | LR | LQ | |
| 491 | 5 | 3.8 | 4126 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 491 | 8 | 3.8 | 10828 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | E |
| 491 | 5 | 3.8 | 11317 | 5 | 5 | - | - | --- | --- | --- | --- | E |
| 510 | 1 | 4.0 | 9720 | 2 | 2 | 2 | 6 | --- | --- | --- | 700 | E |
| 510 | 4 | 4.0 | 6686 | 5 | 5 | - | - | --- | --- | --- | --- | F |
| 510 | 5 | 4.0 | 4005 | 2 | 2 | 1 | 2 | --- | --- | 300 | --- | F |
| 510 | 8 | 4.0 | 11173 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 510 | 9 | 4.0 | 11765 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | E |
| 536 | 1 | 4.3 | 9593 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | E |
| 536 | 5 | 4.3 | 4360 | 5 | 5 | - | - | --- | --- | --- | --- | F |
| 604 | 4 | 4.5 | 6206 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | F |
| 604 | 5 | 4.5 | 3605 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | E |
| 604 | 8 | 4.5 | 11348 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | F |
| 662 | 1 | 4.6 | 9624 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | F |
| 662 | 4 | 4.6 | 5781 | 5 | 5 | - | - | --- | --- | 500 | --- | F |
| 662 | 5 | 4.6 | 4182 | 2 | 2 | 1 | 2 | --- | --- | --- | --- | F |
| 662 | 9 | 4.6 | 10970 | 5 | 5 | - | - | --- | --- | --- | --- | F |
| 116 | 2 | 5.5 | 6505 | 2 | 2 | 1 | 2 | --- | --- | 900 | --- | X |
| 116 | 4 | 5.5 | 6273 | 5 | 5 | - | - | --- | --- | --- | --- | X |
| 116 | 6 | 5.5 | 4240 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | X |
| 260 | 3 | 5.5 | 5628 | 1 | 2 | 1 | 2 | 4.2 | --- | 900 | --- | X |
| 260 | 6 | 5.5 | 4292 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | X |
| 260 | 7 | 5.5 | 9526 | 2 | 2 | 2 | 2 | --- | --- | --- | 500 | X |
| 339 | 1 | 5.5 | 10217 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | X |
| 339 | 5 | 5.5 | 4288 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | X |
| 339 | 6 | 5.5 | 4318 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | X |
| 339 | 7 | 5.5 | 9551 | 2 | 2 | 1 | 2 | --- | --- | 200 | --- | X |

TABLE IV-7
RESULTS OF CHIRP FILTERING
(PAGE 5 OF 5)

| EVENT | STA | m _b | DELTA | DETECTION | | | | SNNR | | OPTIMUM | | TYPE |
|-------|-----|----------------|-------|-----------|----|-------|----|-------------|-----|---------|------|------|
| | | | | BP | | CHIRP | | IMPROVEMENT | | CHIRP | | |
| | | | | LR | LQ | LR | LQ | LR | LQ | LR | LQ | |
| 330 | 8 | 5.5 | 10341 | 2 | 5 | 6 | 5 | --- | --- | 1200 | --- | X |
| 339 | 5 | 5.5 | 10562 | 5 | 5 | - | - | --- | --- | --- | --- | X |
| 450 | 4 | 4.4 | 6227 | 2 | 2 | 1 | 2 | --- | --- | 800 | --- | X |
| 456 | 5 | 4.4 | 4271 | 3 | 3 | 3 | 3 | --- | --- | --- | --- | X |
| 456 | 8 | 4.4 | 10379 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | X |
| 626 | 1 | 5.2 | 10224 | 2 | 2 | 2 | 6 | --- | --- | --- | --- | X |
| 626 | 4 | 5.2 | 6229 | 1 | 2 | 1 | 2 | 0.3 | --- | 600 | --- | X |
| 626 | 5 | 5.2 | 4281 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | X |
| 626 | 9 | 5.2 | 10346 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | X |
| 652 | 1 | 5.7 | 12265 | 5 | 5 | - | - | --- | --- | --- | --- | X |
| 652 | 4 | 5.7 | 4181 | 5 | 5 | - | - | --- | --- | --- | --- | X |
| 652 | 5 | 5.7 | 2524 | 5 | 5 | - | - | --- | --- | --- | --- | X |
| 652 | 8 | 5.7 | 11709 | 5 | 5 | - | - | --- | --- | --- | --- | X |
| 672 | 2 | 5.5 | 3939 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | X |
| 672 | 4 | 5.5 | 6201 | 5 | 5 | - | - | --- | --- | --- | --- | X |
| 672 | 5 | 5.5 | 4266 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | X |
| 672 | 8 | 5.5 | 10349 | 2 | 2 | 2 | 2 | --- | --- | --- | --- | X |
| 679 | 2 | 6.3 | 6626 | 1 | 1 | 1 | 1 | 2.3 | 2.5 | 200 | 400 | X |
| 679 | 4 | 6.3 | 4813 | 1 | 1 | 1 | 1 | 4.7 | 2.5 | 400 | 400 | X |
| 679 | 5 | 6.3 | 5025 | 1 | 1 | 1 | 1 | 4.5 | 4.6 | 500 | 500 | X |
| 679 | 8 | 6.3 | 9188 | 1 | 1 | 1 | 1 | 5.9 | 4.4 | 1100 | 1200 | X |

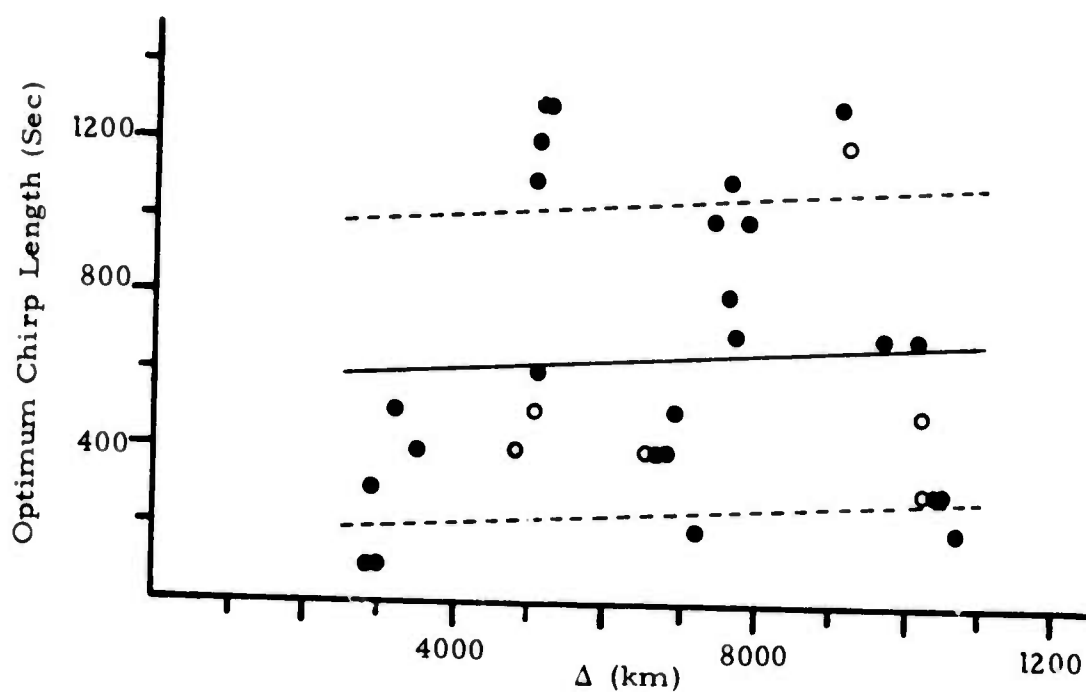


FIGURE IV-22
CHIRP FILTER LENGTH VERSUS DISTANCE
(TRANSVERSE COMPONENT)

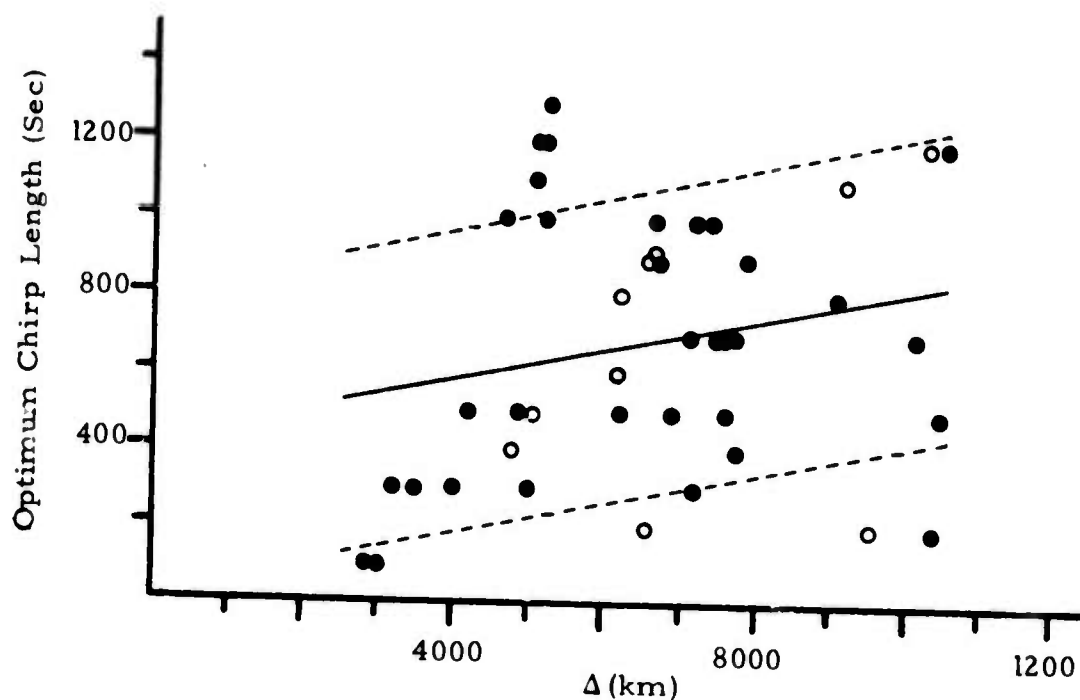


FIGURE IV-23
CHIRP FILTER LENGTH VERSUS DISTANCE
(VERTICAL COMPONENT)
IV-51

The scatter in the plotted data is so great that little can be deduced from the plots. In order to ensure that the optimum chirp length will be used at least 70% of the time, it will be necessary to use 9 chirps each 100 seconds longer than the previous and centered about the least-square-error fit (Heiting et al, 1972). Therefore, in future work, at least this many chirps will be used.

5. Improvements in Surface-Wave Detection

Figures IV-24, 25, 26, and 27 illustrate the improvement in surface-wave detection made possible by application of matched filters. The first three show detection improvements of station-events; the fourth figure shows detection improvements of the network (i. e. detection by any one of the matched filters is considered as a detection of that event, presumed explosion or earthquake).

The percent detection levels to be discussed but not shown in the figures, are maximum likelihood estimates and are subject to large errors due to the small population considered.

The notch in the detection plots at $m_b = 5.1$ is an earthquake with a depth of 130 km and relatively low surface-wave excitation.

With this in mind, the following points also should be considered when viewing these figures:

Figure IV-24: Reference Waveform Filter Versus Bandpass Filter

The 50 percent detection level for the bandpass filter is $m_b = 5.00 \pm 0.65$. The 50 percent detection level for the reference waveform filter is 4.34 ± 0.62 . Reference waveform filters detected 63 percent of the station-event pairs and bandpass filters detected 28 percent.

Figure IV-25: Chirp Filter Versus Bandpass Filter

The 50 percent detection level for the bandpass filter

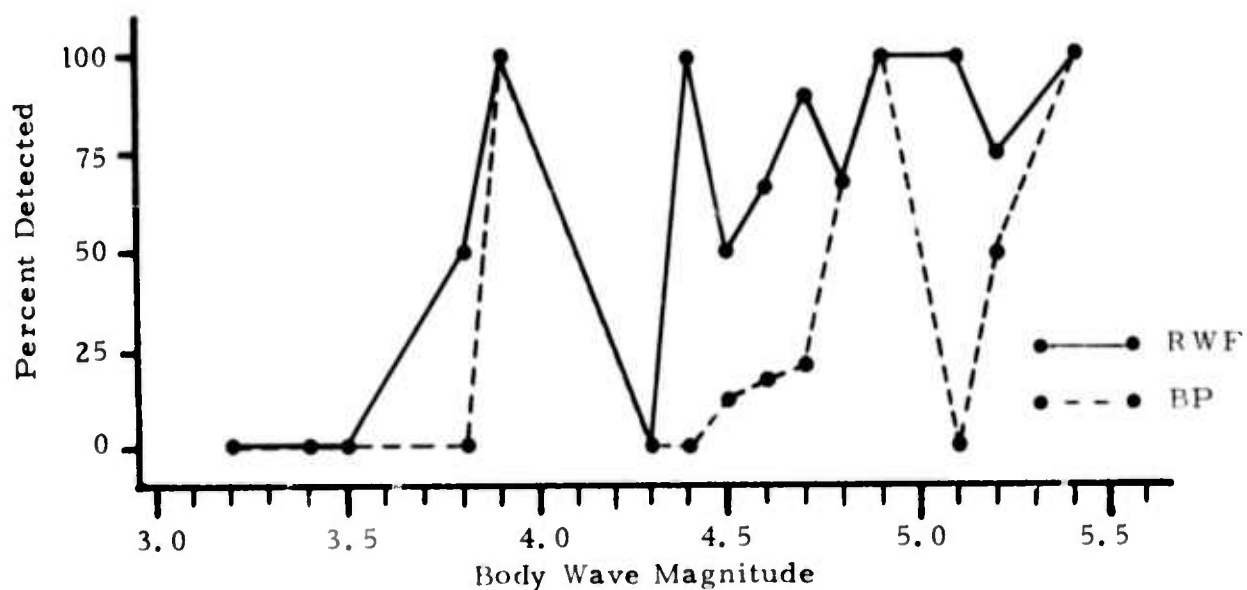
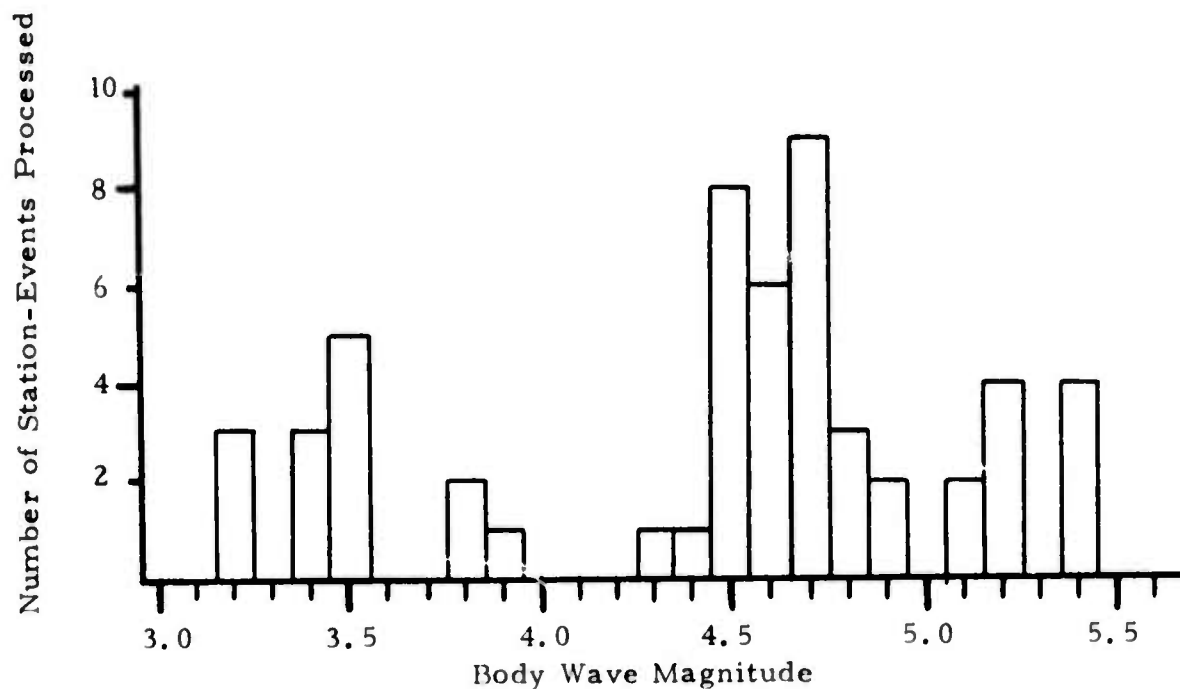


FIGURE IV-24
SURFACE WAVE DETECTION DATA FOR
REFERENCE WAVEFORM FILTER VERSUS BANDPASS FILTER

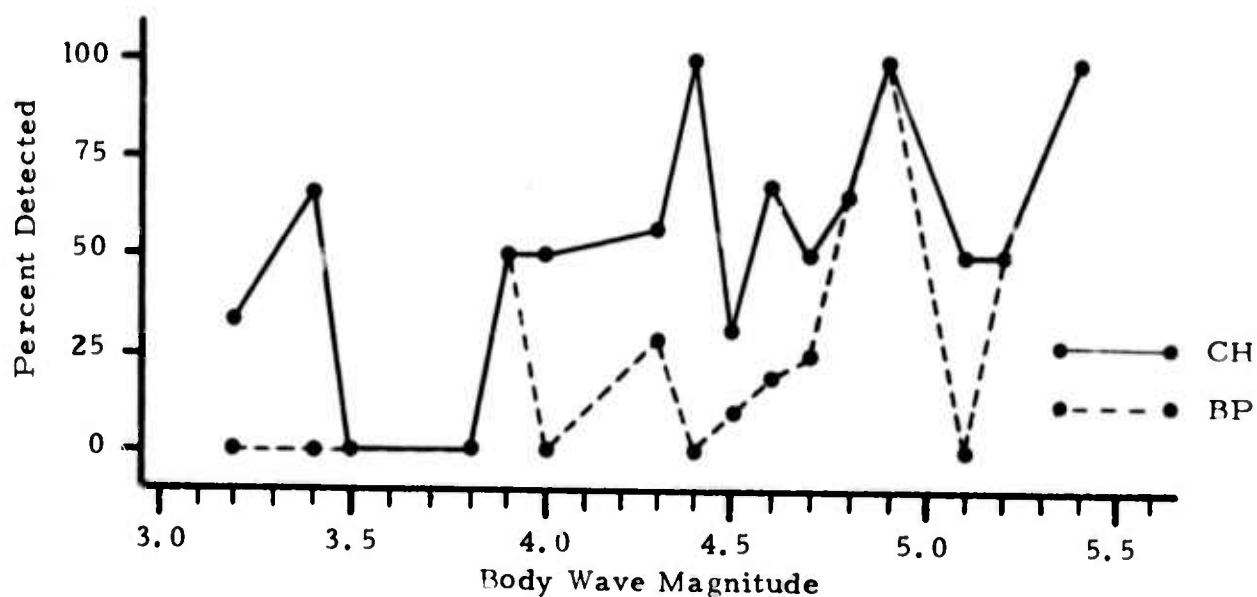
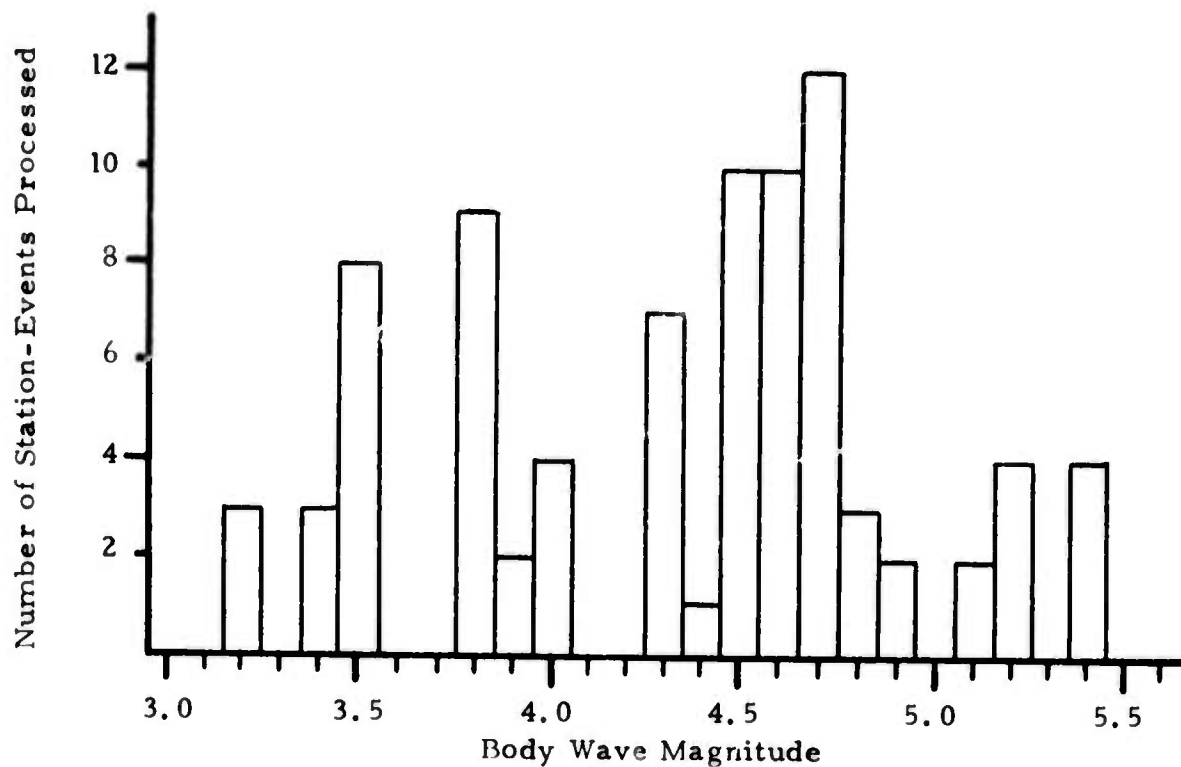


FIGURE IV-25
SURFACE WAVE DETECTION DATA FOR
CHIRP FILTER VERSUS BANDPASS FILTER

is $m_b = 4.99 \pm 0.63$. The 50 percent level for the chirp filter is $m_b = 4.46 \pm 0.08$. Chirp filters detected 44 percent of the station-event pairs and bandpass filters detected 23 percent.

Figure IV-26: Combined Reference Waveform and Chirp Filters Versus Bandpass Filters

A station-event is considered as a detection if either reference waveform or chirp filter yielded a detection. The 50 percent detection level for the bandpass filter is $m_b = 4.99 \pm 0.63$. The 50 percent detection level for combined matched filters is $m_b = 4.17 \pm 0.78$. Matched filters detected 56 percent of the station-event pairs and bandpass filters detected 23 percent.

Figure IV-27: Network Matched Filter Versus Network Bandpass Filter

An event is considered detected when one or more stations detects with either of the matched filters and similarly for the bandpass filter. The 50 percent level for bandpass filter is $m_b = 4.47 \pm 0.63$. The 50 percent level for the matched filters is $m_b = 3.53$. Matched filters detected 82 percent of the events and bandpass filter 44 percent.

The results of the TCA processing are shown in Figure IV-28. The maximum likelihood estimate indicates that the TCA processor improved the 50 percent detection level from an $m_b = 4.74 \pm 0.57$ to an $m_b = 4.46 \pm 0.80$. Further, the TCA processor detected 44 percent of the station-event pairs as compared to 24 percent detected by the bandpass filter. The 50 percent detection level and percentages of station-events detected are comparable to the values determined for the chirp filter, Figure IV-25.

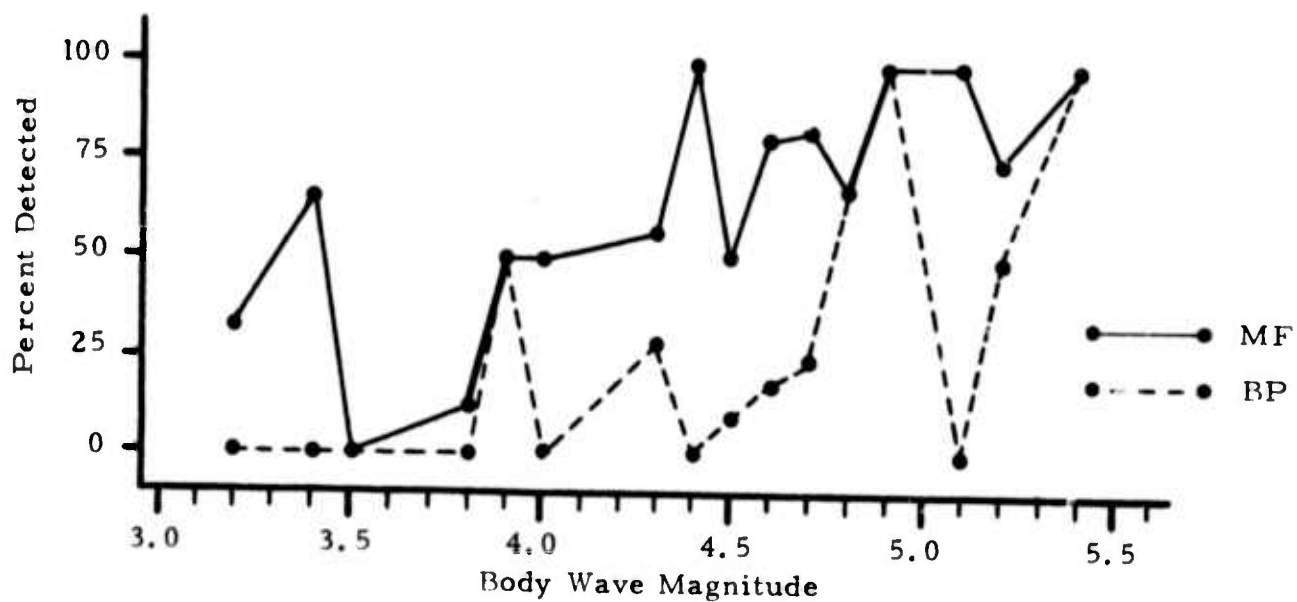
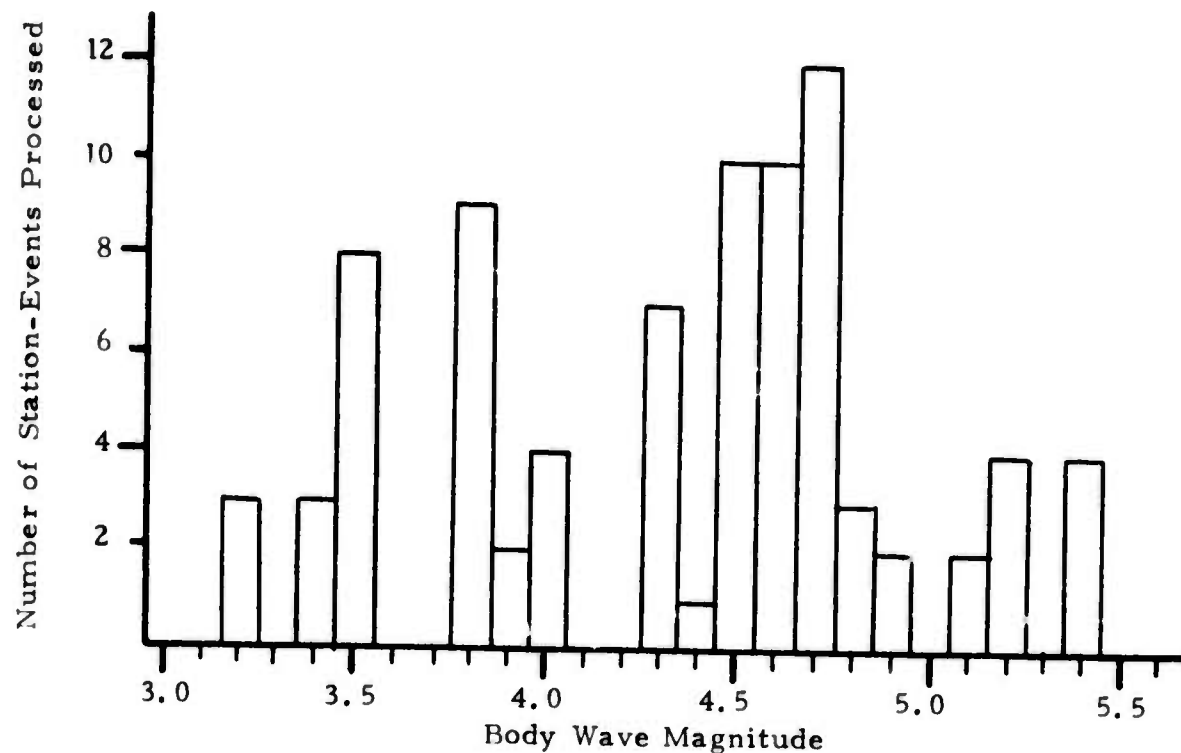


FIGURE IV-26
SURFACE WAVE DETECTION DATA FOR COMBINED
REFERENCE WAVEFORM AND CHIRP FILTERS VERSUS BANDPASS FILTER

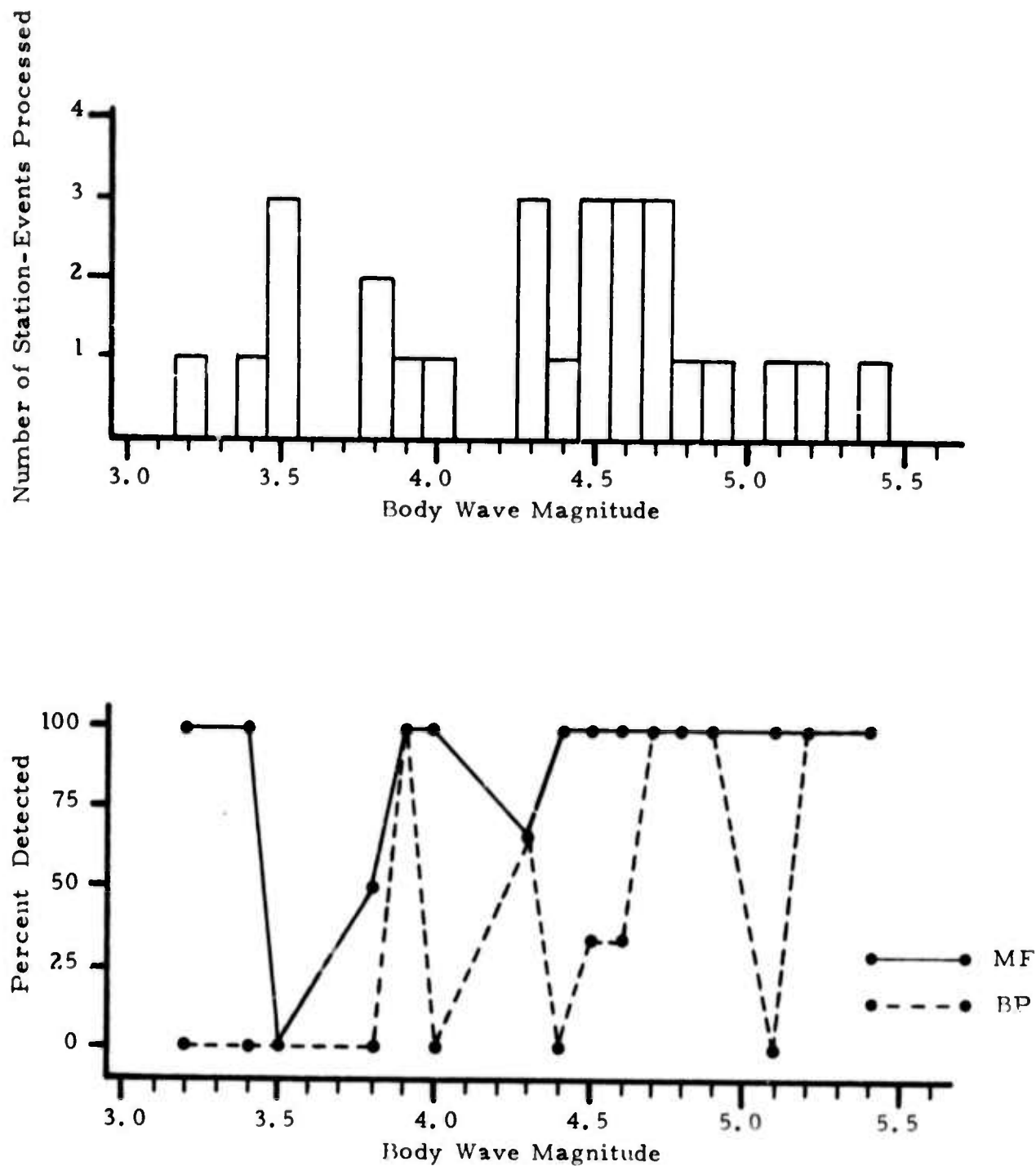


FIGURE IV-27
SURFACE WAVE DETECTION DATA FOR THE NETWORK
MATCHED FILTER VERSUS NETWORK BANDPASS FILTER

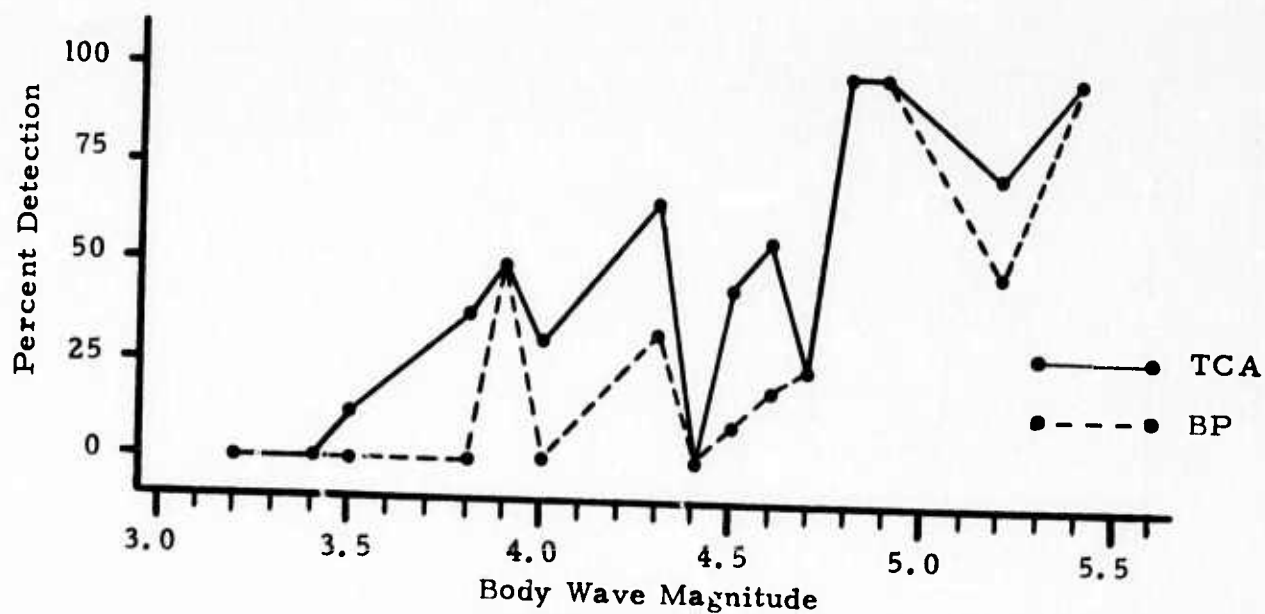
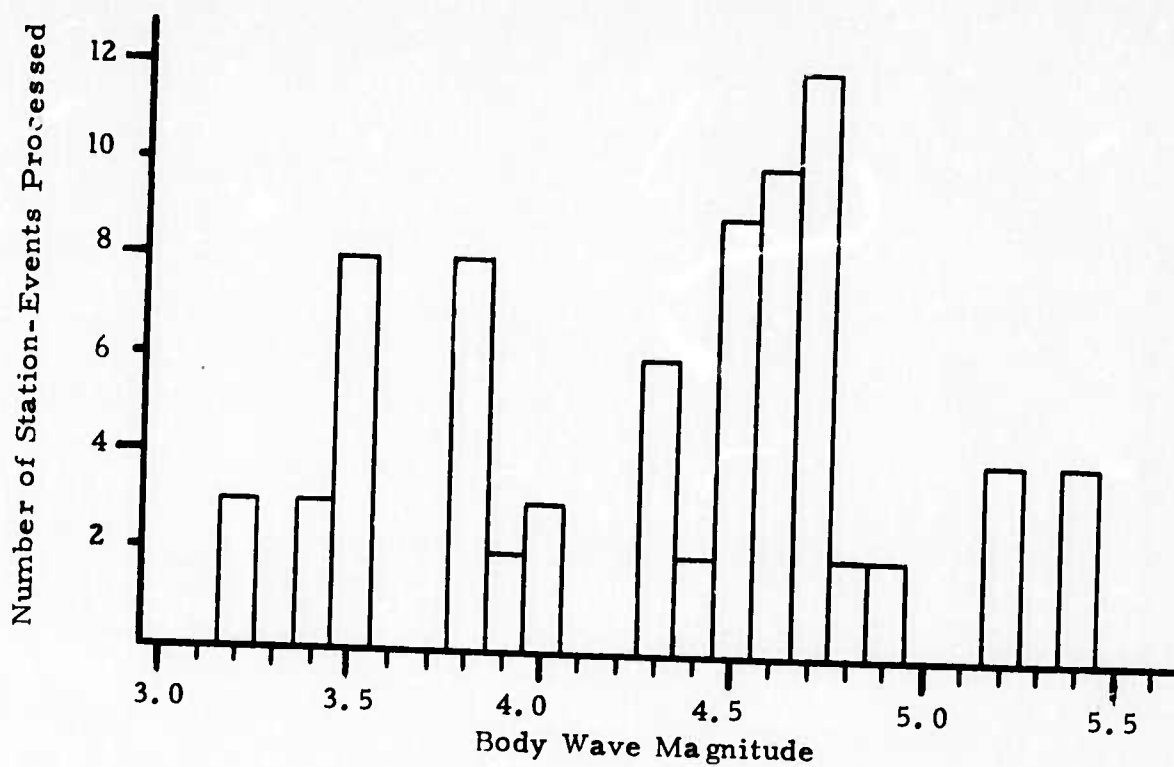


FIGURE IV-28
SURFACE WAVE DETECTION DATA FOR THE
TCA PROCESSOR VERSUS BANDPASS FILTER

IV-58

The large standard deviations given throughout this analysis are indicative of the small data base and this is obvious from the figures. Thus, little weight should be given to the reported 50 percent detection levels. However, the overall detection percentages show that about twice as many station-events or events are detected by any of the filters as compared to those detected by the bandpass filter.

6. Summary and Conclusions

The average SNNR improvements in dB for reference waveform and chirp filters are as follows:

| REFERENCE WAVEFORM FILTER | | RAYLEIGH | LOVE |
|------------------------------|------------------------|----------|------|
| | EARTHQUAKES | 3.5 | 0.1 |
| CHIRP FILTER | PRESUMED EXPLOSIONS | 3.8 | -2.7 |
| | EARTHQUAKES | 3.5 | 2.6 |
| | PRESUMED EXPLOSIONS | 3.7 | 3.5 |

Thus, reference waveform and chirp filters yielded essentially the same average SNNR dB improvements when matched with Rayleigh waves. When matched with Love waves, the chirp filters gave much higher SNNR dB improvement than did the reference waveform. This is primarily due to the difficulty of obtaining uncontaminated representative Love waves as filters. Therefore, in terms of overall average SNNR improvements the chirp filters perform better than the reference waveform filters for this ensemble of events.

Clearly, the application of matched filters to the VLPE does significantly improve detection as is evidenced by the factor of two increase in overall detections. However, the small data base precludes the determination of definite detection thresholds and comparisons with either the single VLPE stations and networks discussed in part B-3 or the SNNR dB improvements.

The preliminary analysis of the TCA processor yielded

detection results comparable to those for the chirp filter. In future studies, the SNNR gains will be determined for the TCA processor along with detection thresholds for various combinations of the TCA processor and matched filters on single stations and networks.

SECTION V

VLPE DISCRIMINATION CAPABILITY

A. INTRODUCTION

This section presents the capability of the single VLPE stations and the VLPE network to discriminate between presumed underground explosions and earthquakes located in Eurasia.

Lambert and Becker (1973) presented a preliminary evaluation of M_s versus m_b discrimination capabilities of VLPE single stations, the VLPE network, and the VLPE-ALPA-NORSAR network. The above report consisted of a data base comprised of 545 Eurasian events or the analysis of 2130 event-station pairs. The present report includes those data plus 329 Eurasian events or the analysis of 1447 additional event-station pairs.

In part B. of this section we discuss M_s versus m_b for single stations and the VLPE network. Part C. includes Love to Rayleigh wave amplitude ratios as a function of station, region, and network. Part D. presents preliminary radiation pattern results and discusses the capability of the VLPE to discern radiation patterns of surface waves detected at far field.

B. M_s (T = 20 SECONDS) VERSUS m_b

1. Single VLPE Stations

The surface wave magnitude (M_s) is defined as (Harley, 1972),

$$M_s = \log A/T + \log \Delta + 1.12$$

where M_s = surface wave magnitude.

A = peak-to-peak displacement in $m\mu$,

T = period in seconds for A,

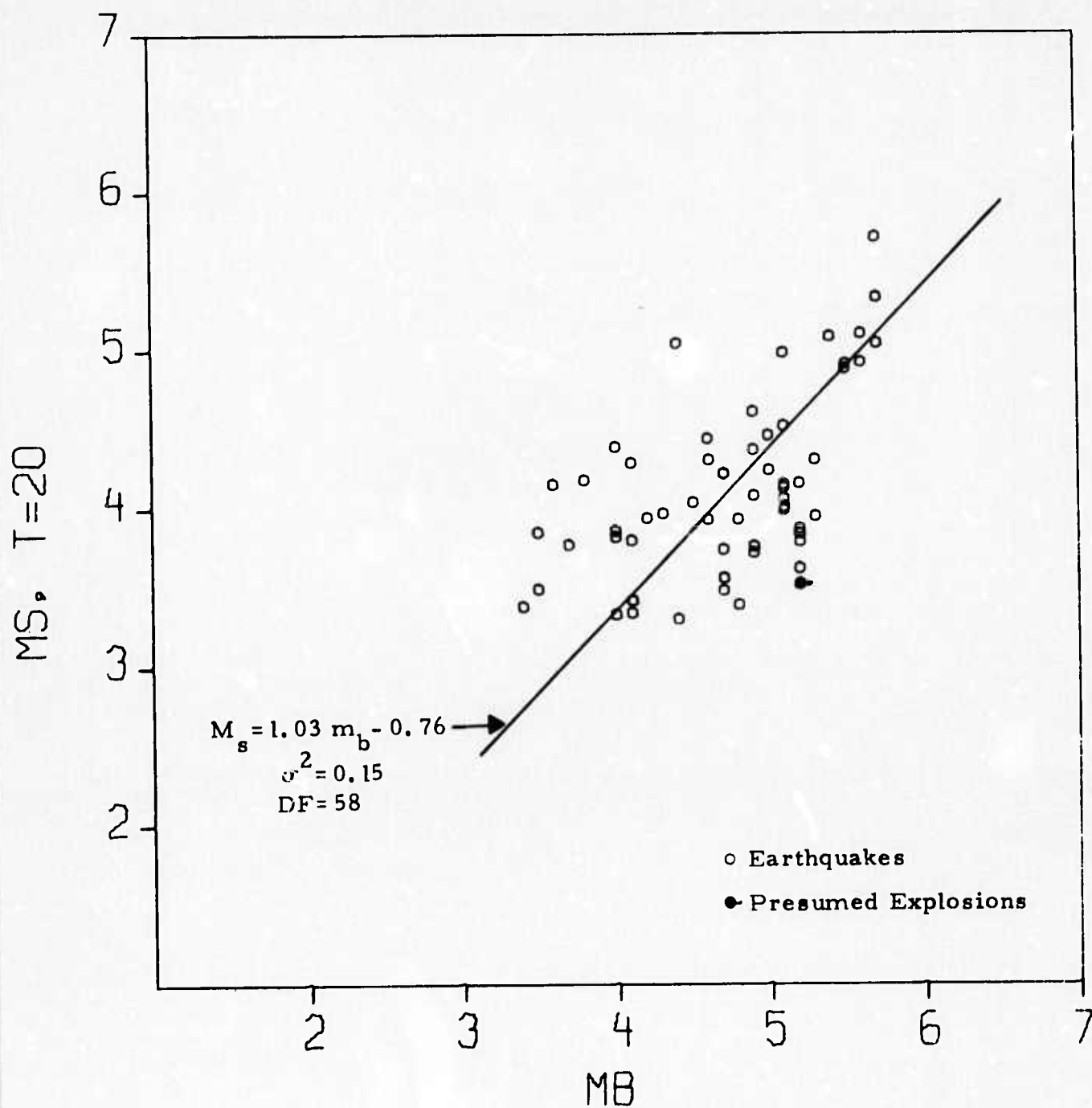
Δ = epicentral distance in degrees.

As previously indicated in II-B, all body wave magnitudes (m_b) were reviewed, where possible, and only teleseismic m_b determinations were considered as valid estimates.

Figures V-1 through V-11 show M_s ($T=20$ seconds) versus m_b for CTA, CHG, FBK, TLO, EIL, KON, OGD, KIP, ALQ, ZLP, and MAT. Further, best fit straight lines are shown for the $M_s :: m_b$ earthquake populations. Previously, the general trend for a population of M_s and m_b measurements has been determined by considering one magnitude as the independent variable and the other as the dependent variable. However, in this study we consider M_s and m_b to be independent of each other and determine a best linear fit by minimizing the distances normal to a line and the data points (Appendix V-A). These lines are shown on each figure in the form of $M_s = \beta m_b + a$, along with the variance σ^2 , and the degrees of freedom ($DF = n-2$; n = number of points).

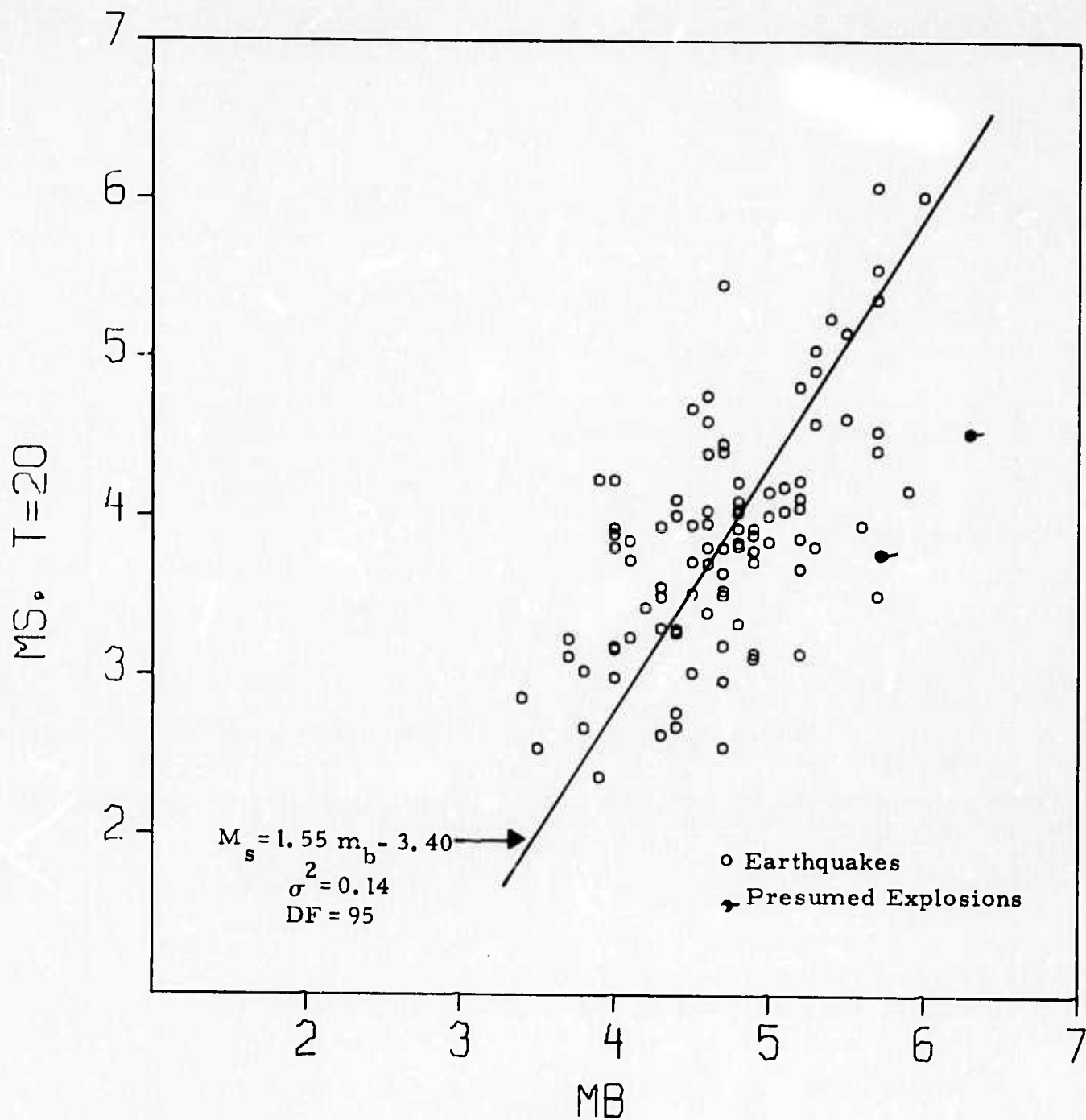
In determining the best linear fits to the data we have included all available data for each station. However, it is well known that event magnitudes are over estimated when they are near the detection threshold of any seismological station or network. Thus, the linear fits shown here should be considered as tentative estimations of the station response to Eurasian events. In addition to the above considerations, we have insufficient data available for stations ZLP and MAT (Figures V-10 and V-11).

In general, separation between earthquakes and presumed explosions is not distinct. However, Lambert and Becker (1973) showed that the variance (σ^2) for $M_s :: m_b$ data of events during January 1, 1972 through March 20, 1972 was significantly larger than for June 1, 1972 through July 31, 1972 data. They attributed this to erratic static gains and to the increase of noise for the winter months. Further, they found that many events located at about 30° N latitude and 50° E longitude are consistently misclassified.



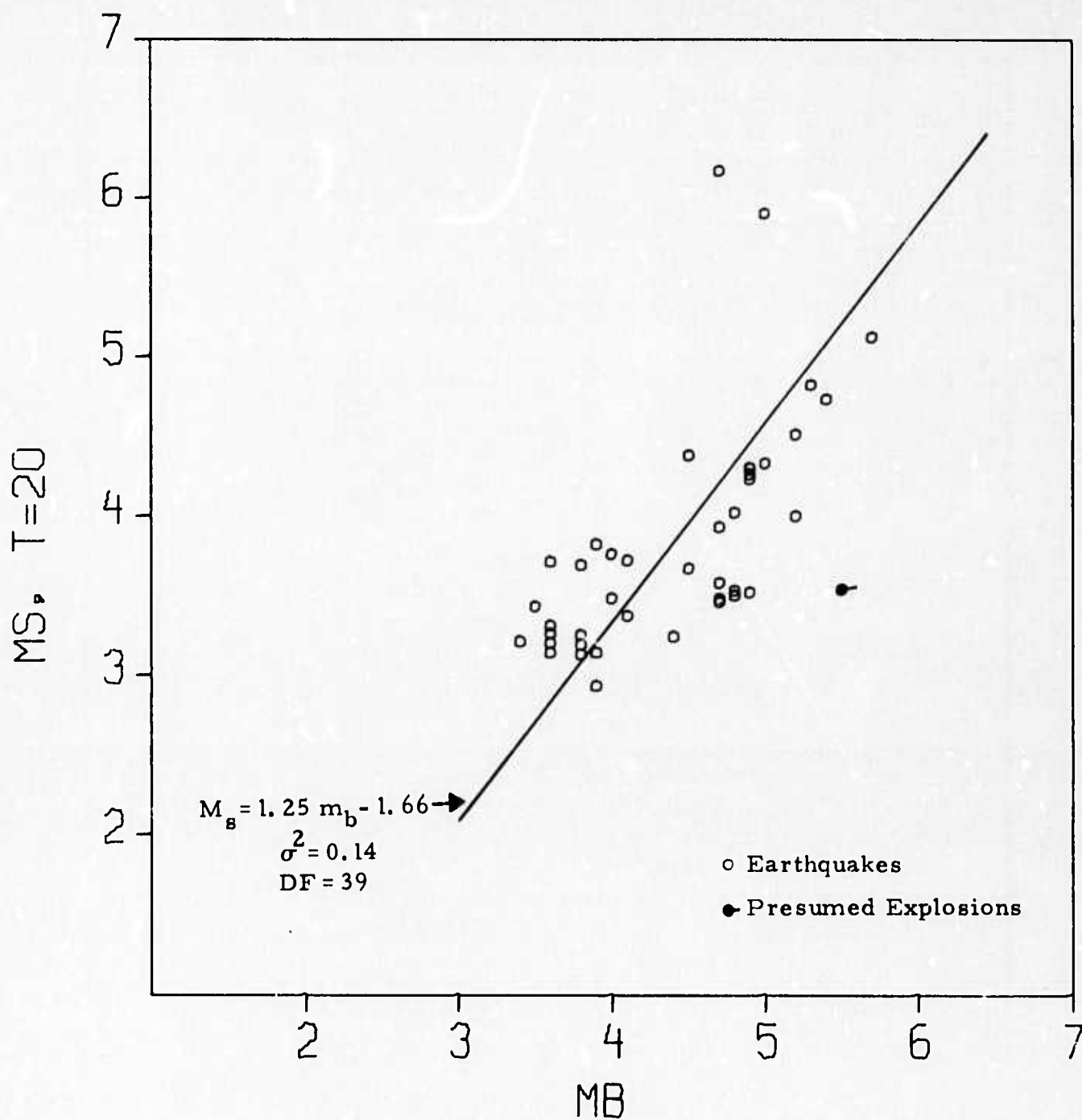
M_s VERSUS m_b AT
 CTA 06/01/72 - 12/31/72

FIGURE V-1



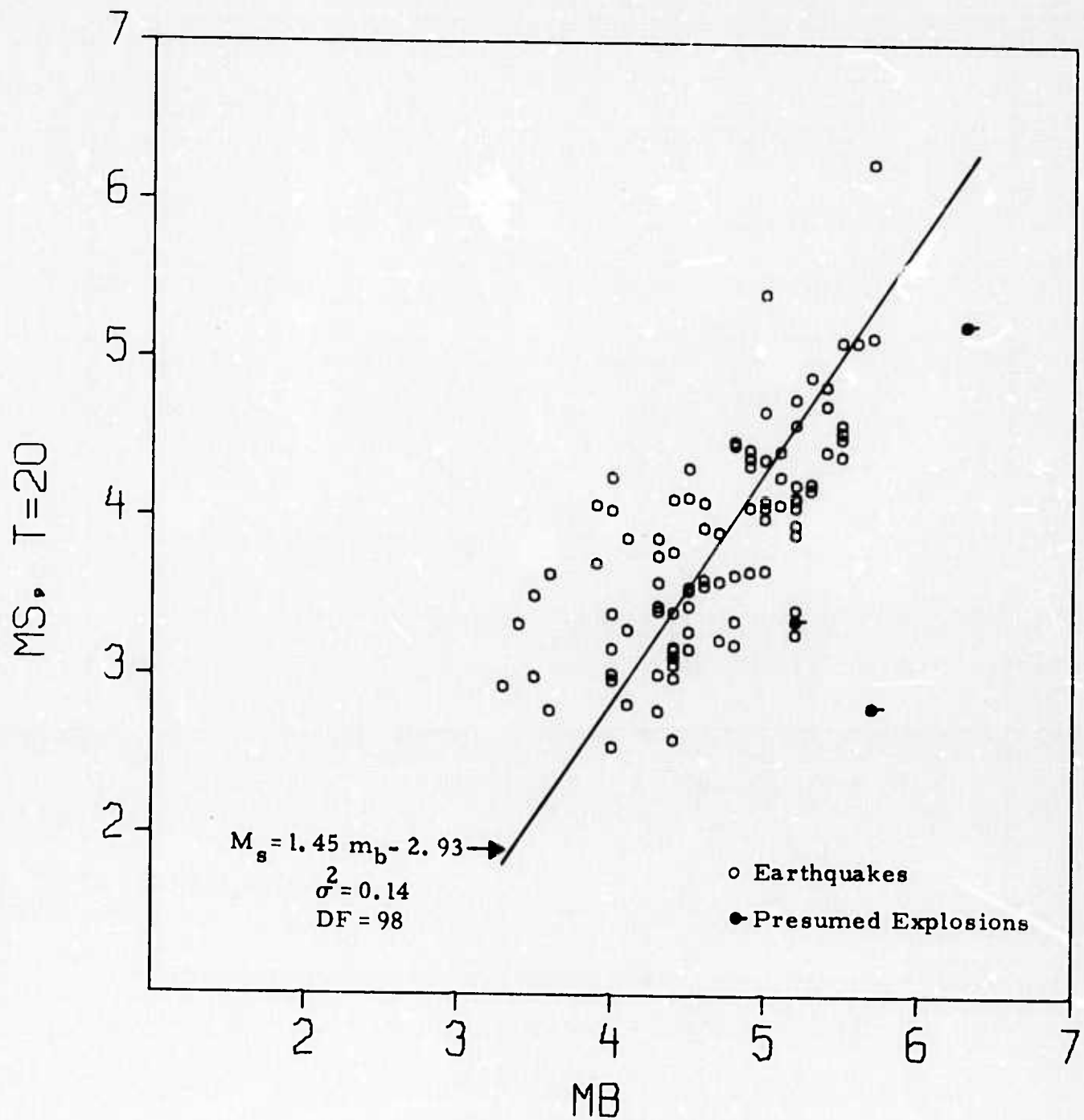
M_s VERSUS m_b AT
 CHG 01/01/72 - 12/31/72

FIGURE V-2



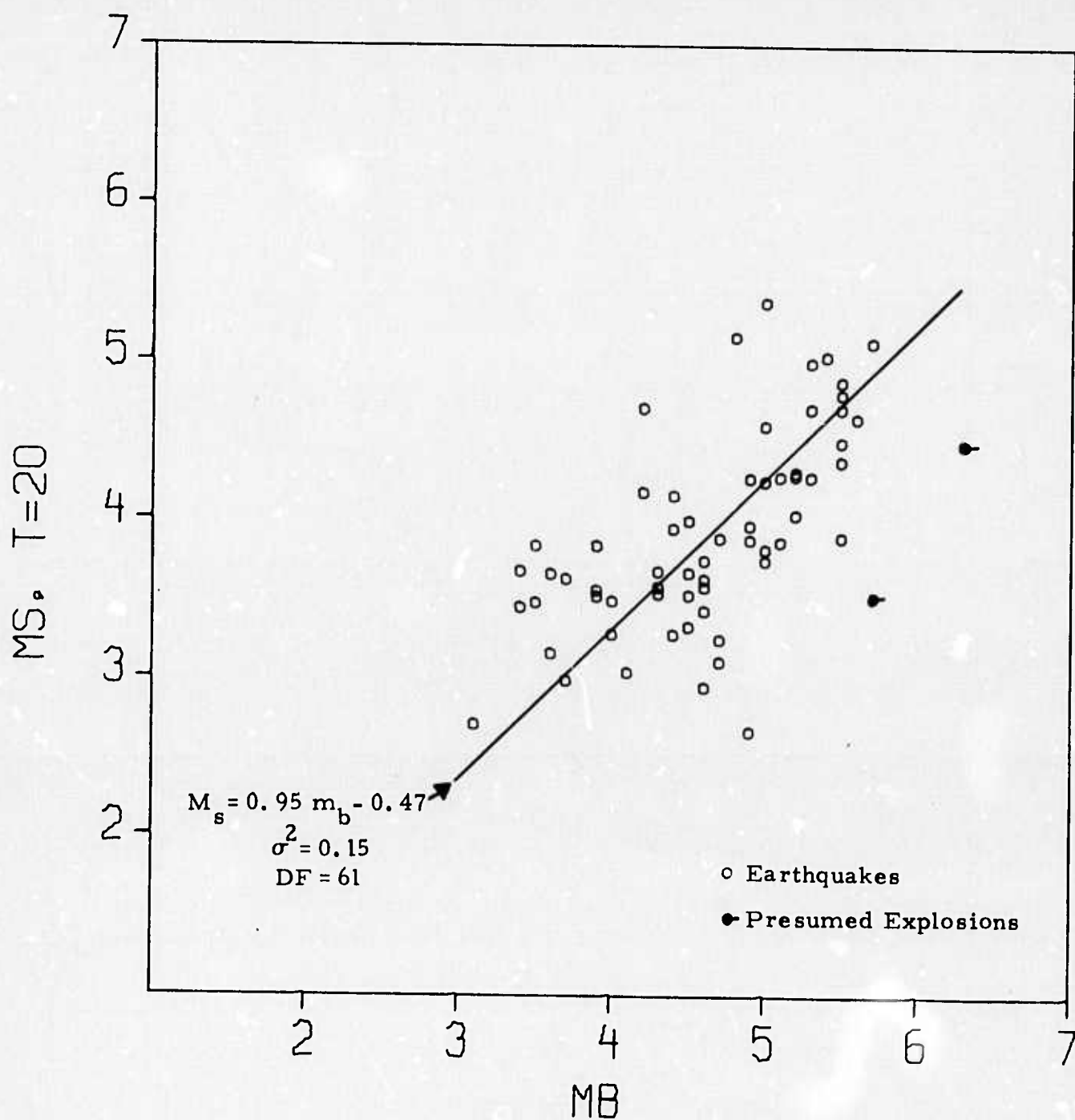
M_s VERSUS m_b AT
FBK 01/01/72 - 03/20/72

FIGURE V-3



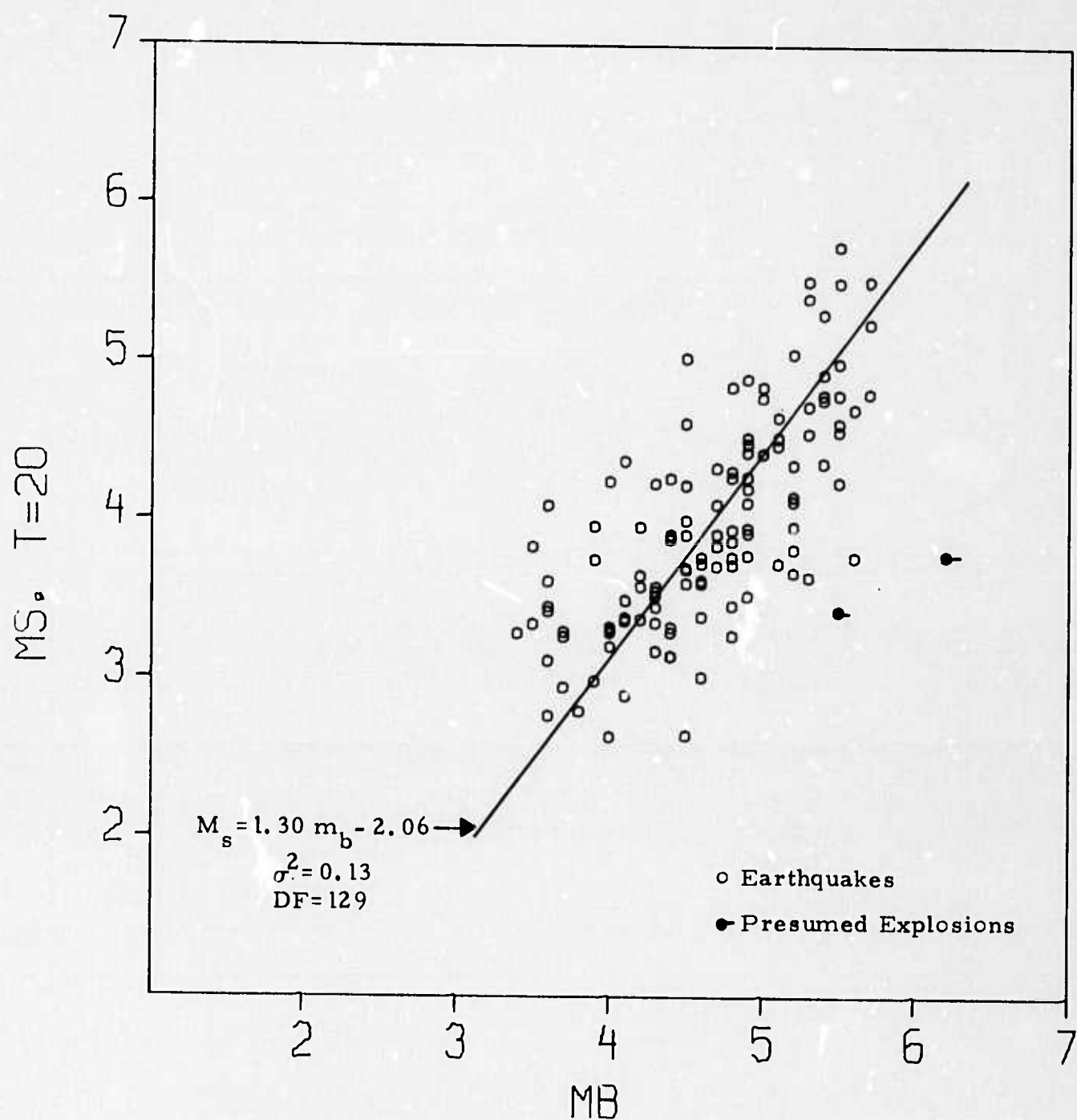
M_s VERSUS m_b AT
TLO 01/01/72 - 08/31/72

FIGURE V-4



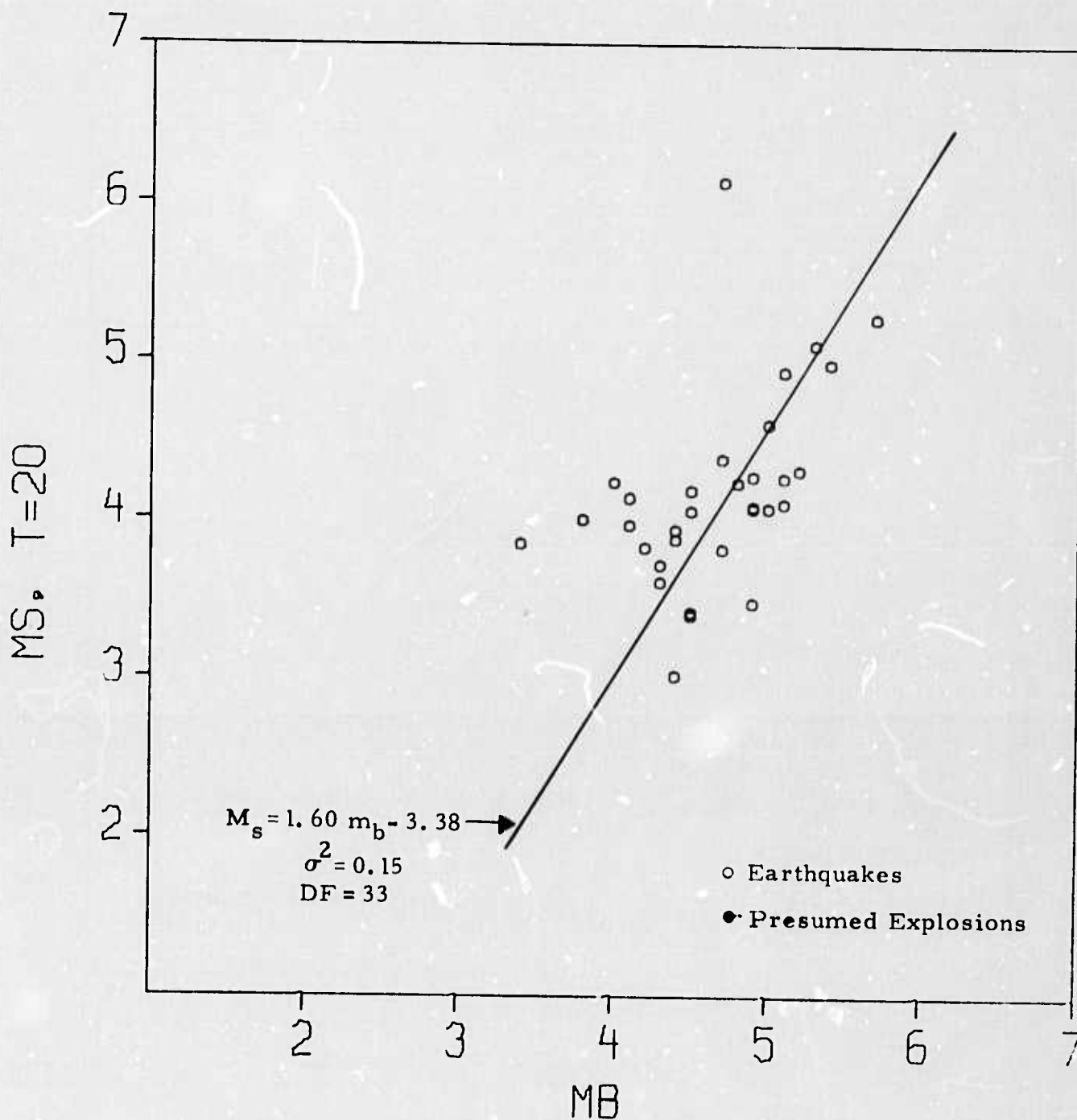
M_s VERSUS m_b AT
 EIL 06/01/72 - 12/31/72

FIGURE V-5



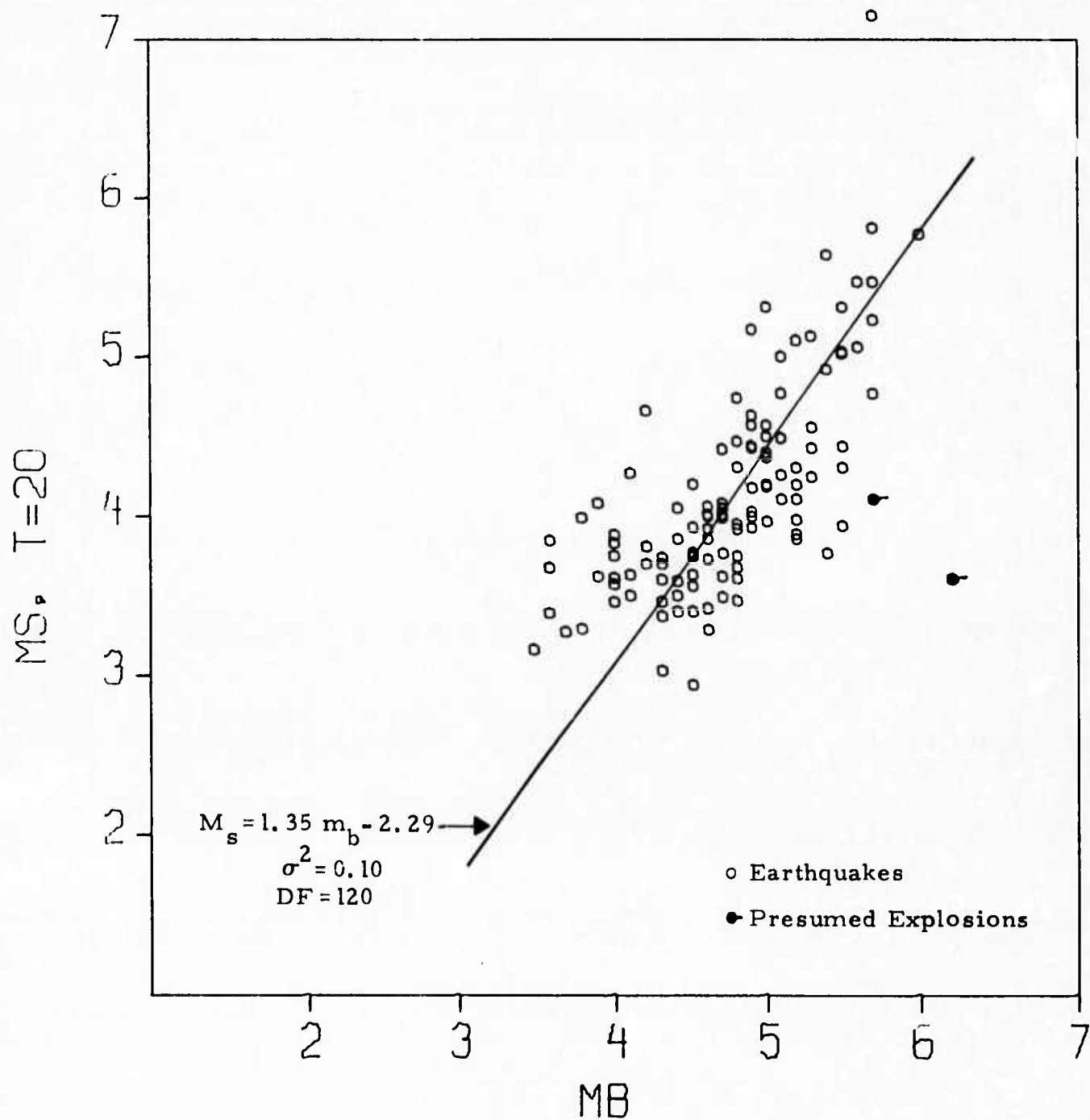
M_s VERSUS m_b AT
KON 01/01/72 - 12/31/72

FIGURE V-6



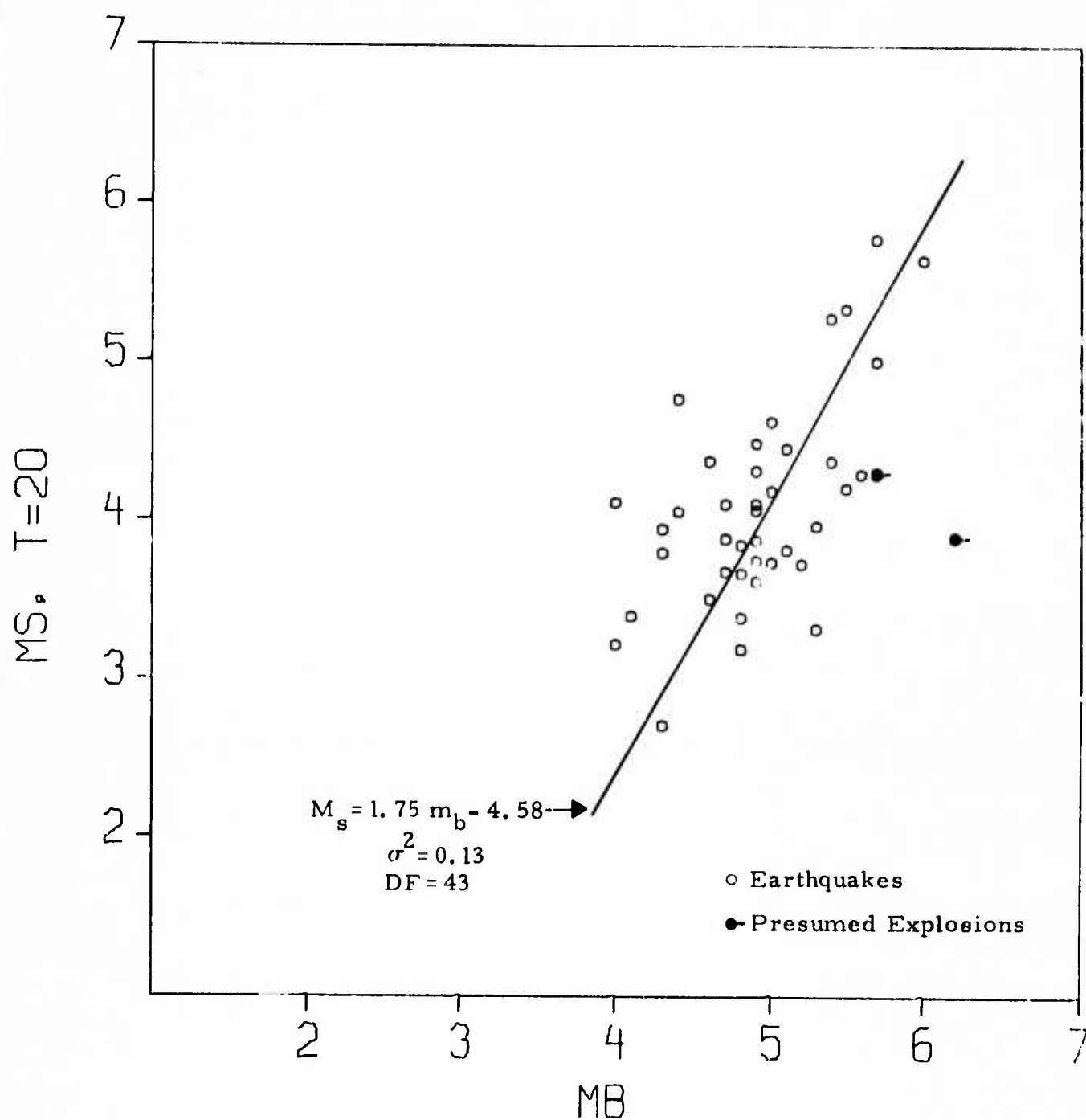
M_s VERSUS m_b AT
 OGD 01/01/72 - 08/31/72

FIGURE V-7



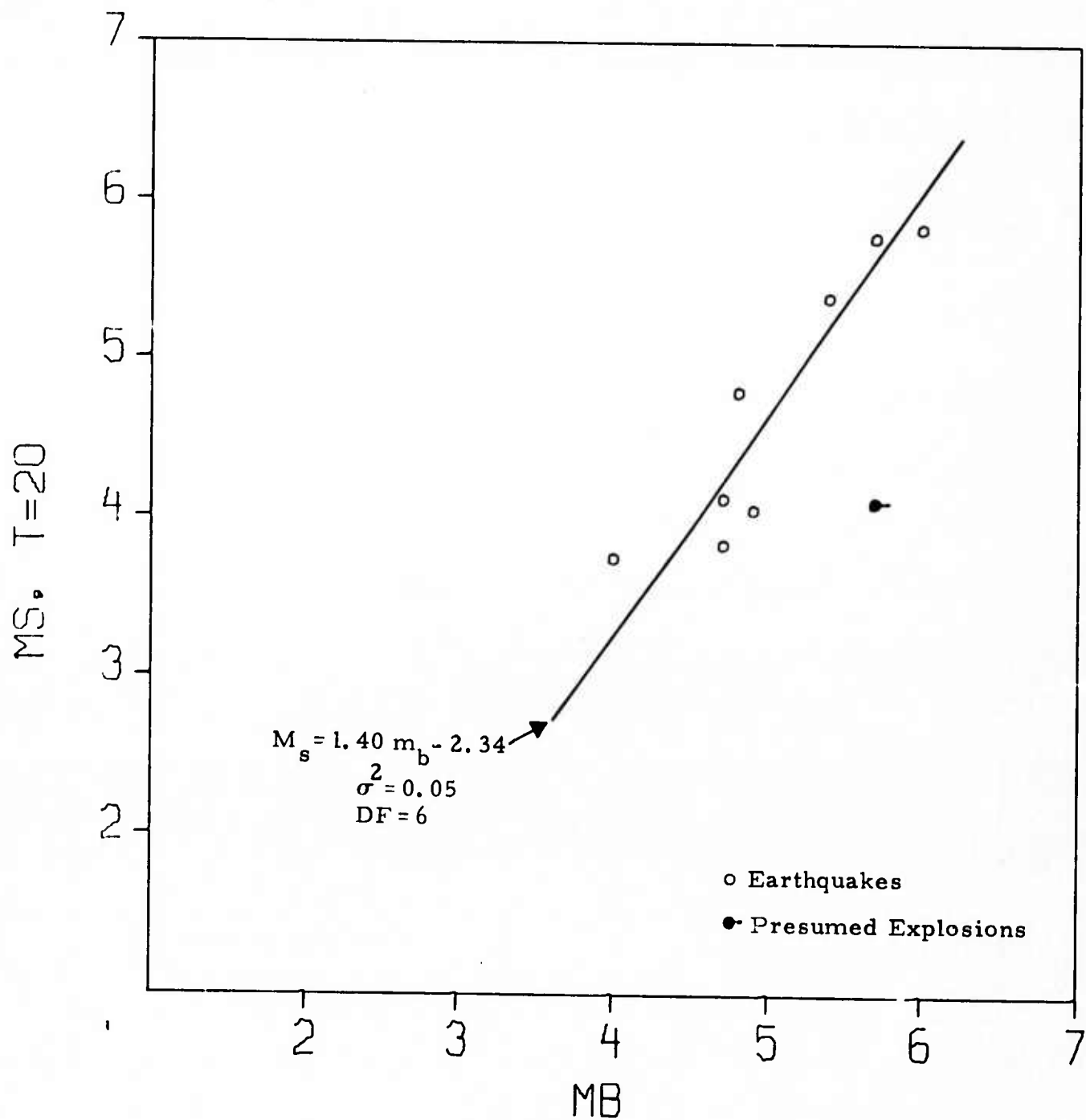
M_s VERSUS m_b AT
 KIP 06/01/72 - 12/31/72

FIGURE V-8



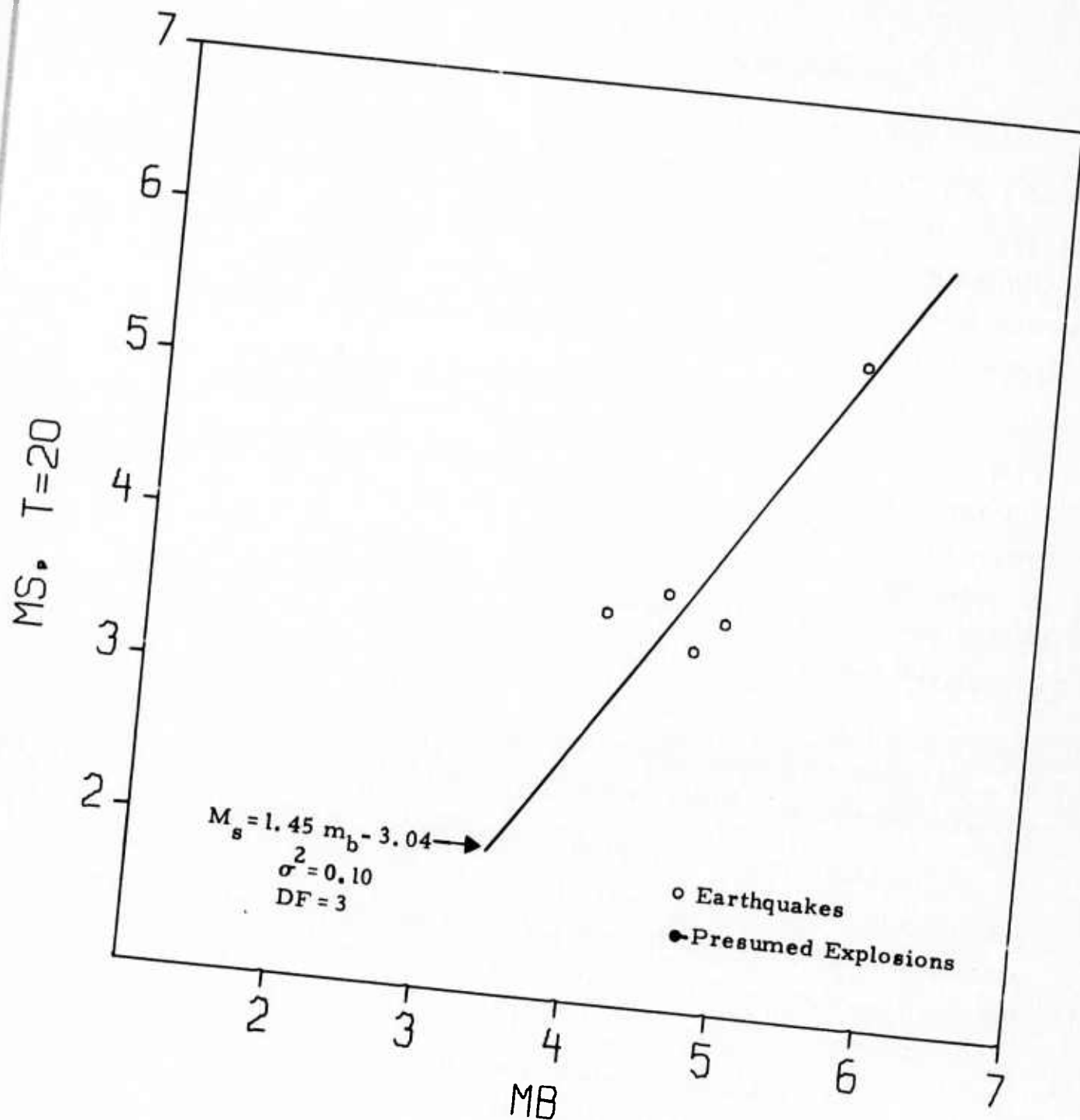
M_s VERSUS m_b AT
 ALQ 06/01/72 - 12/31/72

FIGURE V-9



M_s VERSUS m_b AT
ZLP 12/01/72 - 12/31/72

FIGURE V-10



M_s VERSUS m_b AT
 MAT 12/22/72 - 12/31/72

FIGURE V-II

2. VLPE Networks

One of the purposes of this study is to determine the capability of the VLPE network to distinguish between earthquakes and explosions. For this part of the study, we use the maximum amplitude of the Rayleigh wave for the magnitude determination. In most cases, the M_s determined at 20 seconds period is the largest value; however, in some instances M_s determined at 30 seconds period is either the largest or the only M_s reported.

Table V-1 lists the average M_s for each event, for the August 1, through December 31, 1972 ensemble of events. The Lambert and Becker (1973) report and Appendix V-B lists the average M_s for each event, for the January 1 through March 20, 1972 and June 1 through July 31, 1972 ensemble of events. Included with this M_s is the number of stations (n) taken in forming the average and the standard deviation (SD) where at least three stations provided useful signals.

Figure V-12 shows all events with their M_s value determined by one or more estimates. Figure V-13 shows only those events with their M_s value determined by two or more estimates.

Considering the total data base, separation between earthquakes and presumed underground explosions is not distinct. Many of the same earthquakes that overlapped into the presumed explosion population at single stations remain as problems even with the M_s value determined by two or more estimates.

We determined the best linear fit to these earthquake data as described above for the single stations and in Appendix V-A. For both cases the slope is 1.00 and 1.05 and the intercept is -0.76 to -1.02 with the main mass of data contained within m_b of 3.7 to 5.3 ($3.7 \leq m_b \leq 5.3$). From section IV we found for the various networks the 50% detection threshold in terms of m_b was on the average 4.2. The theoretical source spectra, Tsai (1972),

TABLE V-1
VLPE NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
(PAGE 1 OF 6)

| Event Number | m_b | VLPE | | |
|-----------------|-------|------|------------------|-------|
| | | n | Average M_s | S. D. |
| 549 | 3.7 | 1 | 3.27 | 0.31 |
| 553 | 3.8 | 1 | (2.71) | |
| 554 | 4.5 | 3 | (3.35) | |
| 555 | 3.4 | 1 | 3.44 | |
| 557 | 4.7 | 2 | (3.92) | |
| 558 | 5.1 | 5 | 4.92 | 0.46 |
| 559 | 5.0 | 5 | 5.03 | 0.46 |
| 560 | 4.2 | 1 | (3.10) | 0.44 |
| 561 | 4.3 | 2 | 3.49 | |
| 562 | 4.5 | 2 | (3.55) | |
| 563 | 4.0 | 1 | 3.86 | |
| 564 | 3.9 | 1 | 3.51 | |
| 565 | 5.3 | 4 | 4.37 | 0.44 |
| 566 | 4.5 | 3 | 3.73 | 0.41 |
| 570 | 4.3 | 2 | (3.43) | 0.53 |
| 571 | 4.0 | 1 | 3.01 | |
| 573 | 5.7 | 2 | 6.70 | |
| 578 | 4.7 | 1 | 3.77 | |
| 579 | 4.9 | 2 | 4.34 | |
| 582 | 4.5 | 3 | (3.65) | 0.45 |
| 583 | 5.5 | 2 | (4.04) | |
| 585 | 4.0 | 1 | (2.91) | |
| 586 | 5.0 | 1 | 3.81 | |
| 589 | 4.2 | 1 | 4.70 | |
| 591 | 4.5 | 2 | 3.78 | 0.45 |
| 592 | 4.0 | 2 | (2.69) | |
| 594 | 4.7 | 2 | 3.95 | |
| 596 | 5.1 | 2 | (3.94) | |
| 598 | 5.5 | 3 | (4.01) | |
| 600 | 4.5 | 1 | (4.45) | |

TABLE V-1

VLPE NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
(PAGE 2 OF 6)

| Event Number | m_b | VLPE | | |
|-----------------|-------|------|------------------|-------|
| | | n | Average M_s | S. D. |
| 601 | 4.4 | 2 | 3.61 | |
| 605 | 5.1 | 3 | 4.26 | 0.00 |
| 606 | 4.8 | 3 | 4.52 | 0.62 |
| 608 | 4.5 | 1 | 4.31 | |
| 610 | 5.2 | 3 | 4.10 | 0.09 |
| 611 | 5.0 | 3 | 4.27 | 0.09 |
| 612 | 4.0 | 1 | 3.01 | |
| 614 | 5.3 | 3 | 4.53 | 0.52 |
| 617 | 4.4 | 2 | (3.48) | |
| 626 | 5.2 | 1 | 3.35 | |
| 627 | 3.5 | 2 | 3.23 | |
| 629 | 3.6 | 1 | 3.15 | |
| 630 | 4.3 | 2 | (3.73) | |
| 640 | 3.9 | 1 | 3.55 | |
| 641 | 4.0 | 1 | 3.83 | |
| 643 | 4.0 | 3 | (3.63) | 0.21 |
| 644 | 5.1 | 1 | 4.16 | |
| 645 | 5.1 | 1 | (3.30) | |
| 649 | 4.3 | 3 | (3.63) | 0.20 |
| 650 | 3.5 | 1 | 3.16 | |
| 651 | 4.9 | 3 | (4.13) | 0.18 |
| 652 | 5.7 | 2 | (3.18) | |
| 653 | 5.2 | 4 | 4.11 | 0.16 |
| 655 | 4.0 | 3 | (3.49) | 0.51 |
| 656 | 4.8 | 4 | (3.32) | 0.13 |
| 658 | 4.5 | 1 | (3.39) | |
| 659 | 4.0 | 1 | 2.55 | |
| 660 | 4.1 | 1 | 3.34 | |
| 661 | 5.2 | 4 | (4.25) | 0.32 |
| 664 | 3.7 | 1 | (2.89) | |

TABLE V-1
VLPE NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
(PAGE 3 OF 6)

| Event Number | m_b | VLPE | | |
|-----------------|-------|------|------------------|-------|
| | | n | Average M_s | S. D. |
| 665 | 4.0 | 1 | (2.68) | |
| 671 | 3.6 | 1 | 3.68 | |
| 673 | 3.8 | 1 | 2.67 | |
| 676 | 4.8 | 1 | 4.47 | |
| 677 | 3.6 | 2 | 3.28 | |
| 678 | 4.2 | 3 | (3.98) | 0.79 |
| 679 | 6.3 | 3 | 4.74 | 0.41 |
| 680 | 5.2 | 1 | 4.12 | |
| 681 | 3.7 | 2 | (3.07) | |
| 682 | 3.7 | 2 | (2.82) | |
| 683 | 4.4 | 3 | 3.39 | 0.40 |
| 684 | 3.6 | 2 | 3.55 | |
| 685 | 3.7 | 1 | 3.12 | |
| 687 | 5.5 | 3 | 4.82 | 0.21 |
| 689 | 5.5 | 3 | 4.57 | 0.21 |
| 690 | 5.5 | 4 | 4.45 | 0.13 |
| 691 | 4.6 | 1 | 3.39 | |
| 692 | 4.3 | 1 | 3.35 | |
| 693 | 5.5 | 4 | (4.45) | 0.20 |
| 697 | 4.4 | 3 | 4.56 | 0.61 |
| 698 | 4.8 | 3 | (3.81) | 0.17 |
| 699 | 6.2 | 3 | 3.76 | 0.14 |
| 702 | 5.5 | 5 | 5.24 | 0.23 |
| 703 | 3.8 | 2 | (2.72) | |
| 704 | 5.2 | 3 | 4.69 | 0.49 |
| 708 | 4.5 | 2 | 3.83 | |
| 710 | 4.3 | 4 | 3.93 | 0.22 |
| 711 | 5.3 | 3 | 4.52 | 0.24 |
| 712 | 4.3 | 1 | 3.50 | |
| 713 | 4.5 | 2 | 4.12 | |

TABLE V-1
VLPE NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
(PAGE 4 OF 6)

| Event Number | m_b | VLPE | | |
|-----------------|-------|------|------------------|-------|
| | | n | Average M_s | S. D. |
| 716 | 5.5 | 4 | 4.89 | 0.65 |
| 718 | 4.7 | 4 | (3.94) | 0.42 |
| 723 | 4.8 | 1 | 4.84 | |
| 725 | 3.9 | 1 | (3.08) | |
| 726 | 4.1 | 2 | 4.05 | |
| 728 | 4.5 | 1 | 2.64 | |
| 729 | 4.4 | 4 | 3.68 | 0.34 |
| 734 | 4.3 | 1 | 3.52 | |
| 735 | 4.0 | 1 | (2.86) | |
| 737 | 4.6 | 4 | (3.50) | 0.35 |
| 739 | 4.0 | 2 | (3.05) | |
| 741 | 4.8 | 2 | (3.32) | |
| 742 | 4.0 | 2 | 3.21 | |
| 743 | 4.0 | 2 | 3.78 | . |
| 744 | 5.7 | 6 | (5.36) | 0.32 |
| 747 | 4.1 | 1 | 4.29 | |
| 748 | 4.0 | 2 | 3.41 | |
| 749 | 4.0 | 1 | (3.16) | |
| 750 | 4.9 | 1 | 3.72 | |
| 751 | 4.3 | 3 | (3.64) | 0.29 |
| 752 | 5.4 | 2 | 4.00 | |
| 755 | 5.2 | 1 | 3.52 | |
| 757 | 3.9 | 1 | (3.26) | |
| 758 | 5.1 | 3 | 4.23 | 0.27 |
| 760 | 5.6 | 2 | 3.86 | |
| 761 | 5.2 | 5 | 3.74 | 0.10 |
| 762 | 4.9 | 4 | (4.07) | 0.30 |
| 764 | 4.7 | 3 | (3.64) | 0.15 |
| 765 | 4.8 | 2 | 3.86 | |
| 771 | 4.4 | 1 | 3.29 | |

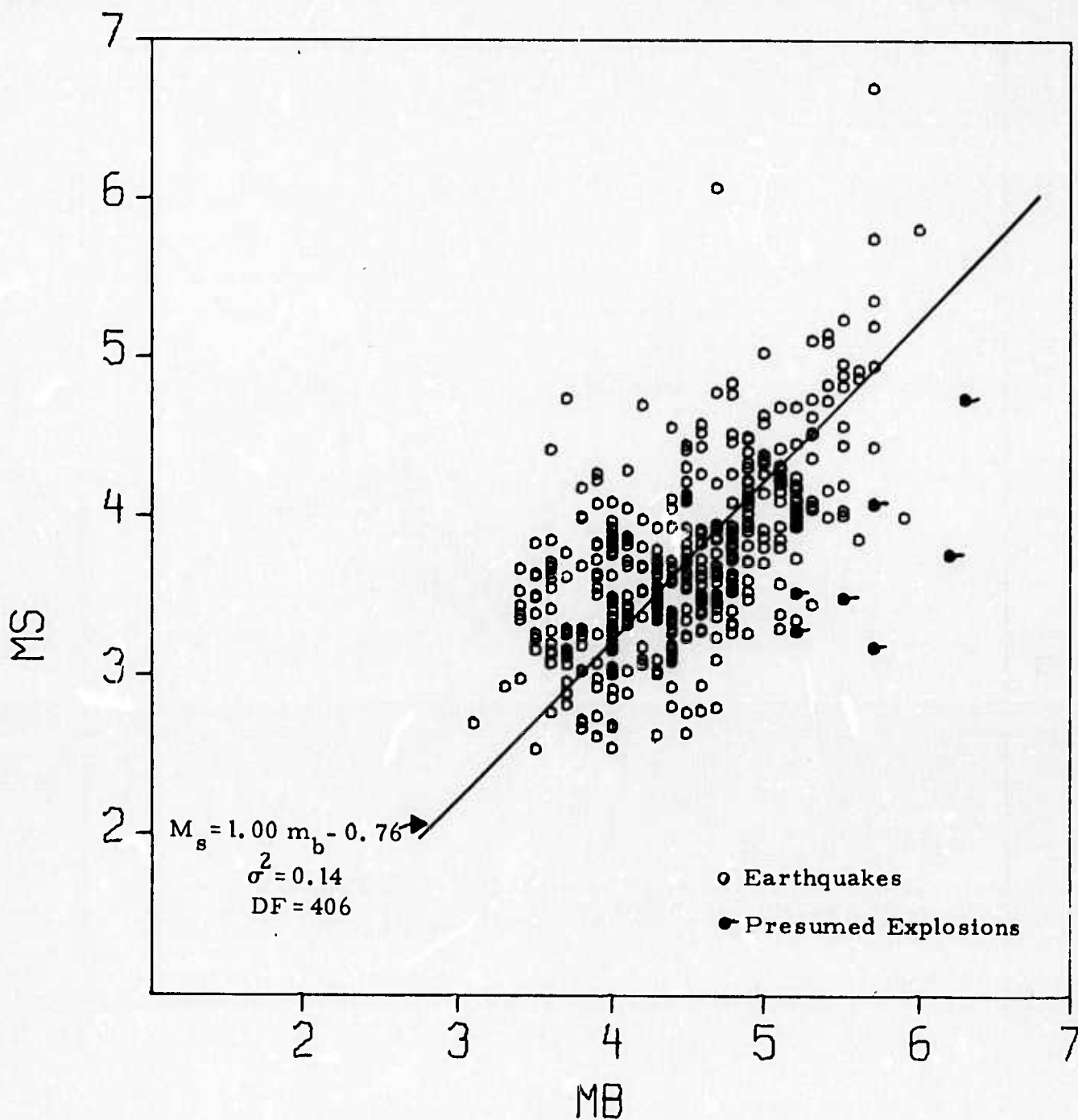
TABLE V-1
VLPE NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
(PAGE 5 OF 6)

| Event Number | m_b | VLPE | | |
|-----------------|-------|------|------------------|------|
| | | n | Average M_s | S.D. |
| 773 | 3.9 | 1 | 2.98 | |
| 774 | 4.7 | 2 | (2.80) | |
| 775 | 5.4 | 5 | 5.15 | 0.18 |
| 776 | 4.8 | 4 | 3.73 | 0.24 |
| 778 | 5.1 | 4 | (4.10) | 0.29 |
| 781 | 5.0 | 3 | (3.71) | 0.27 |
| 783 | 4.4 | 1 | 3.59 | |
| 785 | 5.3 | 3 | 4.63 | 0.25 |
| 786 | 4.3 | 1 | (3.03) | |
| 787 | 3.7 | 1 | (3.14) | |
| 790 | 4.7 | 3 | 3.95 | 0.39 |
| 791 | 3.7 | 1 | (3.16) | |
| 797 | 5.7 | 4 | 4.08 | 0.19 |
| 799 | 6.0 | 4 | 5.81 | 0.16 |
| 802 | 4.8 | 2 | 4.77 | |
| 813 | 4.8 | 4 | 4.09 | 0.21 |
| 814 | 4.1 | 1 | 3.42 | |
| 818 | 5.7 | 4 | 4.44 | 0.22 |
| 821 | 4.6 | 1 | 3.29 | |
| 823 | 4.3 | 1 | 3.94 | |
| 825 | 4.7 | 5 | 4.21 | 0.23 |
| 826 | 4.7 | 1 | (3.51) | |
| 827 | 4.4 | 1 | 4.05 | |
| 828 | 5.7 | 5 | 5.75 | 0.27 |
| 836 | 4.6 | 2 | 3.57 | |
| 837 | 4.9 | 5 | 3.72 | 0.35 |
| 839 | 4.0 | 4 | 3.81 | 0.23 |
| 840 | 3.8 | 1 | 3.99 | |
| 842 | 4.7 | 4 | (3.87) | 0.16 |
| 844 | 4.6 | 5 | 4.27 | 0.16 |

TABLE V-1
VLPE NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
(PAGE 6 OF 6)

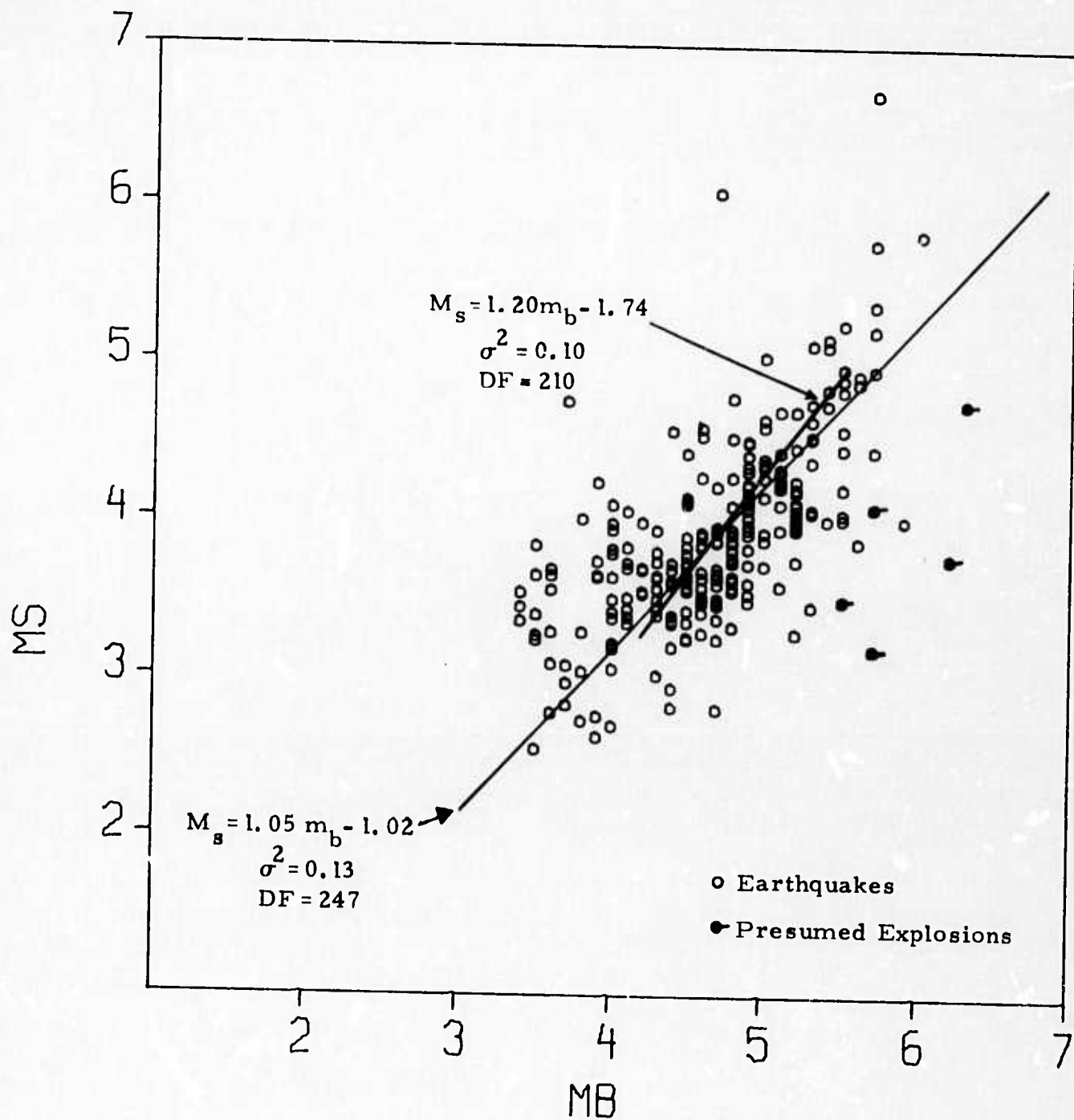
| Event Number | m_b | VLPE | | |
|-----------------|-------|------|------------------|-------|
| | | n | Average M_s | S. D. |
| 848 | 4.2 | 1 | 3.07 | 0.28 |
| 852 | 4.1 | 1 | (3.44) | |
| 856 | 3.7 | 2 | 2.96 | |
| 857 | 4.8 | 3 | 3.62 | |
| 858 | 4.7 | 4 | 3.66 | |
| 859 | 5.7 | 7 | 5.20 | 0.12 |
| 860 | 3.5 | 1 | 3.63 | 0.10 |
| 862 | 4.6 | 1 | 2.94 | |
| 863 | 3.6 | 1 | 3.61 | |
| 867 | 4.1 | 3 | 3.43 | |
| 868 | 4.3 | 1 | 3.53 | |
| 870 | 4.1 | 2 | 3.69 | 0.55 |
| 873 | 4.5 | 2 | 3.62 | |
| 874 | 4.4 | 1 | 3.27 | |
| 875 | 4.9 | 4 | 4.22 | |

() Averages with M_s , $T=30.0$ seconds
V-20



ONE OR MORE STATIONS
 MS VERSUS MB

FIGURE V-12



TWO OR MORE STATIONS
 MS VERSUS MB

FIGURE V-13

shows that for m_b between 4.2 and 5.5 we should expect a linear slope. We considered all M_s data for $4.2 \leq m_b \leq 5.5$ where M_s was determined by two or more estimates and obtained $M_s = 1.20 m_b - 1.74$, $\sigma^2 = 0.10$, with 210 degrees of freedom (Figure V-13). This agrees well with that predicted from the theoretical source spectra and further, the slope is equal to that observed at ALPA where Strauss (1973) reports $M_s = 1.20 m_b - 2.20$ for the same m_b increment.

3. Summary

Utilizing all the data analyzed for the year 1972 we find that it is not possible to discriminate completely between presumed explosions and earthquakes located in Eurasia. However, Lambert and Becker (1973) show for a subset of data from June 1 through July 31, 1972 where M_s is determined from two or more values there is complete separation of the two populations. Clearly, we need to study regional and temporal subsets of the data, and various networks of VLPE sites to define the problems of discriminating with M_s and m_b .

Single station general linear trends of $M_s - m_b$ are determined without consideration of errors introduced to low magnitude estimates due to noise. Further, we need more data at many of the stations and the bias caused by noise for small events must be considered, to ascertain the true station response to events from Eurasia.

C. LOVE TO RAYLEIGH WAVE AMPLITUDE RATIOS (LQ/LR)

A potential measure of detection and discrimination capability for the VLPE is the LQ/LR ratio. Various authors have reported larger shear-to-compressional amplitudes for earthquakes than for underground nuclear explosions.

Strauss (1973) reports a mean LQ/LR ratio of 1.16 at ALPA with nearly equal detection rates for LQ and LR. Similarly, Laun et al (1973)

reports a value of 1.35 for NORSAR with the LQ and LR detection rates again nearly equal.

Figure V-14 shows the distribution of LQ/LR ratios for earthquakes recorded by VLPE stations. We obtain a mean value of 1.18 for this ratio. No LQ/LR ratios were obtained at EIL for either the January 1 through March 20, 1972 or June 1 through August 31, 1972 event ensembles. Further, the ratios determined at OGD for June 1 through August 31, 1972 event ensemble were not included due to erratic gains encountered on the horizontal components. Individual station and event LQ/LR ratios are tabulated in Appendixes II-B through II-L. The average LQ/LR value of 1.18 may be biased due to problems associated with the horizontal instruments and due to the fact that the detection rate for Love waves could not be determined. However, the mean LQ/LR ratio of 1.18 observed by the VLPE network is consistent with those independently determined at ALPA and NORSAR.

Table V-2 presents the arithmetic means and the variances of the log (LQ/LR) values plus the antilogs of the mean as a function of region. The locations of the regions studied are shown in Figure V-15. Two regions have LQ/LR ratios of less than one, East Kazakh and the Kurile Island region. The three ratios from East Kazakh are from two large presumed explosions (event numbers 699 and 797).

Von Seggern (1972) gives the distribution for 412 LQ/LR ratios for underground explosions from the Nevada Test Site (NTS) and the Amchitka test site. Most of the ratios were obtained from the NTS and a few from Amchitka. We determined the mean of these values to be about 0.60. This compares favorably with the East Kazakh presumed explosion value of 0.72. Further, this value of 0.72 is probably high due to the almost total lack of Love wave amplitude measurements for any of the presumed explosions as measured at the various VLPE sites.

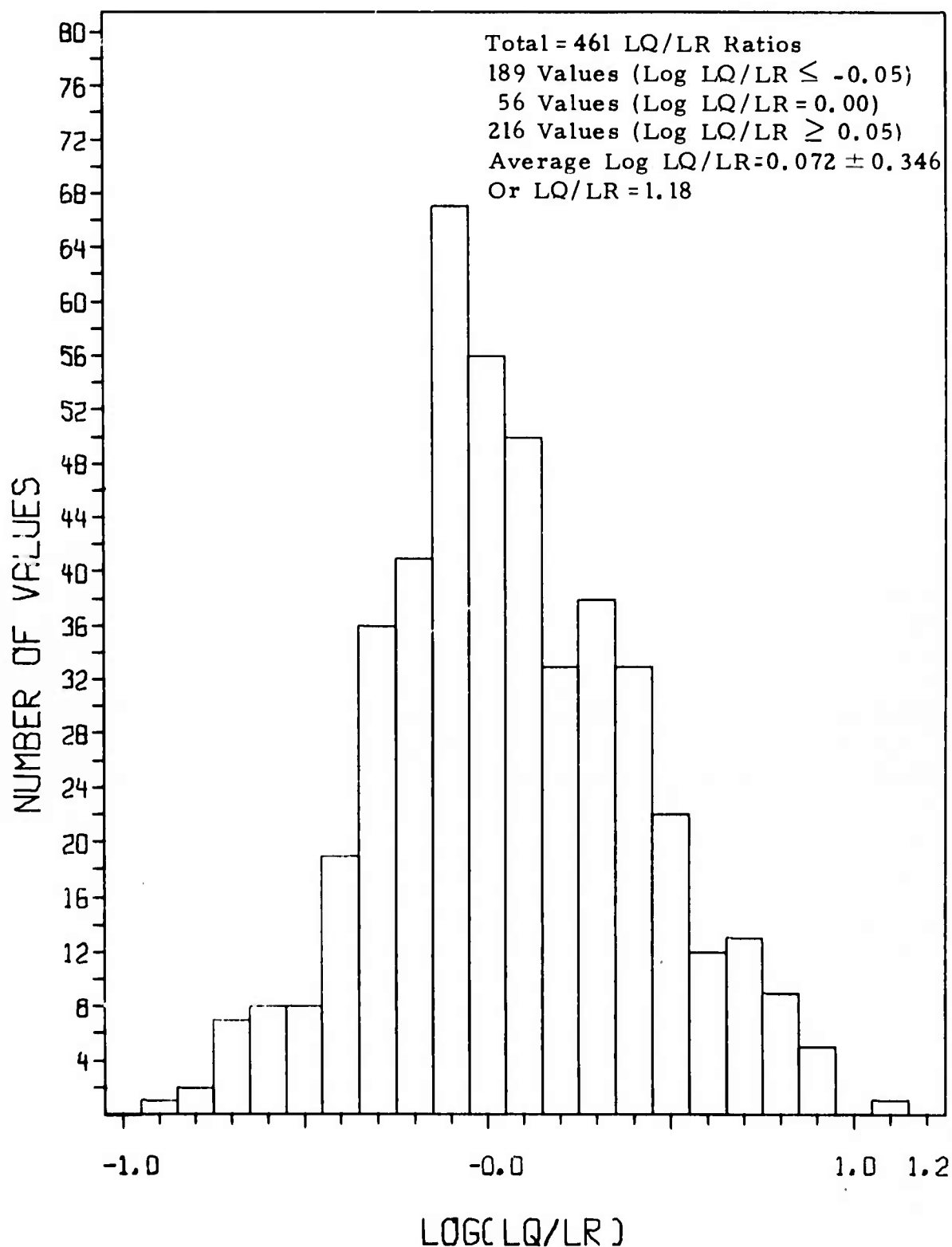
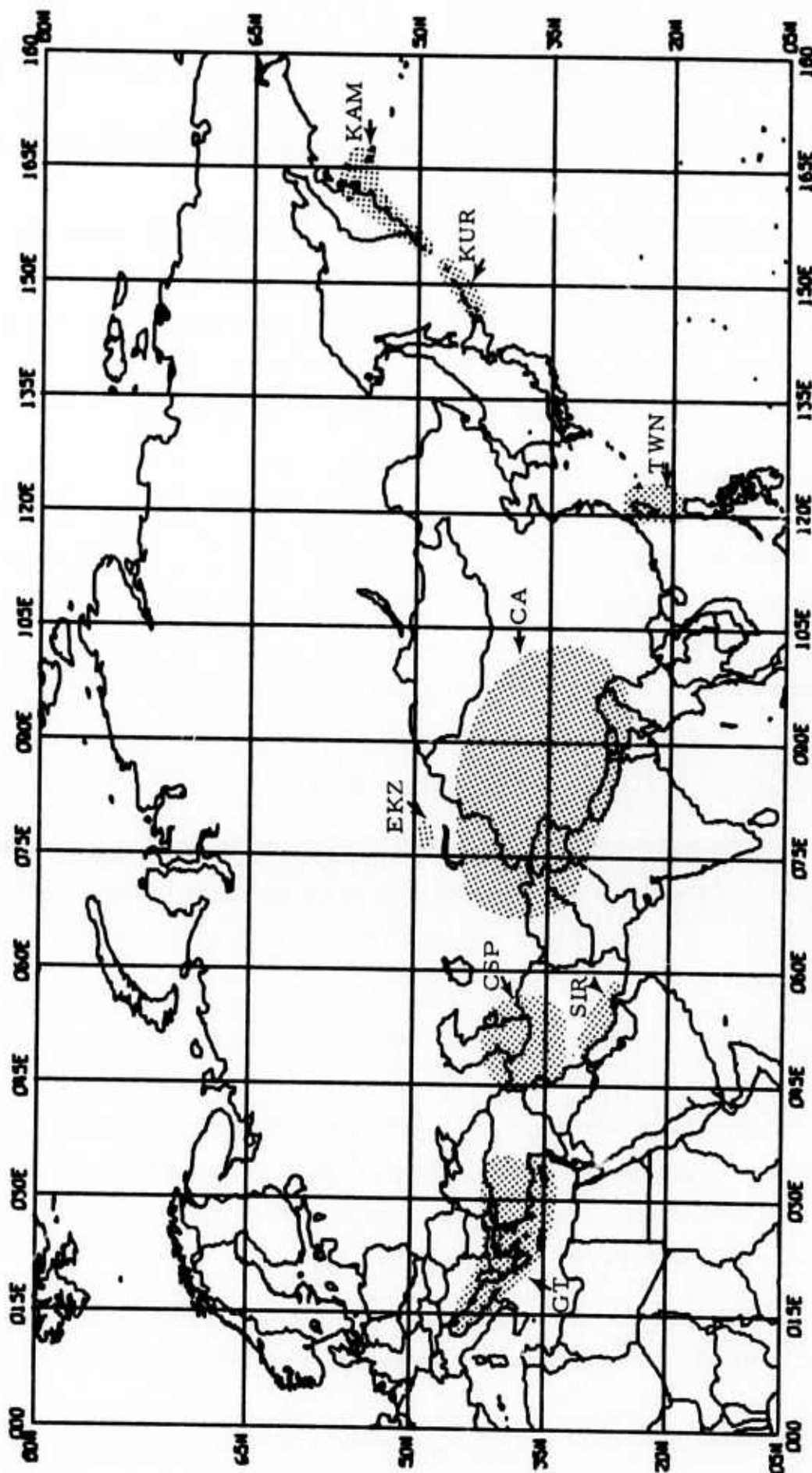


FIGURE V-14
 LOVE TO RAYLEIGH WAVE AMPLITUDE RATIOS
 OF EURASIAN EVENTS SEEN BY VLPE STATIONS
 V-25

TABLE V-2
TABLE OF ARITHMETIC MEANS OF LOG (LQ/LR) VALUES AND
THEIR RESPECTIVE VARIANCES AND ANTILOGS
(AS A FUNCTION OF REGION)

| Region | Arithmetic Mean of Log(LQ/LR) | σ^2 of Mean of Log(LQ/LR) | Antilog of Mean |
|--------------------|-------------------------------------|-------------------------------------|--------------------|
| Central Asia | 0.04(N=64) | 0.12 | 1.10 |
| Caspian Sea | 0.12(N=15) | 0.08 | 1.32 |
| East Kazakh | -0.14(N=3) | 0.11 | 0.72 |
| Greece-Turkey | 0.15(N=81) | 0.15 | 1.42 |
| Kamchatka | 0.02(N=79) | 0.12 | 1.04 |
| Kurile Is. | -0.04(N=59) | 0.11 | 0.91 |
| Southern Iran | 0.15(N=25) | 0.13 | 1.41 |
| Taiwan | 0.08(N=53) | 0.10 | 1.21 |
| No Specific Region | 0.06(N=82) | 0.11 | 1.14 |



MILLER MODIFIED MERCATOR PROJECTION
 MAP SCALE: 0.750 IN. / 15 DEG. LONGITUDE

FIGURE V-15

LOCATION OF THE SEISMIC REGIONS

Table V-3 shows the arithmetic means of the LQ/LR ratios as a function of region and station. The index "Station Code" refers to the VLPE stations in the following order: 1(CTA), 2(CHG), 3(FBK), 4(TLO), 5(EIL), 6(KON), 7(OGD), 8(KIP), 9(ALQ), 10(ZLP) and 11(MAT). Variances for these values have not been included since the number of LQ/LR values for each station per region is quite small (average $N=6$). In addition, the table presents the azimuths computed from the approximate region centers to each station as defined by Strauss (1973) and shown in Figure V-15.

There does not seem to be any correlation between these azimuths and the LQ/LR values. That is, for a given station the mean LQ/LR with the same approximate azimuths appear unrelated. Similarly, for a given region the mean ratios of different stations with similar azimuths vary significantly. This suggests that earthquake source parameters vary significantly within a given region; however, we have insufficient data to reach any definite conclusion.

D. SURFACE WAVE RADIATION PATTERNS

Amplitude and phase radiation patterns of seismic energy from the source have been utilized very little in discrimination. One major difficulty is that the influence of path and recording site on amplitudes must be minimized.

Attempts to determine radiation patterns for presumed East Kazakh explosions and earthquakes near the presumed explosions utilizing the distance function in the M_s formula were unsuccessful. This was primarily due to the paucity of LR or LQ data at many azimuths and the fact that the distance function in the M_s formula essentially accounts only for the average effective attenuation over all stations.

Toksoz et al (1964) minimizes path and site effects by ratioing Love and Rayleigh wave amplitudes; however, as shown above in the discussion

TABLE V-3
TABLE OF ARITHMETIC MEANS OF LQ/LR RATIOS
(AS A FUNCTION OF REGION & STATION)

| Regions | | | | | | | | |
|---------|--------------|-----|-------------|-----|-------------|-----|---------------|-----|
| | Central Asia | AZ | Caspian Sea | AZ | East Kazakh | AZ | Greece Turkey | AZ |
| 1 | 1.13 N=4* | 124 | - N=0 | 103 | - N=0 | 121 | 1.19 N=3 | 88 |
| 2 | 1.82 N=5 | 146 | 2.44 N=1 | 100 | 0.83 N=1 | 147 | 1.69 N=13 | 84 |
| 3 | 0.93 N=11 | 22 | - N=0 | 8 | - N=0 | 21 | 1.29 N=6 | 357 |
| 4 | 1.10 N=5 | 302 | 2.27 N=5 | 290 | - N=0 | 295 | 2.53 N=14 | 284 |
| 5 | 1.87 N=6 | 272 | 0.89 N=2 | 240 | - N=0 | 258 | - N=0 | 133 |
| 6 | 1.88 N=24 | 320 | 0.82 N=3 | 323 | - N=0 | 312 | 2.24 N=30 | 340 |
| 7 | 0.53 N=3 | 345 | 0.72 N=1 | 321 | - N=0 | 341 | 0.67 N=9 | 309 |
| 8 | 2.12 N=6 | 56 | 1.57 N=3 | 29 | 0.52 N=1 | 52 | - N=0 | 3 |
| 9 | - N=0 | 10 | - N=0 | 340 | 0.86 N=1 | 5 | 4.94 N=5 | 322 |
| 10 | - N=0 | 307 | - N=0 | 274 | - N=0 | 310 | 1.58 N=1 | 259 |
| 11 | - N=0 | 77 | - N=0 | 61 | - N=0 | 84 | - N=0 | 48 |

*N=Total number of LQ/LR ratios considered

TABLE V-3
TABLE OF ARITHMETIC MEANS OF LQ/LR RATIOS
(Continued)

| Station Code | Regions | | | | | | | | | | |
|--------------|-------------|--------------|---------------|--------------|------------------|-------------|-------------|--------------|--------------|--------------|---|
| | Kamchatka | AZ | Kurile Is. | AZ | Southern Iran | AZ | Taiwan | AZ | No Region | AZ | |
| | 1 | 1.69 N=6 | 196 | 2.24 N=5 | 122 | 1.84 N=4 | 106 | 1.22 N=5 | 149 | 1.48 N=5 | ? |
| | 2 | 2.01 N=9 | 260 | 0.84 N=9 | 253 | 1.73 N=4 | 93 | 1.59 N=13 | 266 | 2.22 N=12 | ? |
| | 3 | 1.50 N=12 | 46 | 1.41 N=8 | 37 | 1.99 N=2 | 9 | 1.26 N=4 | 27 | 1.09 N=11 | ? |
| | 4 | 1.45 N=11 | 350 | 3.34 N=1 | 339 | 0.86 N=2 | 299 | 1.38 N=8 | 321 | 1.72 N=14 | ? |
| | 5 | 0.36 N=2 | 317 | 0.87 N=2 | 306 | - N=0 | 276 | - N=0 | 297 | 0.72 N=4 | ? |
| | 6 | 1.31 N=16 | 345 | 0.97 N=9 | 339 | 2.99 N=7 | 329 | 2.14 N=10 | 332 | 1.08 N=18 | ? |
| | 7 | 1.50 N=4 | 42 | 0.29 N=3 | 31 | - N=0 | 323 | 1.19 N=4 | 14 | 0.81 N=3 | ? |
| | 8 | 1.23 N=15 | 122 | 1.40 N=12 | 100 | 1.40 N=4 | 34 | 0.91 N=5 | 73 | 2.29 N=11 | ? |
| 9 | 1.62 N=3 | 67 | 1.21 N=5 | 55 | 1.97 N=1 | 342 | 2.76 N=4 | 40 | 0.77 N=3 | ? | |
| 10 | 0.59 N=1 | 67 | 0.65 N=4 | 301 | 0.80 N=1 | 269 | - N=0 | 62 | 1.60 N=1 | ? | |
| 11 | .. N=0 | 134 | 0.72 N=1 | 164 | - N=0 | 59 | - N=0 | 41 | - N=0 | ? | |

of LQ/LR ratios only three such values were available from two presumed explosions from East Kazakh.

Turnbull and Sun (1973) determined the source parameters and resultant radiation patterns for two Central Italy events (numbers 97 and 105) with the use of VLPE LR and LQ spectra. These results compare favorably with body wave solutions of appropriate Italian events described by McKenzie (1972).

Figures V-16 and V-17 present the theoretical LQ/LR radiation patterns as determined by Turnbull and Sun (1973). The solid dots are the observed LQ/LR amplitude ratios. The observed ratios do compare well with the theoretical patterns, but they also demonstrate the need for more data at more azimuths to determine source parameters.

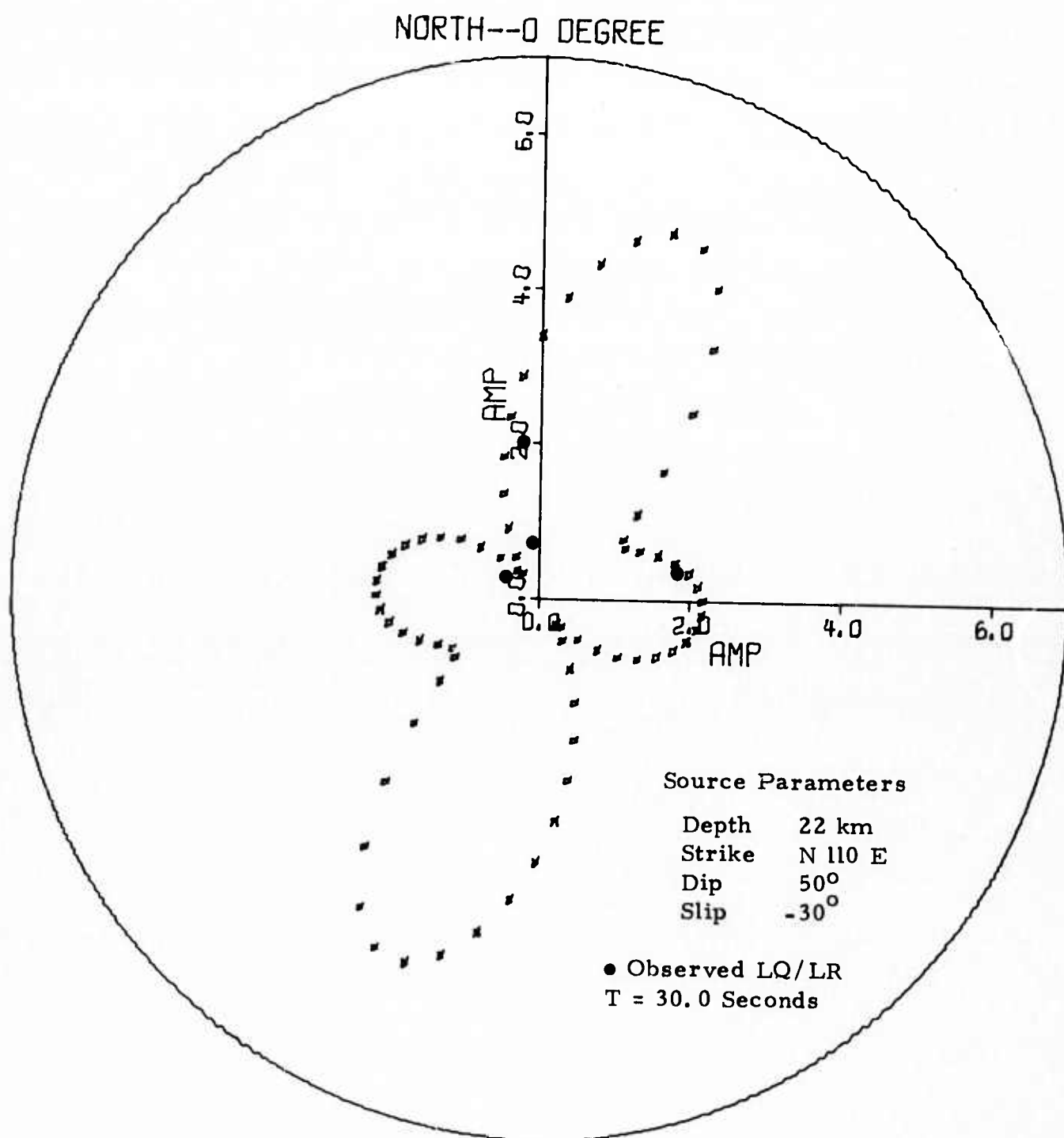


FIGURE V-16
THEORETICAL AND OBSERVED LQ/LR RADIATION PATTERN FOR EVENT 97

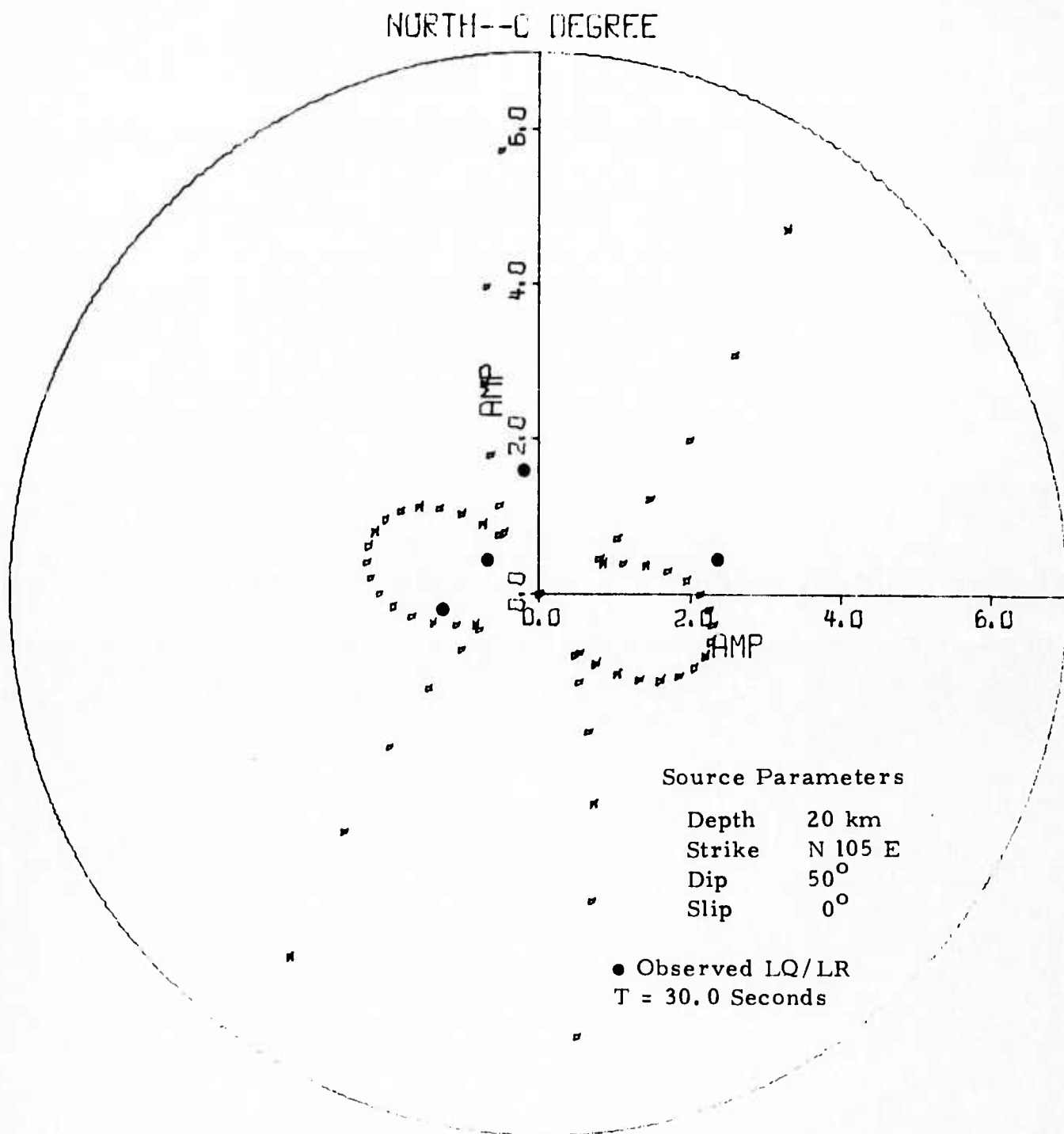


FIGURE V-17

THEORETICAL AND OBSERVED LQ/LR RADIATION PATTERN FOR EVENT 105
V-33

SECTION VI

SUMMARY AND CONCLUSIONS

A. NOISE SUMMARY

Data from vertical and simultaneous component noise samples from VLPE sites show the following:

- The presence of a "stable noise minimum" is evident in the approximate range of 22-35 seconds.
 - At most VLPE sites a microseismic peak is present in the 17-20 second period range.
 - There is a leveling off of the vertical and horizontal noise field at periods below the microseismic peak while at periods above 30-35 seconds great variability in the horizontal noise field relative to the vertical noise field.
 - Seasonal variations in the vertical noise fields are suggested by the slowly changing long term nature of the vertical noise fields.
 - Intercomponent frequency dependent cross-correlation of the RMS amplitudes is rarely observed but when present, it occurs only at the same periods on both correlated components.
- Despite this occasional correlation, we interpret this to mean that in general noise on one component is independent of noise on the other two.

A larger more continuous data base is required to ascertain whether seasonal variations in the noise field occur at the VLPE sites. We have insufficient noise data for stations EIL, ZLP, and MAT for all aspects of noise analysis.

B. SUMMARY OF VLPE DETECTION CAPABILITY

- The single station detectability estimates for m_b and M_s are listed in Table IV-1.
- Separate estimates were computed for all events within 50 degrees epicentral distance. It is seen that the difference in 50 percent detectability for these two subsets ranges from 0.2 to 0.5 m_b units.
- The best stations are CHG and KON (m_b of 4.35 and 4.38) and the average m_b for all stations is 4.56.
- The three networks requiring one operational station are almost equivalent in terms of the 50 percent m_b threshold ($m_b \approx 4.2$). The same three networks requiring two operational stations also are about equivalent in terms of the 50 percent m_b threshold ($m_b \approx 4.5$). The network detectability estimates for m_b and M_s are listed in Table IV-2.
- M_s threshold values listed in Tables IV-1 and IV-2 are subject to significant uncertainties, and it is expected that more reliable estimates may be obtained in our future studies when direct detection statistics based on M_s values become available.
- The probability of mixed events occurring at VLPE networks are displayed in Table IV-3. These probabilities are valid only for the present VLPE capability.
- Based on 844 events with at least one operational station we classified 22 percent of the events as mixed events.
- The actual number of events that remained as mixed events for the total network was 49 and the average number of operational

stations was 3.8. This results in 5.8 percent mixed events remaining.

- Matched filters (reference waveform and chirp) yielded an average of 3.6 dB SNNR improvement when applied to Rayleigh waves.
- Application of matched filters increases the number of detections by a factor of two. However, the small data base used precludes the determination of accurate detection thresholds.
- Preliminary evaluation of the Three Component Adaptive processor yielded detection results comparable to those for the chirp filter.

C. SUMMARY OF VLPE DISCRIMINATION CAPABILITY

- M_s versus m_b separation between earthquakes and presumed explosions is not distinct at single VLPE stations or the total VLPE network. We need to study regional and temporal subsets of the data and various networks of VLPE sites to define the problems of discriminating with M_s and m_b .
- Single station and the total-network linear trends of M_s versus m_b are determined. However, the effect of noise on low magnitude estimates must be considered and trends must be segmented or fitted with a higher order polynomial to ascertain the true station and network response to events from Eurasia.
- We obtained a mean of 1.18 for the Love to Rayleigh wave amplitude ratio for Eurasian earthquakes, and for two presumed explosions from East Kazakh, three ratios gave an average LQ/LR of 0.72.
- A mean LQ/LR of about 0.60 was determined for 412 ratios reported by Von Seggern for explosions from mostly the NTS and a few from Amchitka. This compares favorably with the East Kazakh

value of 0.72 especially since this value is probably high due to the almost total lack of Love wave amplitude measurements for any of the presumed explosions.

- No correlation of LQ/LR ratios between regions and stations having the same azimuths was observed. This suggests that either the earthquake source parameters vary significantly within the defined regions and/or reflects the poor quality of data available from the VLPE horizontal components.
- Attempts to determine radiation patterns for presumed East Kazakh explosions and earthquakes near the presumed explosions were unsuccessful due to the lack of LR or LQ data at many azimuths.

For future studies, we can make the following recommendations:

- A larger more continuous data base is required to ascertain whether seasonal variations in the noise field occur at the VLPE sites. Acquire more data for stations EIL, ZLP, and MAT to complete the noise analysis at these sites.
- Determine the detection thresholds of VLPE stations and networks in terms of M_s based on direct detection statistics when sufficient M_s data becomes available.
- Enlarge the data base for application of matched filters and Three Component Adaptive processor to define the capabilities of these techniques.
- Determine the true M_s versus m_b response of single station and network for Eurasian events.

SECTION VII

ACKNOWLEDGMENTS

We wish to thank T. W. Harley and L. S. Turnbull for their many helpful discussions and critical reading of this paper. We especially wish to acknowledge F. Ringdal, A. I. Tolstoy and L. S. Turnbull for their assistance with the theory and programs used in the determination of the maximum likelihood detection threshold estimates and the linear M_s versus m_b trends. We are also grateful to E. S. Becker and A. I. Tolstoy for their capable assistance in processing, analysis, and reduction of the data.

SECTION VIII
REFERENCES

- Alsup, S. A., and E. S. Becker, 1973a, Simultaneous Three-Component Broad-Band Earth Noise Structure at Very Long Period Experiment Station; Special Report No. 10, AFTAC Contract No. F 33657-72-C-0725, Texas Instruments Incorporated Dallas, Texas.
- Alsup, S. A., and E. S. Becker, 1973b, Long-Term Broad-Band Vertical Earth Noise Structure at Very Long Period Experiment Sites; Special Report No. 3, AFTAC Contract No. F33657-72-C-0725, Texas Instruments Incorporated, Dallas, Texas.
- Harley, T. W., 1971, Long Period Array Processing Development; Final Report, AFTAC Contract No. F33657-69-C-1063, Texas Instruments Incorporated, Dallas, Texas.
- Harley, T. W. and L. N. Heiting, 1972, Indirect Estimates of Surface Wave Detection Probabilities; Special Report No. 1, AFTAC Contract No. F33657-71-C-0842, Texas Instruments Incorporated, Dallas, Texas.
- Heiting, L. N., G. D. McNeely, and A. C. Strauss, 1972, Special Report No. 4, Extended Array Evaluation Program, AFTAC Contract No. F33657-71-C-0843, Texas Instruments Incorporated, Dallas, Texas.
- Lacoss, R. T., 1971, NORSAR Conference, Oslo, Norway, November.
- Lambert, D. G., and E. S. Becker, 1973, Evaluation of the Detection and Discrimination Capabilities of the Very Long Period Experiment (VLPE) Single Stations, VLPE Network, and the VLPE-ALDA-NORSAR combined Network; Special Report No. 6, AFTAC Contract No. F33657-72-C-0725, Texas Instruments Incorporated, Dallas, Texas.

- Lane, S. S., 1973, Special Report No. 15, In Preparation, AFTAC Contract No. C33657-72-C-0725, Texas Instruments Incorporated, Dallas, Texas.
- Laun, P. R., W. W. Shen, and W. H. Swindell, 1973, Continued Evaluation of the Norwegian Long Period Array; Special Report No. 7, AFTAC Contract No. F33657-72-C-0725, Texas Instruments Incorporated, Dallas, Texas.
- McKenzie, D., 1972, Active Tectonics in the Mediterranean Region; Geophys. J. R. Astr. Soc., 2, 109-185.
- Pomeroy, P. W., G. Hade, J. Sarino, and R. Chander, 1969, Preliminary Results from High-Gain Wide-Band Long-Period Electromagnetic Seismograph Systems; J. Geophys. Res., 74, 3295-3302.
- Ringdal, F. and R. L. Whitlaw, 1973, Special Report No. 11, In Preparation, AFTAC Contract No. C33657-72-C-0725, Texas Instruments Incorporated, Dallas, Texas.
- Savino, J., L. R. Sykes, R. C. Liberman, and P. Molar, 1971, Excitation of Seismic Surface Waves with Periods of 15 to 70 Seconds for Earthquakes and Underground Explosions; J. Geophys. Res., 76, 8002-8020.
- Savino, J. M., A. J. Murphy, J. M. W. Rynn, R. Tatham, L. R. Sykes, G. L. Choy, K. McCann, 1972, Results from the High-Gain Long-Period Seismograph Experiment; The Geophys. J. R. Astr. Soc., 31, 179-204.
- Strauss, A. C., 1973, Final Evaluation of the Detection and Discrimination Capability of the Alaskan Long Period Array; Special Report No. 8, AFTAC Contract No. F33657-72-C-0725, Texas Instruments Incorporated, Dallas, Texas.

- Toksöz, M. N., A. Ben-Menaham, and D. C. Harkrider, 1964, Determination of Source Parameters by Amplitude Equalization of Seismic Surface Waves: 1. Underground Nuclear Explosions; J. Geophys. Res., 69, 4355-4366.
- Tsai, Y. B., 1972, Utility of Tsai's Method for Seismic Discrimination; Semi-Annual Technical Report No. 2, AFSOR Contract No. F44620-71-C-0112, Texas Instruments Incorporated, Dallas, Texas.
- Turnbull, L. S., and D. F. D. Sun, 1973, Determination of Seismic Source Parameters from Frequency Dependent Rayleigh and Love Wave Radiation Patterns; In Preparation.
- Unger, R., 1973, Selection of Reference Waveforms for Matched Filter Processing of Long Period Signals from Seismic Events; Special Report No. 5, AFTAC Contract No. F33657-72-C-0725, Texas Instruments Incorporated, Dallas, Texas.
- von Seggern, D. H., 1972, Seismic Shear Waves as a Discriminate Between Earthquakes and Underground Nuclear Explosions; Seismic Data Laboratory, Report No. 295, Teledyne Geotech.
- Wirth, M. H., 1971, Computation of Multiple-Event Probabilities; Seismic Data Laboratory, Report No. 277, Teledyne Geotech.

APPENDIX II-A
EVENT LIST

II-A-1

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT | | | COORDINATES | | | MR | SEISMIC AREA |
|-------|-------|----------|-------------|-------|-----|----|-------------------------|
| NO. | DATE | O.T. | LAT | LONG | | | |
| 0001 | 01/01 | 15.04.19 | 59.7 | 154.8 | 4.1 | L | E SIBERIA |
| 0002 | 01/01 | 16.55.06 | 50.7 | 155.8 | 4.6 | L | KURIL IS |
| 0003 | 01/01 | 18.13.54 | 49.4 | 156.5 | 4.0 | L | KURIL IS |
| 0004 | 01/02 | 05.37.25 | 46.1 | 146.2 | 4.0 | L | N W OF KURIL IS |
| 0005 | 01/02 | 09.17.53 | 37.9 | 20.7 | 4.2 | P | IONIAN SEA |
| 0006 | 01/02 | 10.27.35 | 41.8 | 84.5 | 5.2 | P | S SINKIANG PROV. |
| 0007 | 01/03 | 06.36.28 | 51.6 | 159.4 | 4.8 | P | OFF E COAST KAMCHATKA |
| 0008 | 01/03 | 19.26.42 | 52.0 | 159.0 | 4.5 | N | NEAR E COAST KAMCHATKA |
| 0009 | 01/03 | 23.40.37 | 58.8 | 130.9 | 3.4 | L | E RUSSIA |
| 0010 | 01/04 | 02.29.18 | 55.6 | 161.2 | 4.2 | L | NEAR E COAST KAMCHATKA |
| 0011 | 01/04 | 05.08.49 | 22.4 | 122.0 | 4.8 | P | TAIWAN REGION |
| 0012 | 01/04 | 10.42.31 | 55.6 | 163.8 | 4.4 | L | OFF E COAST KAMCHATKA |
| 0013 | 01/04 | 12.15.17 | 22.4 | 122.2 | 4.8 | P | TAIWAN |
| 0014 | 01/04 | 12.16.39 | 37.4 | 129.2 | 3.9 | L | S KOREA |
| 0015 | 01/04 | 13.13.01 | 60.0 | 101.7 | 3.9 | L | CENTRAL RUSSIA |
| 0016 | 01/05 | 02.16.10 | 43.8 | 147.2 | 4.5 | P | KURIL IS |
| 0017 | 01/05 | 04.57.41 | 47.8 | 16.2 | 4.0 | P | AUSTRIA |
| 0018 | 01/05 | 12.02.54 | 37.8 | 73.1 | 4.5 | L | TADZHIK SSR |
| 0019 | 01/05 | 14.26.48 | 56.6 | 169.4 | 4.0 | L | KOMANDORSKY IS |
| 0020 | 01/05 | 16.09.50 | 57.3 | 160.5 | 3.9 | L | KAMCHATKA |
| 0021 | 01/06 | 06.30.35 | 40.7 | 72.4 | 4.7 | P | KIRGIZ SSR |
| 0022 | 01/06 | 06.33.34 | 23.2 | 123.4 | 4.7 | P | TAIWAN |
| 0023 | 01/06 | 09.41.22 | 30.2 | 50.5 | 5.2 | P | IRAN |
| 0024 | 01/07 | 08.04.05 | 37.0 | 72.0 | 3.9 | N | AFGHANISTAN USSR BORDER |
| 0025 | 01/07 | 20.37.22 | 44.1 | 45.1 | 4.2 | L | SW RUSSIA |
| 0026 | 01/08 | 05.35.42 | 22.0 | 119.0 | 4.7 | N | TAIWAN REGION |
| 0027 | 01/08 | 14.32.27 | 23.0 | 119.0 | 4.6 | N | TAIWAN REGION |
| 0028 | 01/09 | 03.23.06 | 54.4 | 164.4 | 3.6 | L | KOMANDORSKY |
| 0029 | 01/09 | 14.00.59 | 55.7 | 163.6 | 4.3 | L | OFF E COAST KAMCHATKA |
| 0030 | 01/09 | 14.47.46 | 45.1 | 148.4 | 3.8 | L | KURIL IS |
| 0031 | 01/10 | 05.23.52 | 20.9 | 120.4 | 5.0 | P | PHILIPINE ISLANDS |
| 0032 | 01/10 | 13.56.55 | 55.7 | 163.7 | 4.4 | P | OFF E COAST KAMCHATKA |
| 0033 | 01/11 | 08.54.34 | 54.7 | 168.2 | 3.9 | L | KOMANDORSKY |
| 0034 | 01/11 | 15.46.45 | 43.4 | 147.8 | 4.0 | L | KURIL IS |
| 0035 | 01/12 | 06.36.28 | 37.7 | 30.0 | 4.4 | L | TURKEY |
| 0036 | 01/12 | 13.51.20 | 35.0 | 23.5 | 4.9 | P | CRETE |
| 0037 | 01/12 | 20.20.15 | 55.6 | 163.9 | 4.8 | P | OFF E COAST KAMCHATKA |
| 0038 | 01/12 | 20.27.39 | 55.5 | 163.6 | 4.0 | L | OFF E COAST KAMCHATKA |
| 0039 | 01/13 | 17.24.07 | 61.9 | 147.1 | 5.2 | P | E SIBERIA |
| 0040 | 01/14 | 03.20.20 | 67.5 | 171.5 | 3.9 | P | CHUKCHI SEA |
| 0041 | 01/14 | 22.10.04 | 32.9 | 46.9 | 5.1 | P | IRAN-IRAQ BORDER REGION |
| 0042 | 01/15 | 00.58.23 | 49.6 | 155.0 | 3.9 | L | KURIL IS |
| 0043 | 01/15 | 18.07.58 | 57.4 | 120.7 | 4.7 | P | E RUSSIA |
| 0044 | 01/15 | 20.21.50 | 40.3 | 79.0 | 5.4 | P | S. SINKIANG PROVINCE |
| 0045 | 01/15 | 20.45.22 | 39.3 | 79.9 | 4.6 | L | S SINKIANG PROV |
| 0046 | 01/16 | 04.38.16 | 55.6 | 162.5 | 3.8 | L | NEAR E COAST KAMCHATKA |
| 0047 | 01/16 | 11.00.49 | 55.6 | 163.2 | 3.9 | L | OFF E COAST KAMCHATKA |
| 0048 | 01/17 | 05.54.20 | 34.5 | 26.5 | 4.1 | L | CRETE |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT | | O.T. | COORDINATES | | MR | | SEISMIC AREA |
|-------|-------|----------|-------------|-------|-----|---|--------------------------|
| NO. | DATE | | LAT | LONG | | | |
| 0049 | 01/18 | 14.02.01 | 44.6 | 149.1 | 4.8 | P | KURIL IS REGION |
| 0050 | 01/18 | 21.12.02 | 37.5 | 49.7 | 4.9 | P | NW IRAN |
| 0051 | 01/18 | 23.26.12 | 44.2 | 8.2 | 4.1 | P | N ITALY |
| 0052 | 01/20 | 02.15.07 | 36.6 | 27.1 | 4.8 | P | DODECANESE ISLANDS |
| 0053 | 01/21 | 23.30.46 | 43.2 | 45.2 | 3.8 | L | E CAUCASUS |
| 0054 | 01/22 | 01.41.24 | 50.0 | 152.0 | 4.2 | N | NW KURIL IS |
| 0055 | 01/22 | 17.17.31 | 37.6 | 29.9 | 4.4 | P | TURKEY |
| 0056 | 01/23 | 08.30.47 | 52.0 | 158.0 | 4.2 | N | NE COAST KAMCHATKA |
| 0057 | 01/24 | 05.00.37 | 55.8 | 162.6 | 4.0 | L | NEAR E COAST KAMCHATKA |
| 0058 | 01/24 | 12.39.29 | 51.7 | 158.0 | 4.0 | L | NEAR E COAST KAMCHATKA |
| 0059 | 01/25 | 10.02.40 | 53.9 | 160.9 | 4.6 | P | NEAR E COAST KAMCHATKA |
| 0060 | 01/25 | 20.24.39 | 43.8 | 13.4 | 4.5 | P | CENTRAL ITALY |
| 0061 | 01/25 | 21.03.00 | 22.5 | 122.2 | 4.8 | P | TAIWAN |
| 0062 | 01/25 | 23.00.39 | 22.2 | 122.4 | 4.6 | P | TAIWAN REGION |
| 0063 | 01/25 | 23.22.17 | 43.8 | 13.4 | 4.8 | P | CENTRAL ITALY |
| 0064 | 01/26 | 04.34.27 | 54.0 | 156.9 | 4.1 | L | KAMCHATKA |
| 0065 | 01/26 | 09.14.16 | 55.8 | 164.7 | 3.8 | L | KOMANDORSKY |
| 0066 | 01/26 | 09.20.17 | 48.9 | 155.9 | 4.1 | L | KURILE IS |
| 0067 | 01/26 | 12.11.11 | 47.1 | 141.5 | 3.2 | L | SAKHALIN |
| 0068 | 01/26 | 12.54.39 | 34.5 | 25.5 | 4.0 | I | CRETE |
| 0069 | 01/26 | 15.56.27 | 48.9 | 155.9 | 4.8 | L | KURILE IS |
| 0070 | 01/27 | 14.06.46 | 55.4 | 163.6 | 3.8 | I | OFF E COAST KAMCHATKA |
| 0071 | 01/27 | 20.37.28 | 55.7 | 162.3 | 3.8 | L | NEAR E COAST KAMCHATKA |
| 0072 | 01/28 | 04.22.28 | 27.5 | 126.5 | 4.4 | L | E CHINA SEA |
| 0073 | 01/28 | 10.26.54 | 26.6 | 66.2 | 5.5 | P | WEST PAKISTAN |
| 0074 | 01/28 | 13.37.28 | 15.0 | 47.0 | 4.0 | N | W ARABIAN PENINSULA |
| 0075 | 01/28 | 20.29.04 | 40.8 | 81.4 | 4.5 | L | S SINKIANG PROV |
| 0076 | 01/28 | 20.29.19 | 43.0 | 78.0 | 4.4 | N | KIRGIZ PROV |
| 0077 | 01/28 | 21.54.04 | 45.0 | 136.0 | 4.0 | N | NEAR E COAST OF E RUSSIA |
| 0078 | 01/28 | 23.42.51 | 49.3 | 157.3 | 3.8 | L | KURIL IS REGION |
| 0079 | 01/29 | 06.49.11 | 32.9 | 76.0 | 4.7 | P | KASHMIR-INDIA REGION |
| 0080 | 01/29 | 09.50.58 | 29.0 | 62.0 | 3.9 | N | S. IRAN |
| 0081 | 01/30 | 03.56.41 | 40.9 | 120.2 | 3.9 | L | NE CHINA |
| 0082 | 02/01 | 10.16.09 | 55.8 | 162.8 | 4.1 | L | E. COAST KAMCHATKA |
| 0083 | 02/01 | 17.06.25 | 59.2 | 155.7 | 3.6 | I | EASTERN SIBERIA |
| 0084 | 02/02 | 04.26.59 | 55.7 | 162.0 | 3.7 | L | EAST COAST OF KAMCHATKA |
| 0085 | 02/02 | 05.58.51 | 46.8 | 146.4 | 3.6 | L | NW KURIL IS |
| 0086 | 02/02 | 17.56.39 | 50.7 | 160.1 | 3.6 | L | KURIL IS |
| 0087 | 02/02 | 21.19.49 | 38.9 | 21.2 | 4.6 | P | GREECE |
| 0088 | 02/03 | 02.29.22 | 40.7 | 48.4 | 5.1 | P | E CAUCASUS |
| 0089 | 02/03 | 07.22.49 | 23.4 | 102.4 | 4.5 | P | YUANNAN PROVINCE CHINA |
| 0090 | 02/04 | 02.42.19 | 43.8 | 13.3 | 4.8 | P | CENTRAL ITALY |
| 0091 | 02/04 | 03.34.56 | 51.4 | 118.0 | 4.2 | L | E LAKE BAICAL |
| 0092 | 02/04 | 04.40.50 | 43.9 | 13.2 | 4.8 | P | CENTRAL ITALY |
| 0093 | 02/04 | 07.51.14 | 48.3 | 154.2 | 4.8 | L | KURIL IS |
| 0094 | 02/04 | 09.18.32 | 43.9 | 13.2 | 4.4 | P | CENTRAL ITALY |
| 0095 | 02/04 | 14.08.22 | 30.4 | 64.6 | 5.2 | P | TIBET |
| 0096 | 02/04 | 16.33.24 | 14.0 | 51.0 | 4.5 | N | EAST ARABIAN PENINSULA |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT | | | COORDINATES | | MB | SEISMIC AREA |
|-------|-------|----------|-------------|-------|-----|---------------------------------|
| NO. | DATE | O.T. | LAT | LONG | | |
| 0097 | 02/04 | 17.19.52 | 43.8 | 13.3 | 4.4 | P CENTRAL ITALY |
| 0098 | 02/04 | 18.17.30 | 43.8 | 13.4 | 4.8 | P CENTRAL ITALY |
| 0099 | 02/04 | 19.02.56 | 43.8 | 13.3 | 4.8 | P CENTRAL ITALY |
| 0100 | 02/04 | 19.03.08 | 45.1 | 13.2 | 3.6 | L NORTHERN ITALY |
| 0101 | 02/05 | 01.26.23 | 43.8 | 13.3 | 4.8 | P CENTRAL ITALY |
| 0102 | 02/05 | 03.49.45 | 43.2 | 13.7 | 4.4 | P CENTRAL ITALY |
| 0103 | 02/05 | 05.05.51 | 43.7 | 13.5 | 4.6 | P CENTRAL ITALY |
| 0104 | 02/05 | 07.08.13 | 43.9 | 13.3 | 4.7 | P CENTRAL ITALY |
| 0105 | 02/05 | 15.14.48 | 43.7 | 13.4 | 4.7 | P CENTRAL ITALY |
| 0106 | 02/06 | 01.34.22 | 44.0 | 13.2 | 4.9 | P ADRIATIC SEA |
| 0107 | 02/06 | 04.29.05 | 29.0 | 89.0 | 4.1 | N TIBET |
| 0108 | 02/06 | 07.30.11 | 41.6 | 82.2 | 4.7 | P S SINKIANG PROV. CHINA |
| 0109 | 02/06 | 08.03.43 | 46.0 | 80.0 | 4.3 | N EASTERN KAZKH |
| 0110 | 02/06 | 21.44.29 | 43.8 | 13.2 | 4.4 | P CENTRAL ITALY |
| 0111 | 02/07 | 07.49.48 | 52.3 | 160.1 | 4.8 | P OFF E COAST OF KAMCHATKA |
| 0112 | 02/08 | 03.37.52 | 19.3 | 122.0 | 5.7 | P PHILIPPINE ISLANDS |
| 0113 | 02/08 | 12.19.15 | 43.8 | 13.3 | 4.6 | P CENTRAL ITALY |
| 0114 | 02/08 | 15.42.55 | 22.7 | 122.6 | 4.8 | P TAIWAN REGION |
| 0115 | 02/09 | 14.21.51 | 29.4 | 50.8 | 4.3 | P SOUTHERN IRAN |
| 0116 | 02/10 | 05.02.57 | 50.0 | 78.9 | 5.5 | P EASTERN KAZAKH SSR |
| 0117 | 02/10 | 06.49.16 | 29.7 | 50.9 | 4.5 | P SOUTHERN IRAN |
| 0118 | 02/10 | 09.04.09 | 29.6 | 50.9 | 3.9 | P SOUTHERN IRAN |
| 0119 | 02/10 | 16.40.16 | 29.5 | 50.9 | 4.1 | P SOUTHERN IRAN |
| 0120 | 02/11 | 05.55.46 | 39.9 | 77.4 | 4.9 | P SOUTHERN SINKIANG PROV CHINA |
| 0121 | 02/11 | 12.20.43 | 29.0 | 87.0 | 4.3 | N TIBET |
| 0122 | 02/11 | 13.58.49 | 55.5 | 165.2 | 3.9 | L KORMANDORSKY |
| 0123 | 02/11 | 21.36.17 | 56.1 | 162.9 | 4.6 | P NEAR E COAST OF KAMCHATKA |
| 0124 | 02/13 | 05.24.57 | 43.5 | 147.0 | 3.8 | L KURIL IS |
| 0125 | 02/13 | 13.07.11 | 37.1 | 24.0 | 4.5 | P SOUTHERN GREECE |
| 0126 | 02/13 | 22.36.54 | 55.2 | 165.5 | 3.9 | L KORMANDORSKY |
| 0127 | 02/15 | 16.45.22 | 45.0 | 153.0 | 4.1 | L KURIL IS |
| 0128 | 02/16 | 00.42.24 | 36.9 | 24.2 | 4.5 | P SOUTHERN GREECE |
| 0129 | 02/16 | 23.19.20 | 41.7 | 80.7 | 4.8 | P SOUTHERN SINKIANG PROV. CHINA |
| 0130 | 02/18 | 14.30.23 | 46.6 | 151.0 | 3.7 | L KURIL IS |
| 0131 | 02/18 | 18.07.34 | 43.6 | 147.8 | 4.7 | P KURIL IS |
| 0132 | 02/19 | 06.48.12 | 55.1 | 161.5 | 4.0 | L NEAR EAST COAST KAMCHATKA |
| 0133 | 02/19 | 13.19.25 | 44.4 | 149.1 | 5.2 | P KURIL IS. |
| 0134 | 02/19 | 13.54.46 | 44.6 | 149.1 | 5.4 | P KURIL IS. |
| 0135 | 02/20 | 05.09.15 | 30.7 | 73.1 | 3.9 | I INDIA WEST PAKISTAN BORDER |
| 0136 | 02/20 | 10.08.47 | 47.9 | 145.9 | 4.2 | I SEA OF OKHOTSK (D=397 KM) |
| 0137 | 02/20 | 10.22.46 | 38.5 | 90.5 | 3.9 | I S. SINKIANG PROV. (D=16KM) |
| 0138 | 02/20 | 20.06.11 | 50.8 | 141.5 | 4.1 | I SAKHALIN ISLAND |
| 0139 | 02/21 | 22.00.59 | 54.4 | 161.3 | 4.8 | I NEAR E COAST KAMCHATKA |
| 0140 | 02/21 | 23.02.56 | 41.0 | 22.3 | 4.0 | I YUGOSLAVIA |
| 0141 | 02/22 | 01.14.48 | 36.4 | 70.6 | 5.3 | I HINDU KUSH REGION (D=212 KM) |
| 0142 | 02/22 | 01.53.36 | 49.0 | 115.0 | 4.1 | I USSR MONGOLIA BORDER |
| 0143 | 02/22 | 03.38.29 | 56.0 | 156.0 | 3.4 | I KAMCHATKA |
| 0144 | 02/22 | 08.14.26 | 36.6 | 68.6 | 4.0 | I HINDU KUSH REGION |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT | | O.T. | COORDINATES | | MR | SEISMIC AREA |
|-------|-------|----------|-------------|-------|-----|---------------------------------|
| NO. | DATE | | LAT | LONG | | |
| 0145 | 02/23 | 03.07.04 | 43.7 | 148.4 | 4.8 | I KURILE IS REGION (D=41 KM) |
| 0146 | 02/23 | 03.21.31 | 44.2 | 148.4 | 4.7 | I KURILE ISLANDS (D=40 KM) |
| 0147 | 02/23 | 03.42.41 | 43.9 | 148.3 | 4.9 | I KURILE IS REGION (D=39 KM) |
| 0148 | 02/23 | 05.11.09 | 45.0 | 150.0 | 3.7 | I KURILE IS |
| 0149 | 02/23 | 09.46.50 | 86.0 | 139.0 | 3.7 | I LOMONOSOV RIDGE |
| 0150 | 02/23 | 12.55.32 | 36.8 | 71.5 | 3.8 | I AFGHAN-USSR BORDER (D=177 KM) |
| 0151 | 02/23 | 14.00.49 | 38.1 | 71.7 | 4.3 | I AFGHAN-USSR BORDER |
| 0152 | 02/23 | 19.37.29 | 55.0 | 163.0 | 3.7 | I OFF E COAST KAMCHATKA |
| 0153 | 02/24 | 00.38.00 | 54.0 | 156.0 | 4.5 | I KAMCHATKA |
| 0154 | 02/24 | 01.50.05 | 52.0 | 139.0 | 3.7 | I NEAR EAST COAST OF SIBERIA |
| 0155 | 02/24 | 10.14.02 | 46.9 | 153.8 | 3.7 | I KURILE ISLANDS |
| 0156 | 02/24 | 10.19.37 | 48.8 | 155.7 | 5.0 | I KURILE ISLANDS |
| 0157 | 02/24 | 10.26.51 | 49.0 | 155.0 | 3.6 | I KURILE IS |
| 0158 | 02/24 | 10.39.23 | 52.3 | 161.9 | 4.3 | I OFF KAMCHATKA |
| 0159 | 02/24 | 12.17.39 | 52.0 | 150.0 | 3.8 | I SEA OF OKHOTSK |
| 0160 | 02/24 | 12.24.54 | 49.0 | 155.0 | 3.7 | I KURILE IS |
| 0161 | 02/24 | 18.17.34 | 49.0 | 159.0 | 3.5 | I KURILE IS REGION |
| 0162 | 02/25 | 19.59.29 | 46.0 | 147.0 | 3.8 | I NW OF KURILE IS |
| 0163 | 02/25 | 22.34.49 | 50.0 | 39.0 | 3.7 | I W RUSSIA |
| 0164 | 02/25 | 22.43.07 | 49.2 | 156.0 | 4.0 | I KURILE ISLANDS |
| 0165 | 02/26 | 02.12.57 | 49.2 | 156.2 | 4.9 | I KURILE ISLANDS |
| 0166 | 02/26 | 02.11.46 | 31.2 | 69.2 | 3.9 | I WEST PAKISTAN |
| 0167 | 02/26 | 05.58.22 | 46.8 | 152.6 | 4.9 | I KURILE ISLANDS |
| 0168 | 02/26 | 09.04.32 | 55.0 | 162.0 | 3.3 | I NEAR E COAST KAMCHATKA |
| 0169 | 02/26 | 15.06.42 | 53.3 | 138.7 | 3.8 | I NEAR EAST COAST OF SIBERIA |
| 0170 | 02/26 | 18.32.26 | 51.0 | 149.0 | 4.0 | I SEA OF OKHOTSK |
| 0171 | 02/26 | 18.56.13 | 27.1 | 100.9 | 4.7 | I YUNNAN PROV., CHINA |
| 0172 | 02/26 | 23.31.10 | 50.6 | 57.3 | 5.3 | I USSR-MONGOLIA BORDER |
| 0173 | 02/27 | 08.42.55 | 88.0 | -74.0 | 3.3 | I LOMONOSOV RIDGE |
| 0174 | 02/27 | 08.48.08 | 89.0 | 15.0 | 3.3 | I LOMONOSOV RIDGE |
| 0175 | 02/27 | 10.03.03 | 87.0 | 53.5 | 4.9 | I N. OF FRANZ JOSEF LAND |
| 0176 | 02/27 | 10.08.16 | 76.0 | 119.0 | 4.1 | I LAPTEV SEA |
| 0177 | 02/27 | 11.03.19 | 90.0 | -95.0 | 3.5 | I LOMONOSOV RIDGE |
| 0178 | 02/27 | 14.58.32 | 52.0 | 156.7 | 4.5 | I KAMCHATKA (D=66 KM) |
| 0179 | 02/27 | 17.50.25 | 86.2 | 77.2 | 4.4 | I N. OF SEVERNAYA ZEMLYA |
| 0180 | 02/27 | 19.57.43 | 26.3 | 121.0 | 4.0 | I TAIWAN REGION |
| 0181 | 02/27 | 22.15.03 | 55.0 | 92.2 | 4.5 | I CENTRAL RUSSIA |
| 0182 | 02/28 | 01.04.22 | 46.0 | 148.0 | 4.2 | I NW OF KURILE IS |
| 0183 | 02/28 | 05.18.56 | 36.7 | 71.4 | 4.2 | I AFGHAN-USSR BORDER |
| 0184 | 02/28 | 11.35.31 | 56.0 | 163.0 | 4.1 | I NEAR EAST COAST OF KAMCHATKA |
| 0185 | 02/28 | 14.49.55 | 54.1 | 160.7 | 3.3 | I NEO KAMCHATKA |
| 0186 | 02/28 | 15.44.20 | 51.8 | 50.2 | 3.9 | I CENTRAL RUSSIA |
| 0187 | 02/28 | 16.24.08 | 31.8 | 50.1 | 3.6 | I IRAN |
| 0188 | 02/28 | 16.26.57 | 31.8 | 50.1 | 3.7 | I IRAN |
| 0189 | 02/28 | 16.44.58 | 29.5 | 50.7 | 4.4 | I SOUTHERN IRAN (D=55 KM) |
| 0190 | 02/28 | 17.22.55 | 31.2 | 50.1 | 4.2 | I IRAN |
| 0191 | 02/28 | 17.32.29 | 43.4 | 132.2 | 4.5 | I NEO EASTERN RUSSIA (D=457 KM) |
| 0192 | 02/28 | 18.08.52 | 31.2 | 48.6 | 3.8 | I W IRAN |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT | | | COORDINATES | | MB | SEISMIC AREA |
|-------|-------|----------|-------------|-------|-----|---------------------------------|
| NO. | DATE | T.T. | LAT | LONG | | |
| 0193 | 02/28 | 18.12.35 | 36.0 | 68.7 | 4.4 | I HINDU KUSH |
| 0194 | 02/28 | 18.44.54 | 29.8 | 50.7 | 4.7 | I SOUTHERN IRAN (D=25 KM) |
| 0195 | 02/28 | 18.47.45 | 27.2 | 53.5 | 3.9 | I S IRAN |
| 0196 | 02/28 | 18.59.55 | 30.3 | 50.1 | 3.7 | I IRAN |
| 0197 | 02/28 | 19.02.50 | 34.2 | 47.4 | 3.9 | I W IRAN |
| 0198 | 02/28 | 19.04.08 | 32.3 | 50.4 | 3.4 | I IRAN |
| 0199 | 02/28 | 19.04.57 | 32.3 | 50.4 | 3.3 | I IRAN |
| 0200 | 02/28 | 19.06.57 | 28.2 | 51.2 | 4.4 | I SOUTHERN IRAN |
| 0201 | 02/28 | 19.22.14 | 31.9 | 50.4 | 3.6 | I IRAN |
| 0202 | 02/28 | 19.28.48 | 31.2 | 51.1 | 3.7 | I IRAN |
| 0203 | 02/28 | 19.29.00 | 33.7 | 48.4 | 3.8 | I WESTERN IRAN |
| 0204 | 02/28 | 19.32.19 | 31.3 | 49.7 | 4.2 | I WESTERN IRAN |
| 0205 | 02/28 | 20.04.00 | 56.1 | 164.2 | 3.6 | I KOMANDORSKY ISLANDS |
| 0206 | 02/28 | 23.01.26 | 29.8 | 50.4 | 4.2 | I SOUTHERN IRAN |
| 0207 | 02/28 | 23.06.24 | 30.0 | 52.2 | 4.0 | I IRAN |
| 0208 | 02/28 | 23.30.24 | 29.2 | 50.5 | 4.1 | I SOUTHERN IRAN |
| 0209 | 02/28 | 23.38.32 | 27.9 | 56.8 | 3.7 | I SOUTHERN IRAN |
| 0210 | 02/29 | 08.02.51 | 22.8 | 46.6 | 4.0 | I IRAN-IRAQ BORDER |
| 0211 | 02/29 | 08.07.20 | 99.0 | -51.0 | 3.4 | I LOMONOSOV RIDGE |
| 0212 | 02/29 | 10.47.15 | 56.0 | 164.0 | 4.2 | I KOMANDORSKY IS REGION |
| 0213 | 02/29 | 11.22.49 | 29.1 | 49.7 | 4.0 | I PERSIAN GULF |
| 0214 | 02/29 | 19.47.58 | 39.0 | 74.0 | 4.0 | I S SINKIANG PROV |
| 0215 | 02/29 | 23.42.40 | 55.6 | 162.2 | 4.1 | I OFF KAMCHATKA |
| 0216 | 03/01 | 04.26.46 | 53.0 | 160.0 | 3.7 | I NEAR E COAST KAMCHATKA |
| 0217 | 03/01 | 05.06.22 | 27.0 | 89.0 | 3.9 | I BHUTAN |
| 0218 | 03/01 | 09.51.19 | 87.0 | 99.0 | 3.7 | I N OF SEVERNAYA ZEMLYA |
| 0219 | 03/01 | 10.25.19 | 55.0 | 163.0 | 3.4 | I OFF EAST COAST OF KAMCHATKA |
| 0220 | 03/01 | 16.58.59 | 51.0 | 162.0 | 3.5 | I OFF EAST COAST OF KAMCHATKA |
| 0221 | 03/01 | 22.30.03 | 41.6 | 23.7 | 3.6 | I GREECE-BULGARIA BORDER |
| 0222 | 03/02 | 06.17.29 | 53.0 | 167.0 | 3.6 | I KOMANDORSKY IS REGION |
| 0223 | 03/02 | 12.48.48 | 72.4 | 2.3 | 4.5 | I NORWEGIAN SEA |
| 0224 | 03/02 | 14.10.13 | 31.6 | 42.1 | 4.0 | I IRAQ |
| 0225 | 03/02 | 19.57.42 | 43.0 | 76.0 | 3.5 | I ALMA ATA REGION |
| 0226 | 03/02 | 23.09.10 | 44.9 | 148.1 | 4.6 | I KURILE ISLANDS (D=150 KM) |
| 0227 | 03/03 | 00.39.23 | 53.0 | 159.2 | 4.1 | I NEC KAMCHATKA |
| 0228 | 03/03 | 02.13.11 | 46.6 | 150.6 | 4.6 | I KURILE ISLANDS (D=136 KM) |
| 0229 | 03/03 | 05.26.53 | 77.8 | 116.7 | 3.8 | I LAPTEV SEA |
| 0230 | 03/03 | 08.13.55 | 55.8 | 163.9 | 4.1 | I OFF KAMCHATKA |
| 0231 | 03/03 | 20.39.57 | 45.4 | 147.2 | 4.2 | I KURILE ISLANDS |
| 0232 | 03/03 | 21.26.51 | 44.7 | 18.4 | 4.5 | I YUGOSLAVIA (D=32 KM) |
| 0233 | 03/03 | 23.10.41 | 50.2 | 155.7 | 4.5 | I KURILE ISLANDS |
| 0234 | 03/04 | 02.53.56 | 45.9 | 153.2 | 4.3 | I KURILE ISLANDS |
| 0235 | 03/04 | 04.00.09 | 40.2 | 79.0 | 4.5 | I SOUTHERN SINKIANG PROV. |
| 0236 | 03/04 | 08.22.16 | 42.1 | 83.3 | 4.4 | I N. SINKIANG PROV. |
| 0237 | 03/04 | 14.42.05 | 41.0 | 21.0 | 3.6 | I YUGOSLAVIA |
| 0238 | 03/04 | 18.24.11 | 38.3 | 74.0 | 5.1 | I S. SINKIANG PROV. (D=130 KM) |
| 0239 | 03/04 | 19.27.57 | 36.8 | 71.4 | 4.0 | I AFGHAN-USSR BORDER (D=227 KM) |
| 0240 | 03/05 | 19.07.43 | 21.0 | 73.0 | 4.0 | I INDIA |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

Reproduced from
best available copy.

| EVENT NO. | DATE | O.T. | COORDINATES | | MB | SEISMIC AREA |
|--------------|-------|----------|-------------|--------|-----|---------------------------------|
| | | | LAT | LONG | | |
| 0241 | 03/06 | 06.05.08 | 53.5 | 160.9 | 3.9 | I KAMCHATKA |
| 0242 | 03/06 | 09.59.09 | 45.0 | 150.0 | 3.7 | I KURILE ISLANDS |
| 0243 | 03/06 | 18.50.18 | 50.2 | 148.8 | 5.4 | I SEA OF OKHOTSK (D=502 KM) |
| 0244 | 03/06 | 19.13.25 | 56.0 | 140.0 | 4.2 | I SEA OF OKHOTSK |
| 0245 | 03/06 | 23.17.53 | 40.0 | 103.0 | 4.5 | I NORTHERN CHINA |
| 0246 | 03/07 | 01.14.04 | 35.0 | 69.0 | 4.0 | I HINDU KUSH REGION (D=200 KM) |
| 0247 | 03/07 | 05.21.21 | 43.0 | 21.0 | 2.7 | I YUGOSLAVIA |
| 0248 | 03/07 | 07.09.49 | 28.0 | 56.0 | 4.0 | I SOUTHERN IRAN |
| 0249 | 03/07 | 12.03.00 | 21.0 | 90.0 | 0.0 | I EAST PAKISTAN |
| 0250 | 03/07 | 16.46.25 | 23.3 | 94.9 | 4.3 | I BURMA-INDIA BORDER (D=140 KM) |
| 0251 | 03/08 | 02.38.11 | 51.2 | 151.9 | 4.2 | I SEA OF OKHOTSK |
| 0252 | 03/08 | 03.51.24 | 49.0 | 157.0 | 4.0 | I KURILE IS REGION |
| 0253 | 03/08 | 03.55.22 | 34.0 | 83.0 | 3.8 | I TIBET |
| 0254 | 03/08 | 15.55.14 | 48.2 | 148.2 | 4.2 | I NW OF KURILE IS. (D=204 KM) |
| 0255 | 03/08 | 21.49.11 | 27.6 | 56.7 | 4.9 | I SOUTHERN IRAN (D=45 KM) |
| 0256 | 03/08 | 22.04.02 | 40.8 | 22.8 | 3.5 | I BULGARIA |
| 0257 | 03/09 | 09.13.56 | 51.0 | 157.0 | 3.3 | I NEAR E COAST OF KAMCHATKA |
| 0258 | 03/09 | 23.24.05 | 47.0 | 151.0 | 3.0 | I KURILE IS |
| 0259 | 03/09 | 23.46.18 | 53.0 | 162.0 | 3.6 | I OFF E COAST OF KAMCHATKA |
| 0260 | 03/10 | 04.56.57 | 49.8 | 78.2 | 5.5 | I EASTERN KAZAKH SSR (D=0KM) |
| 0261 | 03/10 | 06.50.18 | 45.1 | 149.5 | 3.7 | I KURILE ISLANDS |
| 0262 | 03/10 | 14.36.17 | 33.8 | 72.7 | 4.4 | I WEST PAKISTAN (D=45 KM) |
| 0263 | 03/10 | 15.07.30 | 50.0 | 11.0 | 3.8 | I GERMANY |
| 0264 | 03/10 | 17.44.32 | 55.4 | 164.2 | 3.8 | I KOMANDORSKY ISLANDS |
| 0265 | 03/11 | 03.28.59 | 38.0 | 70.0 | 4.2 | I AFGHANISTAN-USSR BORDER |
| 0266 | 03/11 | 06.47.07 | 82.7 | 142.3 | 3.6 | I LOMONOSOV RIDGE |
| 0267 | 03/11 | 13.31.39 | 35.0 | 76.0 | 4.1 | I EASTERN KASHMIR |
| 0268 | 03/12 | 02.04.21 | 45.0 | 155.0 | 4.1 | I KURILE IS REGION |
| 0269 | 03/12 | 02.10.50 | 56.0 | 155.0 | 3.8 | I KAMCHATKA |
| 0270 | 03/12 | 17.31.12 | 27.9 | 53.4 | 4.1 | I SOUTHERN IRAN |
| 0271 | 03/13 | 02.11.05 | 49.0 | 158.0 | 3.8 | I KURILE IS REGION |
| 0272 | 03/13 | 05.49.13 | 37.0 | 70.0 | 4.0 | I AFGHANISTAN-USSR BORDER |
| 0273 | 03/13 | 09.23.29 | 29.3 | 25.6 | 2.8 | I AEGEAN SEA (D=42 KM) |
| 0274 | 03/13 | 13.28.33 | 54.9 | 165.6 | 4.0 | I KOMANDORSKY ISLANDS |
| 0275 | 03/13 | 18.27.07 | 34.0 | 83.0 | 4.1 | I TIBET |
| 0276 | 03/14 | 00.40.23 | 17.0 | 94.0 | 3.7 | I BURMA |
| 0277 | 03/14 | 02.43.37 | 44.0 | -116.0 | 3.7 | I WESTERN IDANG |
| 0278 | 03/14 | 14.05.46 | 39.3 | 29.4 | 5.4 | I TURKEY |
| 0279 | 03/14 | 15.47.51 | 39.0 | 126.0 | 3.7 | I N KOREA |
| 0280 | 03/15 | 00.21.25 | 39.5 | 72.3 | 3.7 | I TADZHIK (D=140 KM) |
| 0281 | 03/15 | 06.00.33 | 30.4 | 84.5 | 5.3 | I TIBET |
| 0282 | 03/15 | 12.08.01 | 39.0 | 30.0 | 3.7 | I TURKEY |
| 0283 | 03/16 | 00.04.32 | 39.0 | 105.0 | 3.7 | I NORTHERN CHINA |
| 0284 | 03/16 | 00.48.05 | 25.7 | 55.7 | 3.6 | I EASTERN ARABIAN PENINSULA |
| 0285 | 03/16 | 02.59.06 | 33.2 | 71.0 | 3.5 | I WEST PAKISTAN |
| 0286 | 03/16 | 05.22.55 | 52.2 | 152.2 | 4.5 | I NW OF KURILE IS. (D=435 KM) |
| 0287 | 03/16 | 06.35.40 | 27.2 | 57.9 | 3.8 | I SOUTHERN IRAN |
| 0288 | 03/16 | 07.52.51 | 36.4 | 82.5 | 3.4 | I SOUTHERN STAKIANG PROV |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT NO. | DATE | O.T. | COORDINATES | | MB | SEISMIC AREA |
|-----------|-------|----------|-------------|--------|-----|--------------------------------|
| | | | LAT | LONG | | |
| 0299 | 03/16 | 12.00.09 | 28.0 | 56.0 | 3.6 | I INDIA-CHINA BORDER REGION |
| 0290 | 03/16 | 21.11.35 | 38.0 | 82.0 | 3.5 | I SOUTHERN SINKIANG PROV |
| 0291 | 03/17 | 00.29.01 | 32.3 | -115.6 | 4.1 | I CALIF-MEXICO BORDER (D=8 KM) |
| 0292 | 03/17 | 07.49.02 | 49.0 | 156.2 | 5.2 | I KURILE ISLANDS |
| 0293 | 03/17 | 07.52.33 | 27.9 | 54.3 | 4.0 | I SOUTHERN IRAN |
| 0294 | 03/17 | 09.17.11 | 40.1 | 69.7 | 5.2 | I TADZHIK SSR (D=26 KM) |
| 0295 | 03/17 | 17.11.28 | 28.0 | 54.0 | 3.9 | I SOUTHERN IRAN |
| 0296 | 03/17 | 23.33.37 | 32.0 | 75.0 | 3.5 | I KASHMIR-INDIA BORDER |
| 0297 | 03/18 | 00.41.48 | 46.9 | 143.7 | 5.0 | I SAKHALIN ISLAND (D=405 KM) |
| 0298 | 03/18 | 07.11.55 | 47.0 | 81.0 | 3.6 | I EASTERN KAZAKH SSR |
| 0299 | 03/18 | 13.52.14 | 57.0 | 162.0 | 3.6 | I NEAR E COAST OF KAMCHATKA |
| 0300 | 03/18 | 18.29.33 | 50.6 | 156.7 | 4.7 | I KURILE ISLANDS |
| 0301 | 03/18 | 19.17.25 | 54.0 | 150.0 | 3.7 | I SEA OF OKHOTSK |
| 0302 | 03/18 | 19.54.18 | 41.0 | 72.0 | 3.2 | I KIRGIZ SSR |
| 0303 | 03/19 | 03.34.31 | 42.7 | 38.1 | 3.9 | I BLACK SEA |
| 0304 | 03/19 | 06.03.23 | 49.0 | 159.0 | 3.6 | I KURILE ISLANDS REGION |
| 0305 | 03/20 | 08.04.48 | 44.0 | 147.0 | 4.4 | I KURILE IS |
| 0306 | 03/20 | 10.54.35 | 38.0 | 73.0 | 3.9 | I TADZHIK SINKIANG BORDER |
| 0307 | 03/20 | 14.08.12 | 47.0 | 154.0 | 4.0 | I KURILE IS |
| 0308 | 03/20 | 20.08.31 | 30.0 | 61.0 | 3.4 | I SW AFGHANISTAN |
| 0309 | 03/20 | 21.47.55 | 40.0 | 80.0 | 3.4 | I SOUTHERN SINKIANG PROV |
| 0310 | 06/01 | 00.18.13 | 48.0 | 154.0 | 3.9 | L KURILE ISLANDS |
| 0311 | 06/01 | 01.23.26 | 52.0 | 70.0 | 3.6 | L CENTRAL KAZAKH SSR |
| 0312 | 06/01 | 11.22.15 | 44.0 | 103.0 | 3.7 | N MONGOLIA |
| 0313 | 06/01 | 13.44.11 | 39.0 | 24.0 | 4.1 | L GREECE |
| 0314 | 06/01 | 21.43.49 | 55.0 | 164.0 | 3.8 | L KOMANDORSKY ISLANDS |
| 0315 | 06/02 | 00.12.13 | 30.0 | 53.0 | 4.1 | N SOUTHERN IRAN |
| 0316 | 06/02 | 01.53.07 | 50.0 | 152.0 | 3.8 | L NW OF KURILE ISLANDS |
| 0317 | 06/02 | 04.21.49 | 42.0 | 82.0 | 3.8 | N SOUTHERN SINKIANG |
| 0318 | 06/02 | 04.22.16 | 42.0 | 82.0 | 3.7 | N SOUTHERN SINKIANG |
| 0319 | 06/02 | 05.11.13 | 43.0 | 81.0 | 3.5 | N KAZAKH-SINKIANG BORDER |
| 0320 | 06/02 | 06.30.49 | 42.0 | 81.0 | 3.9 | N SOUTHERN SINKIANG |
| 0321 | 06/02 | 16.49.22 | 36.0 | 92.0 | 3.7 | N TSINGHAI PROV., CHINA |
| 0322 | 06/02 | 20.32.55 | 28.4 | 55.9 | 4.3 | P CHINA-INDIA BORDER |
| 0323 | 06/03 | 02.16.51 | 23.5 | 125.5 | 5.2 | P SW RYUKYU ISLANDS |
| 0324 | 06/03 | 08.21.30 | 29.0 | 53.0 | 4.2 | N SOUTHERN IRAN |
| 0325 | 06/04 | 03.37.49 | 30.0 | 54.0 | 4.2 | N SOUTHERN IRAN |
| 0326 | 06/04 | 07.52.38 | 53.0 | 158.0 | 4.0 | L NEAR E COAST KAMCHATKA |
| 0327 | 06/04 | 12.57.32 | 53.0 | 169.0 | 3.4 | L KOMANDORSKY ISLANDS |
| 0328 | 06/04 | 13.02.07 | 54.0 | 165.0 | 3.5 | L KOMANDORSKY ISLANDS |
| 0329 | 06/04 | 16.29.34 | 39.4 | 26.2 | 4.1 | P TURKEY |
| 0330 | 06/04 | 23.22.18 | 33.0 | 97.0 | 3.5 | N TSINGHAI PROV., CHINA |
| 0331 | 06/05 | 04.12.54 | 56.2 | 163.1 | 4.3 | P NEAR E COAST KAMCHATKA |
| 0332 | 06/05 | 10.44.59 | 37.8 | 21.4 | 4.2 | P SOUTHERN GREECE |
| 0333 | 06/05 | 11.17.57 | 34.0 | 46.0 | 3.9 | N IRAN-IRAQ BORDER |
| 0334 | 06/05 | 11.52.53 | 29.8 | 70.3 | 4.8 | P PAKISTAN |
| 0335 | 06/05 | 19.00.12 | 86.5 | 38.9 | 4.5 | L N. OF FRANZ JOSEF LAND |
| 0336 | 06/06 | 02.04.44 | 44.0 | 148.0 | 3.4 | L KURILE ISLANDS |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT NO. | DATE | O.T. | COORDINATES | | MB | SEISMIC AREA |
|-----------|-------|----------|-------------|--------|-----|-------------------------------|
| | | | LAT | LONG | | |
| 0337 | 06/06 | 06.32.10 | 49.0 | 155.0 | 3.6 | L KURILE ISLANDS |
| 0338 | 06/06 | 10.43.33 | 55.9 | 163.8 | 4.7 | P OFF E COAST KAMCHATKA |
| 0339 | 06/07 | 01.27.57 | 49.8 | 78.2 | 5.5 | P EAST KAZAKH SSR |
| 0340 | 06/07 | 06.00.20 | 56.0 | 166.0 | 3.8 | I KOMANDORSKY ISLANDS |
| 0341 | 06/08 | 09.14.08 | 21.1 | 120.2 | 5.4 | P TAIWAN |
| 0342 | 06/08 | 09.39.21 | 34.1 | 46.2 | 4.9 | P WESTERN IRAN |
| 0343 | 06/08 | 10.17.44 | 21.0 | 120.2 | 4.9 | P TAIWAN |
| 0344 | 06/08 | 12.46.15 | 41.0 | 44.0 | 4.1 | L TURKEY-USSR BORDER |
| 0345 | 06/08 | 16.08.06 | 19.0 | 54.0 | 4.3 | N BURMA |
| 0346 | 06/08 | 16.44.24 | 21.0 | 120.3 | 4.7 | P TAIWAN |
| 0347 | 06/08 | 17.25.52 | 42.2 | 47.2 | 4.5 | P EASTERN CAUCASUS |
| 0348 | 06/08 | 23.10.12 | 29.5 | 92.3 | 4.7 | P TIBET |
| 0349 | 06/09 | 00.16.42 | 47.0 | 153.0 | 4.4 | L KURILE ISLANDS |
| 0350 | 06/09 | 07.42.20 | 34.8 | 26.5 | 4.9 | P CRETE |
| 0351 | 06/09 | 09.45.09 | -8.8 | -108.3 | 4.9 | P N. OF EASTER IS. CORDILLERA |
| 0352 | 06/09 | 19.42.27 | 37.0 | 44.0 | 4.0 | N TURKEY |
| 0353 | 06/10 | 03.39.33 | 31.0 | 51.0 | 3.6 | N IRAN |
| 0354 | 06/10 | 11.29.11 | 28.2 | 66.5 | 4.5 | P PAKISTAN |
| 0355 | 06/10 | 19.21.53 | 43.0 | 150.0 | 3.7 | L KURILE ISLANDS |
| 0356 | 06/10 | 19.31.42 | 32.9 | 46.3 | 4.0 | P IRAN-IRAQ BORDER |
| 0357 | 06/11 | 14.14.01 | 53.0 | 160.0 | 3.3 | L NEAR E COAST KAMCHATKA |
| 0358 | 06/11 | 23.23.04 | 48.0 | 152.0 | 4.0 | L KURILE ISLANDS |
| 0359 | 06/11 | 23.33.44 | 47.0 | 152.0 | 4.3 | L KURILE ISLANDS |
| 0360 | 06/12 | 00.19.16 | 44.0 | 148.0 | 3.7 | L KURILE ISLANDS |
| 0361 | 06/12 | 13.34.01 | 33.1 | 46.3 | 5.4 | P IRAN-IRAQ BORDER |
| 0362 | 06/12 | 13.39.59 | 33.1 | 46.2 | 5.1 | P IRAN-IRAQ BORDER |
| 0363 | 06/12 | 22.37.38 | 53.0 | 162.0 | 3.7 | L OFF E COAST KAMCHATKA |
| 0364 | 06/13 | 00.55.37 | 33.1 | 46.3 | 5.1 | P IRAN-IRAQ BORDER |
| 0365 | 06/13 | 04.53.30 | 55.0 | 162.0 | 3.8 | L NEAR E COAST KAMCHATKA |
| 0366 | 06/14 | 00.49.54 | 40.1 | 51.9 | 4.7 | P CASPIAN SEA |
| 0367 | 06/14 | 04.34.28 | 33.0 | 46.1 | 5.3 | P IRAN-IRAQ BORDER |
| 0368 | 06/14 | 10.27.50 | 57.0 | 164.0 | 3.6 | L KOMANDORSKY ISLANDS |
| 0369 | 06/14 | 12.11.28 | 31.0 | 52.0 | 3.5 | N IRAN |
| 0370 | 06/14 | 12.35.05 | 27.0 | 56.0 | 3.6 | N SOUTHERN IRAN |
| 0371 | 06/14 | 18.55.53 | 43.7 | 13.4 | 4.9 | P CENTRAL ITALY |
| 0372 | 06/14 | 21.01.00 | 43.7 | 13.5 | 4.7 | P CENTRAL ITALY |
| 0373 | 06/15 | 00.33.24 | 38.3 | 22.2 | 4.9 | P GREECE |
| 0374 | 06/15 | 13.49.13 | 54.0 | 169.0 | 3.5 | L KOMANDORSKY ISLANDS |
| 0375 | 06/15 | 14.19.02 | 38.0 | 28.0 | 3.3 | N TURKEY |
| 0376 | 06/16 | 09.54.41 | 56.0 | 161.0 | 4.1 | L KAMCHATKA |
| 0377 | 06/16 | 18.57.52 | 36.0 | 69.2 | 4.5 | P HINDU KUSH |
| 0378 | 06/16 | 22.12.12 | 53.0 | 157.0 | 3.6 | L KAMCHATKA |
| 0379 | 06/16 | 23.22.27 | 34.0 | 46.0 | 3.7 | N IRAN-IRAQ BORDER |
| 0380 | 06/17 | 09.02.48 | 48.3 | 14.5 | 4.6 | P AUSTRIA |
| 0381 | 06/17 | 19.18.21 | 44.2 | 149.1 | 4.6 | P KURILE ISLANDS |
| 0382 | 06/18 | 04.30.47 | 33.0 | 83.0 | 4.3 | N TIBET |
| 0383 | 06/18 | 09.10.54 | 48.0 | 154.0 | 3.9 | L KURILE ISLANDS |
| 0384 | 06/18 | 09.18.49 | 40.0 | 73.0 | 4.3 | L TADZHIK-SINKIANG BORDER |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT | | O.T. | COORDINATES | | MR | SEISMIC AREA |
|-------|-------|----------|-------------|-------|-----|---------------------------|
| NO. | DATE | | LAT | LONG | | |
| 0385 | 06/18 | 22.32.52 | 39.0 | 31.0 | 4.4 | L TURKEY |
| 0386 | 06/19 | 01.43.48 | 54.4 | 168.6 | 5.0 | P KOMANDORSKY ISLANDS |
| 0387 | 06/19 | 18.02.29 | 44.0 | 147.0 | 4.0 | L KURILE ISLANDS |
| 0388 | 06/19 | 18.07.53 | 43.8 | 151.5 | 4.5 | P KURILE ISLANDS |
| 0389 | 06/19 | 22.41.42 | 48.0 | 157.0 | 4.1 | L KURILE ISLANDS |
| 0390 | 06/20 | 05.17.42 | 29.0 | 52.0 | 4.0 | N SOUTHERN IRAN |
| 0391 | 06/20 | 09.18.00 | 52.0 | 131.0 | 3.7 | L EASTERN RUSSIA |
| 0392 | 06/20 | 15.34.37 | 32.0 | 75.0 | 3.6 | N KASHMIR-INDIA BORDER |
| 0393 | 06/21 | 00.12.58 | 53.0 | 161.0 | 4.3 | N NEAR E COAST KAMCHATKA |
| 0394 | 06/21 | 00.19.02 | 54.0 | 159.0 | 3.7 | N NEAR E COAST KAMCHATKA |
| 0395 | 06/21 | 05.06.17 | 40.2 | 30.0 | 4.1 | P TURKEY |
| 0396 | 06/21 | 10.42.45 | 54.0 | 161.0 | 4.3 | L NEAR E COAST KAMCHATKA |
| 0397 | 06/21 | 14.53.09 | 37.0 | 41.0 | 3.8 | N TURKEY |
| 0398 | 06/21 | 15.06.53 | 43.8 | 13.3 | 4.4 | P CENTRAL ITALY |
| 0399 | 06/22 | 02.35.51 | 49.0 | 154.0 | 4.5 | N KURILE ISLANDS |
| 0400 | 06/23 | 04.25.27 | 41.0 | 30.0 | 3.7 | L TURKEY |
| 0401 | 06/23 | 07.18.14 | 37.0 | 21.0 | 3.4 | N SOUTHERN GREECE |
| 0402 | 06/23 | 08.39.36 | 32.9 | 46.2 | 4.6 | P IRAN-IRAQ BORDER |
| 0403 | 06/23 | 16.59.48 | 37.0 | 75.0 | 3.7 | N TADZHIK-SINKIANG |
| 0404 | 06/24 | 06.57.02 | 28.0 | 54.0 | 3.5 | N SOUTHERN IRAN |
| 0405 | 06/24 | 07.17.56 | 43.7 | 16.9 | 5.3 | P YUGOSLAVIA |
| 0406 | 06/24 | 15.29.22 | 36.2 | 69.7 | 6.0 | P HINDU KUSH |
| 0407 | 06/24 | 16.14.54 | 36.0 | 69.0 | 3.8 | N HINDU KUSH |
| 0408 | 06/24 | 18.53.10 | 39.0 | 74.0 | 3.4 | N TADZHIK-SINKIANG |
| 0409 | 06/25 | 04.59.19 | 44.0 | 15.8 | 4.4 | P YUGOSLAVIA |
| 0410 | 06/25 | 07.55.45 | 36.3 | 69.6 | 4.7 | P HINDU KUSH |
| 0411 | 06/25 | 17.35.50 | 54.0 | 160.0 | 4.1 | L NEAR E COAST KAMCHATKA |
| 0412 | 06/26 | 08.03.25 | 21.1 | 120.3 | 5.0 | P TAIWAN |
| 0413 | 06/26 | 17.32.32 | 56.0 | 158.0 | 3.6 | L KAMCHATKA |
| 0414 | 06/26 | 20.59.03 | 36.0 | 69.0 | 3.7 | N HINDU KUSH |
| 0415 | 06/27 | 05.07.42 | 38.0 | 65.0 | 4.0 | N AFGHANISTAN-USSR BORDER |
| 0416 | 06/27 | 06.39.40 | 9.7 | 70.3 | 5.5 | P PAKISTAN |
| 0417 | 06/27 | 06.49.00 | 4.0 | 159.0 | 3.8 | L NEAR E COAST KAMCHATKA |
| 0418 | 06/27 | 09.05.53 | 26.2 | 56.6 | 4.4 | P BURMA |
| 0419 | 06/27 | 10.48.56 | 29.7 | 70.3 | 5.4 | P PAKISTAN |
| 0420 | 06/27 | 12.20.36 | 51.0 | 47.0 | 3.5 | L WESTERN RUSSIA |
| 0421 | 06/27 | 15.59.35 | 26.3 | 69.5 | 5.1 | P HINDU KUSH |
| 0422 | 06/28 | 01.43.56 | 43.0 | 20.5 | 4.9 | P YUGOSLAVIA |
| 0423 | 06/28 | 03.09.59 | 33.0 | 91.0 | 3.6 | N TSINGHAI PROV., CHINA |
| 0424 | 06/28 | 04.48.22 | 56.0 | 165.0 | 4.2 | L KOMANDORSKY ISLANDS |
| 0425 | 06/28 | 06.00.22 | 55.0 | 164.0 | 3.4 | L KOMANDORSKY ISLANDS |
| 0426 | 06/28 | 08.16.55 | 35.0 | 32.0 | 4.3 | N CYPRUS |
| 0427 | 06/28 | 09.49.35 | 27.6 | 33.8 | 5.6 | P UNITED ARAB REPUBLIC |
| 0428 | 06/28 | 14.58.49 | 53.0 | 161.0 | 3.9 | L OFF E COAST KAMCHATKA |
| 0429 | 06/28 | 20.57.40 | 30.0 | 53.0 | 3.9 | N SOUTHERN IRAN |
| 0430 | 06/29 | 00.41.02 | 54.0 | 69.0 | 3.7 | L CENTRAL KAZAKH SSR |
| 0431 | 06/29 | 03.32.11 | 38.9 | 71.4 | 4.9 | P AFGHANISTAN-USSR BORDER |
| 0432 | 06/30 | 17.49.33 | 27.2 | 56.8 | 4.6 | P SOUTHERN IRAN |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT NO. | DATE | O.T. | COORDINATES | | MR | SEISMIC AREA |
|-----------|-------|----------|-------------|-------|-----|---------------------------------|
| | | | LAT | LONG | | |
| 0432 | 06/30 | 18.57.43 | 24.3 | 121.1 | 4.9 | P TAIWAN |
| 0434 | 06/30 | 20.31.33 | 30.0 | 53.0 | 4.0 | N SOUTHERN IRAN |
| 0435 | 07/01 | 02.10.18 | 54.0 | 166.0 | 3.4 | L KOMANDORSKY ISLANDS |
| 0436 | 07/02 | 12.56.07 | 30.1 | 50.8 | 5.4 | P IRAN (D=31 KM) |
| 0437 | 07/02 | 14.05.06 | 30.0 | 50.8 | 4.6 | P IRAN (D=31 KM) |
| 0438 | 07/03 | 02.10.00 | 30.1 | 50.8 | 5.0 | P IRAN (D=38 KM) |
| 0439 | 07/03 | 03.32.50 | 36.2 | 71.1 | 4.3 | P AFGHAN-USSR BORDER (D=128 KM) |
| 0440 | 07/03 | 12.31.05 | 30.0 | 53.0 | 4.0 | N SOUTHERN IRAN (Q=3) |
| 0441 | 07/03 | 19.26.22 | 32.0 | 48.0 | 4.0 | N IRAN-IRAQ BORDER (Q=3) |
| 0442 | 07/03 | 21.38.22 | 30.0 | 51.0 | 5.1 | P IRAN (D=43 KM) |
| 0443 | 07/04 | 04.42.34 | 49.0 | 156.0 | 3.7 | L KURILE ISLANDS |
| 0444 | 07/04 | 06.17.25 | 41.0 | 32.0 | 3.4 | L TURKEY |
| 0445 | 07/04 | 09.28.07 | 28.0 | 54.0 | 3.9 | N SOUTHERN IRAN (Q=2) |
| 0446 | 07/04 | 13.52.19 | 55.0 | 163.0 | 4.4 | L NEC KAMCHATKA |
| 0447 | 07/04 | 21.47.57 | 49.0 | 151.0 | 3.6 | L KURILE ISLANDS |
| 0448 | 07/05 | 01.04.44 | 29.0 | 54.0 | 3.8 | N SOUTHERN IRAN (Q=3) |
| 0449 | 07/05 | 01.09.53 | 44.6 | 81.1 | 4.6 | P NORTHERN SINKIANG (D=N) |
| 0450 | 07/05 | 02.41.54 | 44.0 | 86.0 | 3.5 | N NORTHERN SINKIANG (Q=3) |
| 0451 | 07/05 | 04.09.49 | 43.6 | 87.9 | 4.3 | P NORTHERN SINKIANG (D=N) |
| 0452 | 07/05 | 09.59.09 | 33.0 | 50.0 | 3.4 | N IRAN (Q=3) |
| 0453 | 07/05 | 16.29.27 | 21.0 | 52.0 | 4.0 | N IRAN (Q=2) |
| 0454 | 07/05 | 18.04.54 | 36.9 | 21.5 | 4.7 | P SOUTHERN GREECE (D=17 KM) |
| 0455 | 07/05 | 21.41.09 | 30.0 | 54.0 | 4.1 | N SOUTHERN IRAN (Q=2) |
| 0456 | 07/06 | 01.02.59 | 49.7 | 79.0 | 4.4 | P E. KAZAKH SSP (D=0 KM) |
| 0457 | 07/06 | 05.41.43 | 27.0 | 55.0 | 3.1 | N SOUTHERN IRAN (Q=3) |
| 0458 | 07/06 | 16.05.32 | 20.2 | 69.7 | 4.3 | P WEST PAKISTAN (D=53 KM) |
| 0459 | 07/06 | 19.02.20 | 44.0 | 146.0 | 3.9 | N KURILE ISLANDS (Q=2) |
| 0460 | 07/07 | 05.12.06 | 56.0 | 163.0 | 3.7 | L NEC KAMCHATKA |
| 0461 | 07/07 | 12.04.12 | 20.5 | 98.1 | 5.0 | P BURMA (D=27 KM) |
| 0462 | 07/07 | 22.43.41 | 32.0 | 102.0 | 3.7 | N SZECHWAN PROV. (Q=3) |
| 0463 | 07/08 | 05.46.14 | 41.6 | 23.6 | 4.7 | P GREECE-BULGARIA PCB. (D=20) |
| 0464 | 07/08 | 08.29.27 | 46.1 | 154.6 | 4.9 | P KURILE ISLANDS (D=N) |
| 0465 | 07/08 | 21.07.27 | 48.0 | 151.0 | 4.2 | L KURILE ISLANDS |
| 0466 | 07/09 | 12.21.22 | 36.0 | 19.0 | 4.0 | L MEDITERRANEAN SEA |
| 0467 | 07/10 | 00.41.23 | 28.0 | 130.6 | 4.1 | P RYUKYU IS. REG. (D=20 KM) |
| 0468 | 07/10 | 03.02.02 | 30.0 | 129.0 | 3.8 | N RYUKYU ISLANDS (Q=3) |
| 0469 | 07/10 | 12.26.21 | 53.6 | 161.7 | 4.1 | P NEC KAMCHATKA (D=N) |
| 0470 | 07/10 | 19.03.33 | 43.4 | 89.6 | 4.7 | P NORTHERN SINKIANG (D=N) |
| 0471 | 07/11 | 04.20.41 | 37.0 | 72.0 | 4.2 | L AFGHANISTAN-USSR BORDER |
| 0472 | 07/11 | 06.58.21 | 48.4 | 154.5 | 5.2 | P KURILE ISLANDS (D=62 KM) |
| 0473 | 07/11 | 08.53.49 | 55.0 | 163.0 | 3.6 | L NEC KAMCHATKA |
| 0474 | 07/11 | 15.32.48 | 32.0 | 60.0 | 3.7 | N IRAN (Q=3) |
| 0475 | 07/11 | 22.49.02 | 36.1 | 45.7 | 4.7 | P IRAN-IRAQ BORDER (D=N) |
| 0476 | 07/12 | 00.14.27 | 49.3 | 155.4 | 5.2 | P KURILE ISLANDS (D=N) |
| 0477 | 07/12 | 01.21.18 | 33.0 | 73.0 | 3.5 | N PAKISTAN (Q=3) |
| 0478 | 07/12 | 14.25.30 | 55.0 | 168.0 | 4.0 | N KOMANDORSKY ISLANDS (Q=2) |
| 0479 | 07/12 | 19.41.48 | 37.2 | 21.9 | 4.1 | P SOUTHERN GREECE (D=92 KM) |
| 0480 | 07/12 | 20.14.51 | 49.0 | 154.0 | 3.7 | L KURILE ISLANDS |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT NO. | DATE | O.T. | COORDINATES | | MB | | SEISMIC AREA |
|-----------|-------|----------|-------------|-------|-----|---|------------------------------|
| | | | LAT | LONG | | | |
| 0481 | 07/13 | 05.27.44 | 31.0 | 89.0 | 3.9 | N | TIBET (Q=2) |
| 0482 | 07/13 | 15.05.44 | 44.0 | 150.0 | 4.2 | N | KURILE ISLANDS REGION (Q=2) |
| 0483 | 07/13 | 18.50.53 | 28.0 | 63.0 | 3.7 | N | WEST PAKISTAN (Q=2) |
| 0484 | 07/13 | 22.21.17 | 43.8 | 13.3 | 4.4 | P | CENTRAL ITALY (D=N) |
| 0485 | 07/13 | 23.02.25 | 22.0 | 123.0 | 3.8 | N | TAIWAN REGION (Q=3) |
| 0486 | 07/14 | 04.33.45 | 36.0 | 21.0 | 3.9 | N | TURKEY (Q=2) |
| 0487 | 07/14 | 13.04.12 | 30.1 | 50.8 | 4.4 | P | IRAN (D=34 KM) |
| 0488 | 07/14 | 13.18.11 | 30.0 | 51.0 | 3.9 | N | IRAN (Q=2) |
| 0489 | 07/14 | 17.49.13 | 30.0 | 51.0 | 3.4 | N | IRAN (Q=2) |
| 0490 | 07/14 | 18.50.33 | 30.0 | 132.0 | 3.9 | L | RYUKYU ISLANDS REGION |
| 0491 | 07/15 | 00.35.52 | 43.0 | 78.0 | 3.8 | N | KIRGIZ SSR (Q=2) |
| 0492 | 07/15 | 02.15.42 | 24.2 | 125.1 | 5.1 | P | SW RYUKYU ISLANDS (D=29 KM) |
| 0493 | 07/15 | 09.51.51 | 47.0 | 152.0 | 4.4 | I | KURILE ISLANDS |
| 0494 | 07/15 | 13.50.04 | 53.0 | 157.0 | 3.7 | L | KAMCHATKA |
| 0495 | 07/15 | 17.25.37 | 46.0 | 149.0 | 3.5 | L | KURILE ISLANDS |
| 0496 | 07/16 | 02.20.24 | 32.5 | 55.9 | 5.2 | P | TIBET (D=N) |
| 0497 | 07/16 | 02.46.51 | 38.3 | 43.3 | 4.9 | P | TURKEY (D=40 KM) |
| 0498 | 07/16 | 03.40.00 | 32.6 | 55.8 | 4.7 | P | TIBET (D=N) |
| 0499 | 07/16 | 13.48.05 | 23.7 | 121.3 | 4.6 | P | TAIWAN (D=N) |
| 0500 | 07/16 | 17.28.03 | 44.0 | 150.0 | 3.7 | L | KURILE ISLANDS |
| 0501 | 07/16 | 20.04.04 | 54.4 | 162.9 | 4.2 | P | NEC KAMCHATKA (D=N) |
| 0502 | 07/16 | 22.41.59 | 27.0 | 101.0 | 3.9 | N | YUNNAN PROV. (Q=2) |
| 0503 | 07/17 | 01.17.26 | 51.0 | 158.0 | 4.2 | L | NEC KAMCHATKA |
| 0504 | 07/17 | 03.14.05 | 34.0 | 30.0 | 3.9 | L | EASTERN MEDITERRANEAN SEA |
| 0505 | 07/17 | 08.29.52 | 55.0 | 159.6 | 5.3 | P | KAMCHATKA (D=N) |
| 0506 | 07/17 | 11.11.46 | 57.0 | 162.0 | 3.3 | L | NEC KAMCHATKA |
| 0507 | 07/17 | 16.15.28 | 35.0 | 22.0 | 3.4 | N | MEDITERRANEAN SEA (Q=3) |
| 0508 | 07/17 | 17.02.48 | 43.0 | 149.0 | 4.1 | I | KURILE ISLANDS REGION |
| 0509 | 07/17 | 20.50.54 | 55.1 | 159.5 | 4.5 | P | KAMCHATKA (D=N) |
| 0510 | 07/18 | 03.27.07 | 29.0 | 77.0 | 4.0 | N | SOUTH SINKIANG (Q=1) |
| 0511 | 07/18 | 06.04.53 | 51.0 | 66.0 | 3.7 | I | CENTRAL KAZAKH SSR |
| 0512 | 07/18 | 13.45.48 | 41.0 | 23.8 | 4.0 | P | GREECE-BULGARIA BORDER (D=N) |
| 0513 | 07/18 | 22.06.50 | 45.0 | 148.0 | 5.0 | P | KURILE ISLANDS |
| 0514 | 07/19 | 10.26.48 | 52.0 | 162.0 | 4.2 | L | NEC KAMCHATKA |
| 0515 | 07/19 | 12.02.50 | 56.0 | 157.0 | 4.3 | L | KAMCHATKA |
| 0516 | 07/19 | 19.43.40 | 38.0 | 70.0 | 3.6 | N | AFGHAN.-USSR BORDER (Q=3) |
| 0517 | 07/20 | 10.04.18 | 28.0 | 91.0 | 3.9 | N | TIBET (Q=2) |
| 0518 | 07/20 | 13.58.43 | 36.0 | 55.0 | 4.3 | N | IRAN (Q=2) |
| 0519 | 07/21 | 14.07.08 | 27.5 | 73.0 | 4.1 | P | TADZHIK SSR (D=197 KM) |
| 0520 | 07/21 | 16.11.32 | 28.8 | 102.3 | 4.8 | P | SZECHWAN PROV., CHINA (D=N) |
| 0521 | 07/22 | 05.10.40 | 44.9 | 36.0 | 4.6 | P | CRIMEA (D=N) |
| 0522 | 07/22 | 16.41.04 | 31.4 | 91.5 | 5.5 | P | TIBET (D=N) |
| 0523 | 07/22 | 21.00.09 | 31.4 | 91.4 | 4.7 | P | TIBET (D=N) |
| 0524 | 07/23 | 18.17.25 | 33.0 | 24.0 | 3.9 | I | MEDITERRANEAN SEA |
| 0525 | 07/23 | 23.41.55 | 31.0 | 91.0 | 3.6 | N | TIBET (Q=2) |
| 0526 | 07/24 | 10.14.35 | 58.0 | 159.0 | 3.7 | L | KAMCHATKA |
| 0527 | 07/24 | 10.22.22 | 29.4 | 40.1 | 4.4 | P | TURKEY (D=N) |
| 0528 | 07/24 | 13.09.26 | 58.0 | 162.0 | 4.0 | L | KAMCHATKA |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT | | | COORDINATES | | MR | SEISMIC AREA |
|-------|-------|----------|-------------|-------|-----|------------------------------|
| NO. | DATE | O.T. | LAT | LONG | | |
| 0529 | 07/24 | 14.58.14 | 35.8 | 80.6 | 4.8 | P KASHMIR-TIBET BORDER (Q=N) |
| 0530 | 07/25 | 01.56.07 | 38.7 | 21.4 | 4.5 | P GREECE (Q=45 KM) |
| 0531 | 07/26 | 02.26.08 | 45.2 | 150.7 | 4.3 | P KURILE ISLANDS (Q=80 KM) |
| 0532 | 07/26 | 18.57.25 | 40.0 | 47.0 | 4.0 | N EASTERN CAUCASUS (Q=3) |
| 0533 | 07/27 | 00.08.46 | 43.6 | 13.4 | 4.4 | P CENTRAL ITALY (Q=N) |
| 0534 | 07/27 | 00.20.55 | 50.0 | 159.1 | 5.1 | P KURILE ISLANDS (Q=N) |
| 0535 | 07/27 | 16.41.30 | 25.4 | 130.5 | 5.1 | P RYUKYU IS. REG. (Q=N) |
| 0536 | 07/28 | 05.50.29 | 42.0 | 81.0 | 4.3 | L SOUTHERN SINKIANG PROV. |
| 0537 | 07/29 | 08.22.17 | 37.0 | 29.0 | 3.8 | L DODECANESE ISLANDS |
| 0538 | 07/29 | 17.10.35 | 32.0 | 68.0 | 3.8 | N AFGHANISTAN (Q=2) |
| 0539 | 07/29 | 21.07.16 | 49.2 | 156.2 | 4.8 | P KURILE ISLANDS (Q=N) |
| 0540 | 07/30 | 01.30.09 | 39.9 | 24.2 | 4.4 | P AEGEAN SEA (Q=N) |
| 0541 | 07/30 | 03.01.07 | 49.2 | 156.2 | 5.1 | P KURILE ISLANDS (Q=45 KM) |
| 0542 | 07/30 | 11.41.01 | 41.0 | 70.0 | 4.0 | N TADZHIK SSR (Q=2) |
| 0543 | 07/30 | 16.00.03 | 21.2 | 121.3 | 4.9 | P TAIWAN REGION (Q=N) |
| 0544 | 07/30 | 19.00.54 | 30.0 | 101.0 | 3.5 | N SZECHWAN PROV. (Q=2) |
| 0545 | 07/30 | 19.46.24 | 41.0 | 27.0 | 3.6 | I TURKEY |
| 0546 | 07/31 | 06.40.28 | 56.2 | 162.9 | 4.8 | P NEC KAMCHATKA (Q=N) |
| 0547 | 07/31 | 17.04.47 | 23.7 | 121.6 | 4.6 | P TAIWAN (Q=24 KM) |
| 0548 | 07/31 | 21.01.25 | 31.0 | 52.0 | 3.6 | N IRAN (Q=3) |
| 0549 | 08/01 | 05.33.41 | 30.0 | 131.0 | 3.7 | I RYUKYU ISL |
| 0550 | 08/01 | 09.44.47 | 36.0 | 72.0 | 4.1 | N PAKISTAN |
| 0551 | 08/01 | 11.03.49 | 33.0 | 32.0 | 3.7 | N MEDITER SEA |
| 0552 | 08/02 | 10.52.27 | 39.0 | 73.0 | 3.7 | N KIRGIZ USSR |
| 0553 | 08/02 | 12.55.19 | 36.0 | 72.0 | 3.9 | N AFGHAN-USSR |
| 0554 | 08/02 | 15.11.59 | 35.0 | 35.0 | 4.5 | I CYPRUS |
| 0555 | 08/02 | 15.47.37 | 25.0 | 24.0 | 3.4 | N CRETE |
| 0556 | 08/02 | 18.42.20 | 43.2 | 146.5 | 4.0 | P KURIL ISL |
| 0557 | 08/02 | 21.33.06 | 28.2 | 57.0 | 4.7 | P S IRAN |
| 0558 | 08/02 | 21.38.50 | 56.1 | 163.2 | 5.6 | P NEC KAMCHATKA |
| 0559 | 08/02 | 23.03.29 | 28.1 | 56.9 | 5.0 | P S IRAN |
| 0560 | 08/02 | 23.12.13 | 28.0 | 57.0 | 4.2 | N S IRAN |
| 0561 | 08/03 | 02.04.26 | 27.8 | 32.5 | 4.3 | P TURKEY |
| 0562 | 08/03 | 02.25.23 | 46.9 | 152.6 | 4.5 | P KURIL ISL |
| 0563 | 08/03 | 03.57.16 | 56.0 | 162.0 | 4.0 | I NEC KAMCHATKA |
| 0564 | 08/03 | 05.51.44 | 40.0 | 32.0 | 3.9 | I TURKEY |
| 0565 | 08/03 | 12.36.47 | 59.5 | 163.2 | 5.3 | P KAMCHATKA |
| 0566 | 08/03 | 21.39.26 | 27.7 | 32.7 | 4.5 | P TURKEY |
| 0567 | 08/03 | 22.47.46 | 28.2 | 57.0 | 4.8 | P S IRAN |
| 0568 | 08/03 | 22.57.23 | 28.0 | 133.0 | 4.0 | N R RYUKYU ISL |
| 0569 | 08/04 | 04.30.30 | 47.0 | 151.0 | 4.0 | I KURIL ISL |
| 0570 | 08/04 | 05.30.00 | 37.9 | 32.0 | 4.3 | P TURKEY |
| 0571 | 08/04 | 09.19.21 | 28.0 | 57.0 | 4.0 | N S IRAN |
| 0572 | 08/04 | 17.09.20 | 48.0 | 155.0 | 3.9 | I KURIL ISL |
| 0573 | 08/04 | 17.51.13 | 49.2 | 156.1 | 5.7 | P KURIL ISL |
| 0574 | 08/04 | 18.26.11 | 49.0 | 156.2 | 4.4 | P KURIL ISL |
| 0575 | 08/05 | 00.49.03 | 49.0 | 157.0 | 3.8 | L KURIL ISL |
| 0576 | 08/05 | 04.08.14 | 28.2 | 52.0 | 4.3 | P S IRAN |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT NO. | DATE | O.T. | COORDINATES | | MR | | SEISMIC AREA |
|--------------|-------|----------|-------------|-------|-----|---|-------------------|
| | | | LAT | LONG | | | |
| 0577 | 08/05 | 04.16.37 | 49.0 | 157.0 | 4.1 | L | KURIL ISL |
| 0578 | 08/05 | 04.52.03 | 49.0 | 156.3 | 4.7 | P | KURIL ISL |
| 0579 | 08/05 | 05.46.29 | 49.0 | 156.2 | 4.9 | P | KURIL ISL |
| 0580 | 08/05 | 05.52.01 | 49.0 | 156.0 | 4.3 | L | KURIL ISL |
| 0581 | 08/05 | 22.11.52 | 49.0 | 155.0 | 3.8 | I | KURIL ISL |
| 0582 | 08/06 | 00.53.12 | 44.7 | 32.6 | 4.5 | P | BLACK SEA |
| 0583 | 08/06 | 01.12.50 | 25.1 | 61.2 | 5.5 | P | S IRAN |
| 0584 | 08/06 | 01.32.16 | 25.7 | 60.9 | 5.0 | P | S IRAN |
| 0585 | 08/06 | 03.45.07 | 34.0 | 29.0 | 4.0 | L | MEDITER SEA |
| 0586 | 08/06 | 07.00.56 | 31.8 | 50.1 | 5.0 | P | IRAN |
| 0587 | 08/06 | 10.08.59 | 36.0 | 27.0 | 4.0 | L | DODECANESE ISL |
| 0588 | 08/06 | 10.59.17 | 49.0 | 157.0 | 4.2 | L | KURIL ISL |
| 0589 | 08/06 | 11.07.30 | 49.0 | 156.4 | 4.2 | P | KURIL ISL |
| 0590 | 08/06 | 14.17.30 | 55.0 | 164.0 | 3.7 | I | KOMANDORSKY ISL |
| 0591 | 08/06 | 18.22.25 | 55.3 | 166.1 | 4.5 | P | KOMANDORSKY ISL |
| 0592 | 08/07 | 05.42.48 | 38.0 | 32.0 | 4.0 | L | TURKEY |
| 0593 | 08/07 | 10.05.58 | 53.0 | 168.0 | 3.9 | I | KOMANDORSKY ISL |
| 0594 | 08/08 | 00.44.55 | 26.3 | 52.6 | 4.7 | P | IRAN |
| 0595 | 08/08 | 14.24.18 | 26.0 | 63.0 | 4.2 | N | W PAKISTAN |
| 0596 | 08/08 | 09.45.49 | 48.1 | 157.1 | 5.1 | P | KURIL ISL |
| 0597 | 08/08 | 17.19.42 | 55.0 | 158.0 | 3.8 | L | KAMCHATKA |
| 0598 | 08/08 | 19.09.34 | 25.0 | 61.1 | 5.5 | P | S IRAN |
| 0599 | 08/09 | 01.28.15 | 56.0 | 166.0 | 3.7 | L | KOMANDORSKY ISL |
| 0600 | 08/09 | 04.02.05 | 39.5 | 20.7 | 4.5 | P | GREECE-ALBANIA |
| 0601 | 08/09 | 09.40.46 | 39.0 | 33.0 | 4.4 | L | TURKEY |
| 0602 | 08/09 | 10.34.54 | 49.0 | 153.0 | 4.1 | L | KURIL ISL |
| 0603 | 08/09 | 14.43.39 | 50.0 | 119.0 | 3.8 | L | USSR-CHINA BORDER |
| 0604 | 08/09 | 16.28.14 | 41.0 | 72.0 | 4.5 | L | TADZHIK USSR |
| 0605 | 08/09 | 19.42.17 | 53.0 | 107.5 | 5.1 | P | LAKE BAIKAL REG |
| 0606 | 08/09 | 20.51.51 | 56.8 | 127.2 | 4.8 | P | E RUSSIA |
| 0607 | 08/09 | 21.09.10 | 47.0 | 153.0 | 4.1 | L | KURIL ISL |
| 0608 | 08/10 | 01.05.40 | 36.0 | 67.0 | 4.5 | I | HINDU KUSH |
| 0609 | 08/10 | 14.07.13 | 55.0 | 166.0 | 3.5 | L | KOMANDORSKY ISL |
| 0610 | 08/10 | 21.06.40 | 32.4 | 53.5 | 5.2 | P | TIBET |
| 0611 | 08/11 | 02.22.14 | 44.7 | 102.0 | 5.0 | P | MONGOLIA |
| 0612 | 08/11 | 06.49.05 | 41.0 | 14.0 | 4.0 | L | S ITALY |
| 0613 | 08/11 | 08.50.34 | 56.0 | 164.0 | 3.3 | L | KOMANDORSKY ISL |
| 0614 | 08/11 | 13.24.44 | 54.6 | 161.6 | 5.3 | P | NEC KAMCHATKA |
| 0615 | 08/11 | 16.52.32 | 31.0 | 52.0 | 3.5 | N | IRAN |
| 0616 | 08/12 | 02.42.24 | 36.0 | 69.0 | 3.9 | N | HINDU KUSH |
| 0617 | 08/12 | 23.47.57 | 41.1 | 22.7 | 4.9 | P | YUGOSLAVIA |
| 0618 | 08/13 | 02.16.28 | 33.0 | 93.0 | 4.1 | N | TSINGHAI |
| 0619 | 08/13 | 09.04.48 | 26.9 | 71.4 | 4.7 | P | AFGANISTAN-USSR |
| 0620 | 08/13 | 10.43.57 | 49.0 | 157.0 | 3.6 | L | KURIL ISL |
| 0621 | 08/13 | 11.32.30 | 49.0 | 154.0 | 3.6 | L | KURIL ISL |
| 0622 | 08/13 | 12.15.47 | 47.0 | 152.0 | 3.6 | L | KURIL ISL |
| 0623 | 08/13 | 18.21.56 | 54.0 | 160.0 | 3.6 | L | NEC KAMCHATKA |
| 0624 | 08/15 | 22.15.37 | 47.0 | 151.0 | 4.1 | L | KURIL ISL |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT | | | COORDINATES | | MR | SEISMIC AREA |
|-------|-------|----------|-------------|-------|-----|--------------------|
| NO. | DATE | O.T. | LAT | LONG | | |
| 0625 | 08/16 | 01.44.47 | 55.0 | 164.0 | 3.4 | I NEC KAMCHATKA |
| 0626 | 08/16 | 03.16.57 | 49.8 | 78.1 | 5.2 | P E KAZAKH |
| 0627 | 08/16 | 05.42.22 | 36.0 | 49.0 | 3.5 | N NW IRAN |
| 0628 | 08/16 | 08.21.14 | 55.0 | 164.0 | 3.6 | I KOMANDORSKY ISL |
| 0629 | 08/16 | 10.15.32 | 38.0 | 71.0 | 3.6 | N AFGHANISTAN-USSR |
| 0630 | 08/16 | 10.26.58 | 55.0 | 165.5 | 4.2 | P KOMANDORSKY ISL |
| 0631 | 08/16 | 12.08.56 | 49.0 | 154.0 | 3.5 | I KURIL ISL |
| 0632 | 08/16 | 19.27.10 | 45.0 | 149.0 | 4.5 | L KURIL ISL |
| 0633 | 08/16 | 21.37.19 | 56.0 | 163.0 | 3.6 | L NEC KAMCHATKA |
| 0634 | 08/17 | 22.34.32 | 44.0 | 149.0 | 4.5 | L KURIL ISL |
| 0635 | 08/17 | 18.14.22 | 30.0 | 73.0 | 5.0 | N N INDIA |
| 0636 | 08/18 | 00.42.22 | 45.0 | 150.0 | 3.5 | I KURIL ISL |
| 0637 | 08/18 | 01.18.20 | 53.0 | 160.0 | 3.6 | I NEC KAMCHATKA |
| 0638 | 08/18 | 02.49.15 | 52.0 | 159.0 | 3.5 | L NEC KAMCHATKA |
| 0639 | 08/18 | 08.10.18 | 40.0 | 22.0 | 3.6 | L GREECE |
| 0640 | 08/18 | 10.03.07 | 25.0 | 64.0 | 3.9 | N W PAKISTAN |
| 0641 | 08/18 | 12.12.08 | 48.0 | 100.0 | 4.0 | L MONGOLIA |
| 0642 | 08/18 | 18.42.19 | 23.8 | 126.6 | 4.8 | P RYUKYU ISL |
| 0643 | 08/18 | 18.50.18 | 55.0 | 163.0 | 4.0 | L NEC KAMCHATKA |
| 0644 | 08/18 | 19.02.01 | 53.0 | 159.9 | 5.1 | P NEC KAMCHATKA |
| 0645 | 08/18 | 21.23.12 | 50.0 | 153.0 | 5.1 | L NW KURIL ISL |
| 0646 | 08/18 | 23.23.18 | 50.0 | 153.0 | 3.7 | L NW KURIL ISL |
| 0647 | 08/19 | 04.20.41 | 22.0 | 94.0 | 3.9 | N BURMA-INDIA |
| 0648 | 08/19 | 06.46.56 | 38.0 | 23.0 | 3.6 | L GREECE |
| 0649 | 08/19 | 17.54.24 | 43.2 | 146.8 | 4.3 | P KURIL ISL |
| 0650 | 08/19 | 21.56.10 | 45.0 | 149.0 | 3.5 | L KURIL ISL |
| 0651 | 08/19 | 23.20.48 | 43.5 | 148.4 | 4.9 | P KURIL ISL |
| 0652 | 08/20 | 02.59.58 | 49.5 | 48.2 | 5.7 | P W KAZAKH |
| 0653 | 08/20 | 08.10.08 | 51.3 | 161.6 | 5.2 | P NEC KAMCHATKA |
| 0654 | 08/21 | 10.15.44 | 55.7 | 161.3 | 4.5 | P NEC KAMCHATKA |
| 0655 | 08/21 | 13.45.49 | 47.0 | 151.0 | 4.0 | L KURIL ISL |
| 0656 | 08/21 | 14.04.34 | 27.2 | 88.0 | 4.8 | P SIKKIM |
| 0657 | 08/21 | 14.24.07 | 22.0 | 94.0 | 4.3 | N BURMA-INDIA |
| 0658 | 08/21 | 18.55.07 | 27.2 | 88.0 | 5.1 | P SIKKIM |
| 0659 | 08/22 | 02.44.10 | 35.0 | 25.0 | 4.0 | L CRETE |
| 0660 | 08/22 | 03.37.00 | 47.0 | 153.0 | 4.1 | L KURIL ISL |
| 0661 | 08/22 | 14.20.19 | 50.2 | 156.7 | 5.2 | P KURIL ISL |
| 0662 | 08/22 | 16.34.56 | 40.0 | 79.0 | 4.6 | L S SIKKIM |
| 0663 | 08/22 | 21.54.53 | 23.0 | 121.0 | 4.2 | N TAIWAN |
| 0664 | 08/23 | 10.38.08 | 49.0 | 156.0 | 3.7 | I KURIL ISL |
| 0665 | 08/23 | 21.14.16 | 39.0 | 29.0 | 4.0 | I TURKEY |
| 0666 | 08/24 | 10.44.01 | 51.0 | 157.0 | 3.3 | I KURIL ISL |
| 0667 | 08/24 | 15.32.39 | 50.0 | 159.0 | 3.8 | L KURIL ISL |
| 0668 | 08/24 | 17.05.56 | 53.0 | 160.0 | 3.8 | L NEC KAMCHATKA |
| 0669 | 08/24 | 22.54.19 | 48.0 | 147.0 | 3.9 | L NW KURIL ISL |
| 0670 | 08/25 | 04.11.20 | 71.0 | 139.0 | 4.0 | L NE SIBERIA |
| 0671 | 08/25 | 10.19.34 | 47.0 | 152.0 | 3.6 | I KURIL ISL |
| 0672 | 08/26 | 03.46.57 | 50.0 | 77.8 | 5.5 | P E KAZAKH |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT | | | COORDINATES | | MR | SEISMIC AREA |
|-------|-------|----------|-------------|-------|-----|------------------|
| NO. | DATE | C.T. | LAT | LONG | | |
| 0673 | 08/26 | 11.21.09 | 22.0 | 101.0 | 3.8 | N SZECHWAN |
| 0674 | 08/27 | 01.14.57 | 38.0 | 30.0 | 3.6 | N TURKEY |
| 0675 | 08/27 | 14.42.46 | 23.0 | 102.0 | 4.0 | N BURMA-INDIA |
| 0676 | 08/27 | 14.49.32 | 22.6 | 100.7 | 4.8 | P BURMA-INDIA |
| 0677 | 08/27 | 16.54.01 | 36.0 | 70.0 | 3.6 | N HINDU KUSH |
| 0678 | 08/28 | 02.39.06 | 56.0 | 163.0 | 4.2 | L NEC KAMCHATKA |
| 0679 | 08/28 | 05.59.56 | 73.3 | 55.1 | 6.3 | P NOVAYA ZEMLYA |
| 0680 | 08/28 | 06.33.40 | 36.0 | 64.0 | 5.2 | L TURK-AFGAN BCP |
| 0681 | 08/28 | 09.00.22 | 49.0 | 155.0 | 3.7 | L KURIL ISL |
| 0682 | 08/28 | 15.27.10 | 33.0 | 49.0 | 3.7 | N W IRAN |
| 0683 | 08/29 | 21.59.23 | 33.0 | 27.0 | 4.4 | L MEDITER SEA |
| 0684 | 08/29 | 21.17.52 | 36.0 | 26.0 | 3.6 | N CRETE |
| 0685 | 08/29 | 23.00.21 | 34.0 | 82.0 | 3.7 | N TIBET |
| 0686 | 08/30 | 00.08.23 | 44.0 | 16.2 | 4.5 | P YUGOSLAVIA |
| 0687 | 08/30 | 15.14.10 | 36.7 | 56.5 | 5.5 | P TSINGHAI |
| 0688 | 08/30 | 17.52.23 | 40.0 | 54.0 | 4.2 | N S SINKIANG |
| 0689 | 08/30 | 18.47.43 | 36.6 | 56.4 | 5.5 | P TSINGHAI |
| 0690 | 08/30 | 18.51.35 | 36.7 | 56.3 | 5.5 | P TSINGHAI |
| 0691 | 08/30 | 20.06.50 | 53.0 | 160.0 | 4.6 | L NEC KAMCHATKA |
| 0692 | 08/30 | 20.42.46 | 38.0 | 56.0 | 4.3 | N TSINGHAI |
| 0693 | 08/31 | 14.03.16 | 52.3 | 55.4 | 5.5 | P C RUSSIA |
| 0694 | 08/31 | 17.22.47 | 49.0 | 106.0 | 3.7 | L MONGOLIA |
| 0695 | 08/31 | 18.12.08 | 55.0 | 163.0 | 3.5 | L NEC KAMCHATKA |
| 0696 | 11/01 | 04.06.45 | 38.5 | 65.2 | 4.4 | P S F UZBEK |
| 0697 | 11/01 | 06.22.29 | 26.7 | 141.5 | 4.4 | P F C HONSHU |
| 0698 | 11/01 | 16.39.51 | 43.4 | 146.3 | 4.8 | P KURIL ISL |
| 0699 | 11/02 | 01.26.58 | 49.9 | 78.8 | 6.2 | P F KAZAKH |
| 0700 | 11/02 | 12.52.23 | 39.4 | 73.2 | 4.3 | P TADZHIK-SINK |
| 0701 | 11/03 | 09.41.32 | 31.0 | 52.0 | 4.0 | N IRAN |
| 0702 | 11/03 | 23.58.09 | 25.0 | 69.5 | 5.5 | L AFGHANISTAN |
| 0703 | 11/05 | 14. 6.59 | 36.0 | 72.0 | 3.8 | N AFGHAN-USSR |
| 0704 | 11/05 | 19.25.42 | 35.1 | 24.9 | 5.2 | P CRETE |
| 0705 | 11/06 | 06.15.06 | 36.9 | 70.8 | 4.2 | L HINDU KUSH |
| 0706 | 11/06 | 07.07.10 | 34.1 | 23.3 | 3.7 | L CYPRLS |
| 0707 | 11/06 | 09.31.56 | 34.6 | 25.1 | 4.3 | L CRETE |
| 0708 | 11/06 | 10.56.09 | 27.0 | 88.7 | 4.8 | P SIKKIM |
| 0709 | 11/06 | 12.18.30 | 38.2 | 69.0 | 4.1 | P TADZHIK |
| 0710 | 11/06 | 16.22.20 | 44.0 | 148.8 | 4.3 | L KURIL ISL |
| 0711 | 11/07 | 06.40.36 | 22.7 | 120.7 | 5.4 | P TAIWAN |
| 0712 | 11/07 | 15.12.34 | 37.0 | 73.0 | 4.3 | N AFGHAN-USSR |
| 0713 | 11/07 | 18.36.29 | 52.3 | 160.0 | 4.5 | L NEC KAMCHATKA |
| 0714 | 11/07 | 22.41.33 | 34.9 | 24.8 | 4.6 | P CRETE |
| 0715 | 11/08 | 11.11.47 | 47.3 | 151.0 | 3.7 | L KURIL ISL |
| 0716 | 11/08 | 14.25.43 | 23.9 | 121.6 | 5.5 | P TAIWAN |
| 0717 | 11/09 | 16.45.10 | 38.0 | 20.5 | 4.2 | L IONIAN SEA |
| 0718 | 11/10 | 04.45.12 | 30.3 | 57.6 | 4.7 | P IRAN |
| 0719 | 11/10 | 09.52.19 | 39.8 | 23.3 | 3.6 | L TURKEY |
| 0720 | 11/10 | 18.22.39 | 50.1 | 154.3 | 3.6 | L KURIL ISL |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT NO. | DATE | O.T. | COORDINATES | | MR | | SEISMIC AREA |
|--------------|-------|----------|-------------|-------|-----|---|------------------|
| | | | LAT | LONG | | | |
| 0721 | 11/11 | 13.57.23 | 49.9 | 129.6 | 3.8 | L | E CHINA-USSR BCR |
| 0722 | 11/11 | 14.08.58 | 41.0 | 77.0 | 3.8 | N | KIRGIZ-SINK BCP |
| 0723 | 11/12 | 02.46.34 | 55.5 | 162.0 | 4.8 | P | NFC KAMCHATKA |
| 0724 | 11/13 | 01.56.51 | 45.7 | 149.0 | 3.7 | L | KURIL ISL |
| 0725 | 11/14 | 18.27.04 | 14.0 | 52.0 | 3.9 | N | E GULF OF ADEN |
| 0726 | 11/15 | 03.36.28 | 22.0 | 123.0 | 4.1 | N | TAIWAN |
| 0727 | 11/15 | 18.15.07 | 29.0 | 53.0 | 3.9 | N | S IRAN |
| 0728 | 11/15 | 12.21.41 | 22.2 | 28.0 | 4.5 | L | E MEDITER SEA |
| 0729 | 11/15 | 14.56.53 | 37.0 | 73.0 | 3.9 | N | AFGHAN-USSR |
| 0730 | 11/16 | 03.13.06 | 35.0 | 24.0 | 3.8 | L | CRETE |
| 0731 | 11/16 | 10.10.47 | 34.0 | 46.0 | 3.9 | N | IRAN-IRAQ BCP |
| 0732 | 11/16 | 11.24.12 | 24.0 | 96.0 | 4.4 | N | BURMA |
| 0733 | 11/17 | 02.13.07 | 35.0 | 24.0 | 3.7 | N | CRETE |
| 0734 | 11/17 | 02.42.36 | 37.4 | 20.3 | 4.3 | P | IONIAN SEA |
| 0735 | 11/17 | 15.58.47 | 44.0 | 152.0 | 4.0 | N | KURIL ISL |
| 0736 | 11/17 | 17.12.02 | 44.4 | 148.6 | 3.7 | L | KURIL ISL |
| 0737 | 11/18 | 08.31.16 | 52.7 | 160.2 | 4.6 | P | NFC KAMCHATKA |
| 0738 | 11/18 | 12.52.53 | 44.8 | 148.5 | 3.9 | L | KURIL ISL |
| 0739 | 11/18 | 17.53.59 | 46.4 | 154.2 | 4.0 | L | KURIL ISL |
| 0740 | 11/19 | 20.53.01 | 43.0 | 82.0 | 4.0 | N | N SIAKIANG |
| 0741 | 11/20 | 03.30.28 | 39.4 | 21.8 | 4.9 | P | GREECE |
| 0742 | 11/20 | 03.34.34 | 31.0 | 51.0 | 4.0 | N | IRAN |
| 0743 | 11/20 | 05.37.12 | 43.0 | 84.0 | 4.0 | N | N SIAKIANG |
| 0744 | 11/21 | 02.47.14 | 23.8 | 121.6 | 5.7 | P | TAIWAN |
| 0745 | 11/21 | 02.51.25 | 23.0 | 121.0 | 4.4 | N | TAIWAN |
| 0746 | 11/21 | 11.51.50 | 58.2 | 63.0 | 3.6 | L | C RUSSIA |
| 0747 | 11/21 | 18.16.17 | 34.2 | 20.3 | 4.1 | L | E MEDITER SEA |
| 0748 | 11/21 | 19.12.58 | 37.0 | 73.0 | 4.0 | N | AFGHAN-USSR |
| 0749 | 11/22 | 03.01.53 | 37.0 | 76.0 | 4.0 | N | S SIAKIANG |
| 0750 | 11/22 | 18.05.51 | 35.9 | 77.4 | 4.9 | P | E KASHMIR |
| 0751 | 11/24 | 01.35.27 | 38.8 | 22.3 | 4.3 | P | GREECE |
| 0752 | 11/24 | 03.48.38 | 40.1 | 21.6 | 5.4 | L | GREECE |
| 0753 | 11/24 | 09.00.08 | 52.8 | 51.1 | 4.7 | P | W RUSSIA |
| 0754 | 11/24 | 09.40.56 | 21.0 | 52.0 | 3.7 | N | IRAN |
| 0755 | 11/24 | 09.59.58 | 51.8 | 64.2 | 5.2 | P | W KAZAKH |
| 0756 | 11/25 | 02.11.39 | 52.3 | 158.9 | 3.4 | L | NFC KAMCHATKA |
| 0757 | 11/25 | 12.18.24 | 33.0 | 57.0 | 3.9 | N | TSINGHAI CHINA |
| 0758 | 11/25 | 13.42.34 | 56.3 | 123.3 | 5.1 | P | E RUSSIA |
| 0759 | 11/25 | 15.20.48 | 38.4 | 22.3 | 4.0 | P | GREECE |
| 0760 | 11/25 | 22.43.30 | 28.4 | 53.7 | 5.6 | P | S IRAN |
| 0761 | 11/26 | 14.52.31 | 52.1 | 158.8 | 5.2 | P | NFC KAMCHATKA |
| 0762 | 11/26 | 16.03.12 | 43.0 | 13.4 | 4.9 | P | C ITALY |
| 0763 | 11/27 | 05.11.11 | 52.8 | 62.1 | 3.9 | L | W KAZAKH |
| 0764 | 11/27 | 21.37.47 | 53.4 | 161.3 | 4.7 | P | NFC KAMCHATKA |
| 0765 | 11/28 | 13.26.15 | 33.8 | 27.9 | 4.8 | P | E MEDITER SEA |
| 0766 | 11/28 | 18.42.47 | 55.4 | 162.1 | 3.6 | L | NFC KAMCHATKA |
| 0767 | 11/29 | 01.57.57 | 32.2 | 26.5 | 4.4 | L | E MEDITER SEA |
| 0768 | 11/29 | 03.19.19 | 36.0 | 72.0 | 3.6 | N | AFGHAN-USSR |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT NO. | DATE | O.T. | COORDINATES | | MR | | SEISMIC AREA |
|--------------|-------|----------|-------------|-------|-----|---|-----------------|
| | | | LAT | LONG | | | |
| 0769 | 11/29 | 16.49.36 | 26.0 | 72.0 | 4.1 | N | AFGHAN-USSR |
| 0770 | 11/30 | 07.24.16 | 72.3 | 144.9 | 3.6 | L | SIBERIAN ISL |
| 0771 | 11/30 | 11.25.32 | 44.1 | 13.0 | 4.6 | P | ADRIATIC SEA |
| 0772 | 11/30 | 18.31.19 | 52.8 | 160.7 | 3.9 | L | CEC KAMCHATKA |
| 0773 | 12/01 | 07.24.52 | 42.7 | 13.2 | 3.9 | P | C ITALY |
| 0774 | 12/01 | 07.32.01 | 29.0 | 52.0 | 4.7 | N | S IRAN |
| 0775 | 12/01 | 11.29.04 | 35.4 | 57.9 | 5.4 | P | IRAN |
| 0776 | 12/01 | 21.15.52 | 54.9 | 162.0 | 4.8 | P | NFC KAMCHATKA |
| 0777 | 12/02 | 03.57.54 | 33.5 | 141.0 | 4.1 | P | CEC HONSHU |
| 0778 | 12/02 | 13.28.24 | 35.4 | 27.1 | 5.1 | P | NO DECANESF ISL |
| 0779 | 12/02 | 20.33.00 | 33.2 | 141.0 | 3.6 | P | CEC HONSHU |
| 0780 | 12/03 | 02.18.46 | 46.0 | 144.0 | 3.9 | L | SAKHALIN ISL |
| 0781 | 12/03 | 08.54.47 | 39.4 | 75.3 | 5.0 | P | S SINKIANG |
| 0782 | 12/03 | 10.07.57 | 46.0 | 145.0 | 4.0 | L | SEA OF OKHOTSK |
| 0783 | 12/03 | 13.13.13 | 53.8 | 160.6 | 4.4 | P | NFC KAMCHATKA |
| 0784 | 12/03 | 15.35.14 | 45.0 | 148.0 | 4.1 | L | KURIL ISL |
| 0785 | 12/03 | 22.08.32 | 31.9 | 131.5 | 5.3 | P | KYUSHU |
| 0786 | 12/04 | 03.24.55 | 35.2 | 27.2 | 4.3 | P | NO DECANESF ISL |
| 0787 | 12/04 | 05.19.32 | 22.2 | 140.9 | 3.7 | P | S OF HONSHU |
| 0788 | 12/04 | 22.52.21 | 35.0 | 72.0 | 3.9 | N | PAKISTAN |
| 0789 | 12/05 | 03.02.12 | 23.3 | 141.0 | 4.2 | P | CEC HONSHU |
| 0790 | 12/05 | 04.11.07 | 23.3 | 140.8 | 4.7 | P | S OF HONSHU |
| 0791 | 12/07 | 02.10.47 | 42.0 | 119.0 | 3.7 | L | NE CHINA |
| 0792 | 12/08 | 04.39.46 | 85.3 | 91.2 | 4.5 | P | N OF SEV ZEMLY |
| 0793 | 12/08 | 05.36.45 | 27.0 | 69.0 | 4.1 | N | AFG-USSR BCP |
| 0794 | 12/08 | 20.16.05 | 24.0 | 121.0 | 4.0 | N | TAIWAN |
| 0795 | 12/09 | 12.21.27 | 50.0 | 157.0 | 3.8 | L | KURIL ISL |
| 0796 | 12/09 | 14.04.49 | 54.0 | 169.0 | 3.5 | L | KOMANDORSKY ISL |
| 0797 | 12/10 | 04.24.58 | 49.8 | 78.1 | 5.7 | P | E KAZAKH |
| 0798 | 12/10 | 04.27.08 | 50.1 | 78.8 | 0.0 | P | E KAZAKH |
| 0799 | 12/10 | 18.26.07 | 44.8 | 149.4 | 6.0 | P | KURIL ISL |
| 0800 | 12/10 | 18.39.37 | 45.0 | 151.0 | 4.2 | L | KURIL ISL |
| 0801 | 12/10 | 23.55.02 | 44.0 | 149.0 | 3.5 | L | KURIL ISL |
| 0802 | 12/11 | 00.22.20 | 44.8 | 149.2 | 4.8 | P | KURIL ISL |
| 0803 | 12/11 | 00.44.11 | 45.0 | 148.0 | 3.6 | L | KURIL ISL |
| 0804 | 12/10 | 01.13.27 | 44.0 | 150.0 | 3.7 | L | KURIL ISL |
| 0805 | 12/11 | 01.30.11 | 38.0 | 22.0 | 3.7 | L | GREECE |
| 0806 | 12/11 | 01.36.59 | 46.0 | 151.0 | 4.3 | L | KURIL ISL |
| 0807 | 12/11 | 02.05.20 | 44.7 | 149.4 | 4.3 | P | KURIL ISL |
| 0808 | 12/11 | 02.26.46 | 45.0 | 148.0 | 3.9 | L | KURIL ISL |
| 0809 | 12/11 | 05.52.00 | 46.0 | 151.0 | 3.6 | L | KURIL ISL |
| 0810 | 12/11 | 07.59.03 | 46.0 | 151.0 | 3.6 | L | KURIL ISL |
| 0811 | 12/11 | 11.10.27 | 44.0 | 153.0 | 3.6 | L | KURIL ISL PFG |
| 0812 | 12/11 | 16.14.46 | 44.8 | 149.2 | 4.3 | P | KURIL ISL |
| 0813 | 12/11 | 19.32.52 | 44.7 | 149.3 | 4.8 | P | KURIL ISL |
| 0814 | 12/12 | 00.08.00 | 45.0 | 149.0 | 4.1 | L | KURIL ISL |
| 0815 | 12/12 | 00.36.04 | 53.1 | 160.0 | 4.7 | P | NFC KAMCHATKA |
| 0816 | 12/12 | 02.22.52 | 38.9 | 21.9 | 3.9 | P | GREECE |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT NO. | DATE | O.T. | COORDINATES | | MB | | SEISMIC AREA |
|--------------|-------|----------|-------------|-------|-----|---|------------------|
| | | | LAT | LONG | | | |
| 0817 | 12/12 | 05.17.02 | 47.0 | 143.0 | 3.6 | L | SAKHALIN ISL |
| 0818 | 12/12 | 09.03.56 | 44.1 | 151.0 | 5.7 | P | KURIL ISL REG |
| 0819 | 12/13 | 01.19.28 | 34.0 | 69.0 | 3.6 | N | AFGANISTAN |
| 0820 | 12/13 | 02.58.52 | 41.6 | 24.0 | 4.5 | P | GREECE-BULGAP |
| 0821 | 12/13 | 04.29.52 | 46.0 | 151.0 | 4.6 | L | KURIL ISL |
| 0822 | 12/13 | 23.48.33 | 45.0 | 150.0 | 4.1 | L | KURIL ISL |
| 0823 | 12/14 | 17.50.22 | 38.2 | 20.2 | 4.7 | P | GREECE |
| 0824 | 12/15 | 02.44.29 | 44.0 | 148.0 | 3.4 | L | KURIL ISL REG |
| 0825 | 12/15 | 14.41.32 | 44.6 | 149.4 | 4.7 | P | KURIL ISL |
| 0826 | 12/15 | 17.55.56 | 35.2 | 27.2 | 4.7 | P | DODECANESE ISL |
| 0827 | 12/16 | 23.00.00 | 85.6 | 85.1 | 4.4 | P | N OF SEV ZEMLY |
| 0828 | 12/17 | 00.18.34 | 44.7 | 149.2 | 5.7 | P | KURIL ISL |
| 0829 | 12/17 | 00.32.23 | 44.7 | 149.3 | 4.8 | P | KURIL ISL |
| 0830 | 12/17 | 00.41.32 | 46.0 | 150.0 | 4.3 | L | KURIL ISL |
| 0831 | 12/17 | 00.52.13 | 45.0 | 150.0 | 3.8 | L | KURIL ISL |
| 0832 | 12/17 | 01.18.17 | 44.8 | 149.2 | 4.7 | P | KURIL ISL |
| 0833 | 12/17 | 01.22.32 | 45.0 | 149.0 | 4.1 | L | KURIL ISL |
| 0834 | 12/17 | 01.26.04 | 44.7 | 149.4 | 4.8 | P | KURIL ISL |
| 0835 | 12/17 | 02.14.21 | 44.0 | 148.0 | 3.7 | L | KURIL ISL |
| 0836 | 12/17 | 05.45.58 | 44.7 | 149.3 | 4.6 | P | KURIL ISL |
| 0837 | 12/17 | 06.24.52 | 44.6 | 149.4 | 4.9 | P | KURIL ISL |
| 0838 | 12/17 | 06.54.07 | 38.0 | 69.0 | 3.4 | N | TADZHIK USSR |
| 0839 | 12/17 | 07.35.31 | 87.0 | 86.0 | 4.0 | L | N OF SEV ZEMLY |
| 0840 | 12/17 | 09.38.51 | 43.0 | 150.0 | 3.8 | L | KURIL ISL REG |
| 0841 | 12/17 | 12.38.12 | 46.0 | 151.0 | 3.7 | L | KURIL ISL |
| 0842 | 12/17 | 12.44.30 | 34.3 | 26.2 | 4.7 | P | CRETE |
| 0843 | 12/17 | 20.48.20 | 49.0 | 160.0 | 3.8 | L | KURIL ISL REG |
| 0844 | 12/19 | 19.34.31 | 35.5 | 27.8 | 4.6 | P | DODECANESE ISL |
| 0845 | 12/20 | 04.15.29 | 31.0 | 67.0 | 4.3 | N | AFGANISTAN |
| 0846 | 12/20 | 11.09.02 | 50.0 | 159.0 | 4.1 | L | KURIL ISL REG |
| 0847 | 12/20 | 13.09.46 | 32.0 | 72.0 | 3.7 | N | PAKISTAN |
| 0848 | 12/21 | 12.31.05 | 54.0 | 162.0 | 4.2 | L | CFC KAMCHATKA |
| 0849 | 12/22 | 00.34.25 | 42.0 | 15.0 | 3.7 | L | CENTRAL ITALY |
| 0850 | 12/22 | 03.01.20 | 56.0 | 164.0 | 4.1 | L | KOMMENDORSKY ISL |
| 0851 | 12/22 | 03.13.44 | 55.0 | 164.0 | 4.1 | L | CFC KAMCHATKA |
| 0852 | 12/22 | 07.33.07 | 49.0 | 156.0 | 4.1 | L | KURIL ISL |
| 0853 | 12/22 | 18.42.39 | 24.0 | 84.0 | 3.9 | N | BURMA-INDIA |
| 0854 | 12/22 | 23.20.22 | 26.0 | 85.0 | 3.8 | N | S SINKIANG |
| 0855 | 12/24 | 19.11.28 | 25.0 | 72.0 | 4.0 | N | PAKISTAN |
| 0856 | 12/25 | 09.14.04 | 40.6 | 27.4 | 3.7 | P | TURKEY |
| 0857 | 12/25 | 12.30.52 | 53.1 | 162.9 | 4.8 | P | CFC KAMCHATKA |
| 0858 | 12/25 | 12.55.52 | 45.5 | 149.8 | 4.7 | P | KURIL ISL |
| 0859 | 12/25 | 18.55.58 | 53.0 | 159.4 | 5.7 | P | CFC KAMCHATKA |
| 0860 | 12/25 | 20.54.27 | 53.0 | 162.0 | 3.5 | L | CFC KAMCHATKA |
| 0861 | 12/26 | 06.13.50 | 24.0 | 67.0 | 3.6 | N | PAKISTAN |
| 0862 | 12/26 | 18.35.22 | 28.4 | 52.7 | 4.6 | P | S IRAN |
| 0863 | 12/27 | 08.15.11 | 39.0 | 25.0 | 3.6 | N | AFGHAN SEA |
| 0864 | 12/28 | 02.59.18 | 46.0 | 151.0 | 4.0 | L | KURIL ISL |

EVENT LIST 1 JAN 72 THROUGH 31 DEC 72

| EVENT | | | COORDINATES | | MR | | SEISMIC AREA |
|-------|-------|----------|-------------|-------|-----|---|----------------|
| NO. | DATE | O.T. | LAT | LONG | | | |
| 0865 | 12/28 | 04.26.55 | 50.0 | 79.0 | 4.5 | L | E KAZAKH |
| 0866 | 12/28 | 05.24.44 | 40.8 | 20.6 | 3.5 | P | GREECE-ALBANIA |
| 0867 | 12/28 | 21.52.19 | 49.0 | 157.0 | 4.1 | L | KURIL ISL REG |
| 0868 | 12/29 | 05.02.44 | 56.0 | 163.0 | 4.3 | L | CEC KAMCHATKA |
| 0869 | 12/29 | 11.26.29 | 53.8 | 169.0 | 4.3 | P | KOMANDORSKY |
| 0870 | 12/30 | 05.25.49 | 30.0 | 85.0 | 4.1 | N | TIRET |
| 0871 | 12/30 | 07.45.43 | 44.0 | 149.0 | 3.8 | L | KURIL ISL |
| 0872 | 12/30 | 09.08.08 | 32.0 | 48.0 | 3.8 | N | IRAN-IRAQ BCR |
| 0873 | 12/30 | 13.29.36 | 33.7 | 87.6 | 4.5 | P | TIRET |
| 0874 | 12/30 | 15.21.07 | 40.4 | 25.8 | 4.4 | P | AEGEAN SEA |
| 0875 | 12/30 | 21.54.06 | 33.6 | 87.7 | 4.9 | P | TIRET |
| 0876 | 12/31 | 00.56.53 | 33.0 | 88.0 | 4.1 | N | TIRET |
| 0877 | 12/31 | 02.49.24 | 36.0 | 85.0 | 3.9 | N | S SINKIANG |

Abbreviations:

I = ISM

L = LASA

N = NORSAR

P = PDE

APPENDIX II- B
BASIC DATA FOR CTA

CTA 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 310 | 68.4 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 311 | 97.7 | 3.60 | 4.15 | 3.93 | 0.0 | 1.25 | 101 |
| 312 | 75.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 313 | 127.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 314 | 76.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 315 | 102.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 316 | 70.3 | 3.80 | 4.18 | 3.80 | 3.11 | 0.34 | 101 |
| 317 | 85.8 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 318 | 85.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 319 | 86.9 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 320 | 86.4 | 3.90 | 4.27 | 3.76 | 0.0 | 0.0 | 601 |
| 321 | 76.0 | 3.70 | 3.77 | 3.28 | 0.0 | 0.0 | 101 |
| 322 | 68.7 | 4.30 | 0.0 | 3.56 | 0.0 | 0.0 | 301 |
| 323 | 48.1 | *5.00 | 4.24 | 4.03 | 3.36 | 0.94 | 101 |
| 324 | 102.3 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 326 | 73.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 327 | 75.7 | 3.40 | 3.38 | 0.0 | 0.0 | 0.83 | 101 |
| 328 | 75.8 | 3.50 | 3.49 | 0.0 | 0.0 | 0.84 | 101 |
| 329 | 114.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 330 | 70.9 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 331 | 77.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 332 | 129.4 | 4.20 | 0.0 | 3.59 | 0.0 | 0.0 | 101 |
| 333 | 109.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 334 | 88.4 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 335 | 111.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 336 | 64.1 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 337 | 69.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 338 | 77.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 339 | 92.0 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 340 | 77.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 341 | 48.4 | 5.40 | 5.08 | 4.61 | 4.23 | 3.21 | 101 |
| 342 | 109.2 | 4.90 | 4.37 | 4.00 | 0.0 | 1.00 | 101 |
| 343 | 48.2 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 344 | 112.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 345 | 64.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 346 | 48.3 | 4.70 | 3.74 | 3.33 | 0.0 | 3.10 | 101 |
| 347 | 110.0 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 348 | 71.8 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 101 |
| 349 | 67.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 350 | 125.4 | 4.90 | 0.0 | 3.47 | 3.14 | 2.68 | 101 |
| 351 | 101.2 | 4.90 | 4.61 | 4.43 | 3.80 | 2.22 | 101 |
| 352 | 111.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 353 | 104.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 354 | 90.9 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 355 | 63.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 356 | 108.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 357 | 74.1 | 3.20 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 358 | 68.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 359 | 67.3 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |

CTA 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|-----------|--------------------|-------|------------|------------|------------|-------------|---------|
| 360 | 64.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 361 | 108.9 | 5.40 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 362 | 109.0 | 5.10 | 4.98 | 4.56 | 3.90 | 4.72 | 101 |
| 363 | 74.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 365 | 76.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 366 | 106.0 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 367 | 109.0 | 5.30 | 0.0 | 4.01 | 0.0 | 0.81 | 101 |
| 369 | 103.7 | 3.50 | 3.85 | 3.41 | 2.85 | 0.0 | 101 |
| 370 | 99.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 371 | 134.4 | *4.50 | 4.04 | 3.93 | 3.49 | 0.60 | 101 |
| 415 | 95.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 416 | 88.4 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 417 | 74.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 418 | 66.8 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 419 | 88.4 | *5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 420 | 111.2 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 421 | 91.7 | 5.10 | 4.01 | 3.61 | 0.0 | 0.0 | 101 |
| 422 | 129.5 | *4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 423 | 74.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 424 | 77.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 425 | 76.6 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 426 | 120.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 427 | 118.5 | 5.60 | 4.92 | 4.63 | 4.28 | 2.06 | 101 |
| 428 | 74.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 429 | 102.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 430 | 99.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 431 | 91.4 | *4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 463 | 127.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 464 | 66.6 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 465 | 68.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 466 | 131.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 467 | 50.4 | 4.10 | 3.80 | 3.44 | 2.95 | 0.0 | 101 |
| 468 | 52.8 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 469 | 74.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 470 | 82.6 | 4.70 | 0.0 | 3.42 | 0.0 | 0.0 | 101 |
| 471 | 90.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 472 | 68.9 | 5.20 | 3.79 | 3.56 | 0.0 | 1.25 | 101 |
| 473 | 76.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 474 | 97.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 475 | 110.0 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 476 | 69.9 | 5.20 | 3.84 | 3.80 | 3.24 | 0.0 | 101 |
| 477 | 87.7 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 478 | 77.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 479 | 129.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 480 | 69.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 481 | 75.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 482 | 64.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 483 | 93.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 484 | 134.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |

CTA 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LG/LR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 485 | 47.8 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 486 | 121.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 487 | 104.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 488 | 104.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 489 | 104.3 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 490 | 51.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 491 | 88.8 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 492 | 48.8 | 5.10 | 4.52 | 3.94 | 3.38 | 0.0 | 101 |
| 493 | 67.3 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 494 | 73.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 495 | 66.1 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 496 | 71.3 | 5.20 | 3.87 | 3.73 | 3.43 | 0.0 | 101 |
| 498 | 71.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 499 | 50.1 | 4.00 | 3.93 | 3.69 | 3.21 | 0.93 | 101 |
| 500 | 64.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 501 | 75.8 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 502 | 64.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 503 | 71.8 | 4.20 | 3.94 | 3.28 | 0.0 | 0.0 | 101 |
| 504 | 122.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 505 | 75.9 | 5.30 | 3.95 | 4.01 | 3.64 | 0.0 | 101 |
| 506 | 78.2 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 507 | 129.0 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 508 | 63.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 509 | 76.0 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 510 | 87.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 511 | 99.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 512 | 127.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 513 | 65.1 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 514 | 73.4 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 515 | 76.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 517 | 71.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 518 | 102.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 521 | 117.6 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 522 | 73.5 | 5.50 | 4.91 | 4.69 | 4.29 | 1.00 | 101 |
| 523 | 73.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 524 | 127.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 525 | 73.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 526 | 78.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 527 | 114.8 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 528 | 79.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 529 | 83.5 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 530 | 129.3 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 531 | 65.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 532 | 109.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 533 | 134.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 534 | 71.0 | 5.10 | 4.15 | 3.88 | 0.0 | 1.43 | 101 |
| 535 | 48.0 | 5.10 | 4.13 | 3.98 | 3.24 | 0.0 | 101 |
| 536 | 86.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 541 | 69.8 | 5.10 | 4.06 | 3.78 | 3.72 | 0.0 | 101 |

CTA 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 542 | 93.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 543 | 48.0 | 4.90 | 3.72 | 3.86 | 0.0 | 0.76 | 101 |
| 544 | 66.4 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 546 | 77.6 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 547 | 49.9 | 4.60 | 4.44 | 3.69 | 3.35 | 0.0 | 101 |
| 548 | 103.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 549 | 52.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 550 | 89.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 551 | 120.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 552 | 90.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 231 |
| 553 | 89.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 554 | 118.4 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 555 | 127.4 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 231 |
| 556 | 63.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 557 | 98.7 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 558 | 77.5 | 5.60 | 5.10 | 4.57 | 4.49 | 1.11 | 101 |
| 559 | 77.5 | 5.00 | 4.46 | 4.66 | 4.16 | 0.85 | 101 |
| 560 | 98.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 561 | 120.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 562 | 67.2 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 563 | 77.2 | 4.00 | 3.86 | 3.22 | 0.0 | 0.0 | 131 |
| 564 | 121.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 565 | 80.8 | 5.30 | 4.31 | 4.08 | 0.0 | 0.0 | 101 |
| 566 | 120.5 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 567 | 98.7 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 568 | 49.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 624 | 67.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 626 | 92.1 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 635 | 64.1 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 636 | 65.2 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 637 | 74.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 638 | 72.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 650 | 65.1 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 651 | 63.6 | 4.90 | 0.0 | 0.0 | 4.05 | 0.0 | 131 |
| 652 | 110.3 | 5.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 653 | 72.6 | 5.20 | 4.16 | 3.69 | 0.0 | 4.67 | 101 |
| 654 | 76.9 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 655 | 67.2 | 4.00 | 3.33 | 3.09 | 2.82 | 0.0 | 101 |
| 656 | 73.6 | 4.80 | 3.39 | 3.23 | 0.0 | 1.37 | 101 |
| 657 | 66.1 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 658 | 73.6 | *4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 659 | 126.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 221 |
| 660 | 67.4 | 4.10 | 3.34 | 2.73 | 0.0 | 0.0 | 131 |
| 661 | 70.9 | 5.20 | 0.0 | 3.81 | 3.41 | 0.0 | 101 |
| 662 | 86.7 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 321 |
| 663 | 49.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 664 | 69.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 665 | 123.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 666 | 71.7 | 3.20 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |

CTA 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 667 | 71.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 321 |
| 668 | 74.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 669 | 68.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 231 |
| 696 | 95.7 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 697 | 57.0 | 4.40 | 5.04 | 4.73 | 4.24 | 0.0 | 101 |
| 698 | 63.5 | 4.80 | 3.93 | 3.80 | 3.13 | 0.0 | 101 |
| 699 | 91.8 | 6.20 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 700 | 90.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 701 | 103.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 702 | 91.2 | 5.50 | 4.88 | 4.32 | 4.32 | 0.80 | 101 |
| 730 | 127.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 731 | 109.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 231 |
| 732 | 65.9 | 4.40 | 3.30 | 3.41 | 0.0 | 1.25 | 101 |
| 733 | 127.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 231 |
| 734 | 130.3 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 735 | 64.3 | 4.00 | 0.0 | 2.86 | 3.03 | 0.0 | 161 |
| 736 | 64.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 737 | 73.8 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 231 |
| 738 | 64.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 251 |
| 739 | 66.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 231 |
| 741 | 128.9 | *4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 742 | 104.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 743 | 85.1 | 4.00 | 4.30 | 3.69 | 3.27 | 0.0 | 101 |
| 744 | 50.0 | 5.70 | 5.71 | 5.45 | 4.82 | 0.27 | 101 |
| 745 | 49.6 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 746 | 103.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 747 | 122.2 | 4.10 | 4.29 | 4.14 | 3.57 | 0.0 | 161 |
| 748 | 89.5 | 4.00 | 3.82 | 0.0 | 0.0 | 0.0 | 101 |
| 749 | 87.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 750 | 85.8 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 751 | 128.6 | 4.30 | 3.97 | 3.30 | 0.0 | 0.0 | 131 |
| 752 | 129.0 | 5.40 | 0.0 | 0.0 | 0.0 | 0.0 | 101 |
| 753 | 108.9 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 754 | 103.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 755 | 100.9 | 5.20 | 3.52 | 3.36 | 0.0 | 3.24 | 131 |
| 756 | 73.2 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 757 | 70.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 758 | 78.8 | 5.10 | 3.90 | 3.87 | 0.0 | 1.52 | 101 |
| 759 | 128.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 760 | 101.5 | 5.60 | 0.0 | 0.0 | 0.0 | 0.0 | 231 |
| 761 | 73.0 | 5.20 | 3.62 | 3.44 | 0.0 | 0.0 | 101 |
| 762 | 134.5 | 4.90 | 4.08 | 3.72 | 3.52 | 0.0 | 131 |
| 763 | 102.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 231 |
| 764 | 74.6 | 4.70 | 3.48 | 2.75 | 0.0 | 0.0 | 131 |
| 765 | 124.2 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 766 | 76.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 767 | 125.3 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 768 | 89.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 769 | 89.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |

CTA 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 770 | 93.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 772 | 74.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 809 | 66.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 810 | 66.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 811 | 64.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 812 | 64.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 813 | 64.8 | **** | 4.00 | 3.66 | 3.40 | 0.0 | 101 |
| 814 | 65.1 | 4.10 | 3.42 | 3.02 | 0.0 | 0.0 | 101 |
| 815 | 74.1 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 816 | 128.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 817 | 67.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 818 | 64.3 | 5.70 | 0.0 | 4.38 | 4.03 | 1.10 | 101 |
| 819 | 91.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 820 | 127.1 | *4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 821 | 66.2 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 822 | 65.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 823 | 130.3 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 824 | 64.1 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 825 | 65.0 | 4.70 | 4.22 | 3.66 | 0.0 | 2.63 | 101 |
| 826 | 124.8 | 4.70 | 0.0 | 3.51 | 0.0 | 0.0 | 131 |
| 827 | 107.9 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 828 | 64.8 | 5.70 | 5.33 | 5.28 | 5.02 | 2.55 | 101 |
| 829 | 64.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 830 | 66.2 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 831 | 65.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 832 | 64.9 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 833 | 65.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 834 | 64.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 835 | 64.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 836 | 64.8 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 837 | 64.7 | 4.90 | 3.76 | 3.16 | 0.0 | 4.02 | 101 |
| 838 | 92.8 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 839 | 108.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 840 | 63.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 841 | 66.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 842 | 125.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 843 | 70.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 844 | 124.3 | 4.60 | 4.31 | 4.10 | 3.21 | 0.21 | 101 |
| 845 | 91.5 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 846 | 71.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 847 | 88.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 848 | 75.3 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 849 | 133.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 850 | 77.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 851 | 76.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 852 | 69.6 | 4.10 | 0.0 | 3.44 | 0.0 | 0.0 | 161 |
| 853 | 67.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 854 | 80.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 855 | 89.3 | 4.00 | 8.0 | 0.0 | 0.0 | 0.0 | 201 |

CTA 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 856 | 124.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 857 | 74.6 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 858 | 65.7 | 4.70 | 3.56 | 3.44 | 2.88 | 0.0 | 101 |
| 859 | 74.0 | 5.70 | 5.04 | 5.19 | 4.62 | 0.90 | 101 |
| 860 | 74.3 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 301 |
| 861 | 88.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 862 | 102.4 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 863 | 126.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 864 | 66.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 865 | 92.3 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 866 | 129.7 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 867 | 69.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 868 | 77.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 869 | 76.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 201 |
| 870 | 77.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 871 | 64.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 872 | 107.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 873 | 77.5 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 874 | 125.8 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 875 | 77.4 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |

APPENDIX II-C
BASIC DATA FOR CHG

CHG 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DFGREFS) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 1 | 56.5 | 4.10 | 3.85 | 3.55 | 2.81 | 2.90 | 102 |
| 2 | 54.7 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 3 | 54.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 4 | 47.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 5 | 69.5 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 6 | 26.1 | 5.20 | 4.23 | 3.32 | 3.05 | 4.47 | 102 |
| 7 | 57.1 | 4.80 | 3.84 | 0.0 | 0.0 | 0.43 | 102 |
| 8 | 57.0 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 9 | 46.2 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 10 | 59.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 11 | 21.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 12 | 60.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 13 | 22.0 | *4.60 | 4.60 | 3.27 | 2.98 | 1.34 | 102 |
| 14 | 32.3 | 3.90 | 4.23 | 4.38 | 3.40 | 0.78 | 102 |
| 15 | 41.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 16 | 47.3 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 17 | 71.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 18 | 29.5 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 19 | 63.7 | 4.00 | 3.80 | 3.39 | 0.0 | 1.50 | 102 |
| 20 | 59.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 21 | 31.6 | 4.70 | 3.51 | 0.0 | 0.0 | 3.98 | 102 |
| 22 | 23.2 | 4.70 | 3.65 | 3.18 | 0.0 | 4.72 | 102 |
| 23 | 45.2 | 5.20 | 3.14 | 0.0 | 0.0 | 3.97 | 102 |
| 24 | 29.8 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 25 | 51.3 | 4.20 | 2.81 | 0.0 | 0.0 | 0.0 | 602 |
| 26 | 19.0 | 4.70 | 5.46 | 3.93 | 0.0 | 1.24 | 102 |
| 27 | 19.2 | 4.60 | 4.76 | 4.00 | 4.11 | 1.05 | 102 |
| 28 | 60.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 29 | 60.4 | 4.30 | 3.56 | 0.0 | 0.0 | 2.86 | 102 |
| 30 | 48.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 31 | 20.3 | 5.00 | 4.16 | 4.16 | 3.78 | 1.00 | 102 |
| 32 | 60.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 33 | 62.8 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 34 | 47.6 | 4.00 | 3.93 | 0.0 | 0.0 | 0.0 | 102 |
| 35 | 62.2 | 4.40 | 0.0 | 2.65 | 0.0 | 0.0 | 102 |
| 36 | 67.7 | 4.90 | 3.93 | 4.14 | 3.93 | 2.32 | 102 |
| 37 | 60.5 | 4.80 | 4.10 | 0.0 | 3.58 | 0.60 | 102 |
| 38 | 60.3 | 4.00 | 4.23 | 0.0 | 3.56 | 0.98 | 102 |
| 39 | 54.4 | 5.30 | 5.05 | 4.68 | 4.17 | 6.40 | 102 |
| 40 | 66.0 | 3.90 | 3.48 | 0.0 | 0.0 | 5.99 | 302 |
| 41 | 48.4 | 5.10 | 0.0 | 3.59 | 2.90 | 2.44 | 102 |
| 42 | 54.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 43 | 41.8 | 4.70 | 3.19 | 0.0 | 0.0 | 5.06 | 102 |
| 44 | 27.5 | 5.40 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 45 | 26.3 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 46 | 59.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 47 | 60.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 48 | 65.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 49 | 48.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |

CHG 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DFGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|-----------|--------------------|-------|---------------|---------------|---------------|----------------|---------|
| 50 | 47.9 | 4.90 | 3.80 | 0.0 | 2.95 | 0.0 | 102 |
| 51 | 77.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 52 | 64.6 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 53 | 51.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 54 | 52.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 55 | 62.3 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 56 | 56.4 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 57 | 59.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 58 | 56.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 59 | 58.5 | 4.60 | 0.0 | 3.67 | 0.0 | 1.33 | 102 |
| 61 | 22.0 | 4.80 | 4.03 | 0.0 | 3.20 | 0.61 | 102 |
| 62 | 22.2 | 4.60 | 3.96 | 3.91 | 0.0 | 0.57 | 102 |
| 60 | 74.0 | *4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 63 | 74.0 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 65 | 61.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 66 | 54.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 67 | 44.7 | 3.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 68 | 54.4 | 4.00 | 3.18 | 0.0 | 0.0 | 4.01 | 102 |
| 69 | 54.4 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 70 | 60.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 71 | 25.6 | 3.80 | 0.0 | 2.54 | 0.0 | 4.17 | 102 |
| 72 | 26.7 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 73 | 31.0 | 5.90 | 4.17 | 2.80 | 0.0 | 1.65 | 102 |
| 74 | 49.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 75 | 26.7 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 76 | 30.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 77 | 40.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 78 | 55.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 79 | 27.9 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 80 | 35.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 83 | 57.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 84 | 59.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 85 | 47.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 87 | 69.0 | 4.60 | 3.40 | 2.52 | 0.0 | 1.55 | 102 |
| 88 | 48.2 | 5.10 | 0.0 | 3.93 | 0.0 | 0.0 | 102 |
| 89 | 5.6 | 4.50 | 3.52 | 3.07 | 0.0 | 0.0 | 102 |
| 90 | 74.1 | *4.50 | 4.68 | 4.57 | 0.0 | 1.41 | 102 |
| 91 | 35.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 92 | 74.1 | 4.80 | 3.33 | 0.0 | 0.0 | 1.54 | 102 |
| 93 | 53.2 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 94 | 74.1 | 4.40 | 3.27 | 3.27 | 0.0 | 1.07 | 102 |
| 95 | 17.4 | 5.20 | 3.87 | 3.64 | 0.0 | 0.96 | 102 |
| 96 | 46.1 | 4.50 | 3.02 | 2.88 | 0.0 | 0.78 | 102 |
| 97 | 74.1 | *4.10 | 3.24 | 3.10 | 0.0 | 1.87 | 102 |
| 98 | 74.0 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 99 | 74.1 | *4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 100 | 73.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 101 | 74.1 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 102 | 73.9 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |

CHG 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 103 | 73.9 | *4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 104 | 74.0 | *4.30 | 3.30 | 2.98 | 0.0 | 2.12 | 102 |
| 105 | 74.0 | *4.20 | 3.43 | 3.13 | 0.0 | 2.39 | 102 |
| 106 | 74.1 | *4.40 | 3.29 | 3.27 | 0.0 | 1.99 | 102 |
| 107 | 13.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 108 | 26.9 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 109 | 31.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 110 | 74.1 | *3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 111 | 75.3 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 112 | 21.8 | 5.70 | 4.42 | 0.0 | 4.10 | 3.52 | 102 |
| 113 | 74.1 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 114 | 22.4 | 4.80 | 3.93 | 3.61 | 3.56 | 1.41 | 102 |
| 115 | 44.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 116 | 35.1 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 117 | 44.8 | 4.50 | 3.72 | 3.31 | 0.0 | 1.81 | 102 |
| 118 | 44.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 119 | 44.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 120 | 28.1 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 121 | 14.9 | 4.30 | 2.63 | 2.42 | 0.0 | 0.0 | 102 |
| 122 | 61.2 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 123 | 60.0 | 4.60 | 4.04 | 0.0 | 3.30 | 0.76 | 102 |
| 145 | 48.1 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 146 | 48.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 147 | 48.1 | 4.90 | 3.11 | 2.49 | 0.0 | 0.0 | 102 |
| 148 | 49.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 149 | 68.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 150 | 31.8 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 151 | 27.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 152 | 59.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 153 | 55.7 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 154 | 45.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 155 | 55.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 156 | 53.8 | 5.00 | 4.01 | 3.51 | 2.63 | 0.0 | 102 |
| 157 | 53.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 158 | 54.5 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 159 | 51.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 160 | 53.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 161 | 55.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 162 | 47.8 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 165 | 47.5 | 4.90 | 3.70 | 2.66 | 2.29 | 0.83 | 102 |
| 168 | 59.3 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 169 | 46.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 170 | 50.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 171 | 6.8 | 4.70 | 2.55 | 1.66 | 0.0 | 0.0 | 102 |
| 172 | 30.6 | 5.30 | 3.82 | 3.00 | 3.00 | 0.0 | 102 |
| 173 | 73.2 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 174 | 71.1 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 175 | 69.1 | 4.90 | 3.70 | 3.30 | 3.02 | 0.0 | 102 |
| 177 | 71.3 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |

CHG 01/01/72 - 12/31/72

| FVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LO/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 178 | 56.4 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 179 | 71.3 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 180 | 21.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 181 | 33.7 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 182 | 48.5 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 183 | 29.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 184 | 60.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 186 | 31.2 | 3.90 | 2.36 | 1.59 | 0.0 | 0.0 | 102 |
| 187 | 45.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 188 | 45.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 189 | 45.0 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 190 | 45.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 191 | 36.9 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 192 | 46.9 | 3.80 | 3.03 | 2.46 | 0.0 | 0.0 | 102 |
| 193 | 31.1 | 4.40 | 2.77 | 2.13 | 0.0 | 0.0 | 102 |
| 194 | 46.0 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 195 | 42.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 196 | 45.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 197 | 48.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 198 | 45.4 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 199 | 45.4 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 200 | 45.8 | 4.40 | 4.11 | 3.74 | 3.08 | 0.0 | 102 |
| 201 | 45.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 202 | 44.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 203 | 47.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 204 | 46.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 205 | 58.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 206 | 47.4 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 207 | 43.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 208 | 44.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 209 | 39.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 210 | 51.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 211 | 72.1 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 212 | 60.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 213 | 45.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 214 | 29.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 216 | 59.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 218 | 68.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 219 | 59.9 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 220 | 58.6 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 231 | 49.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 232 | 69.9 | *4.40 | 2.68 | 2.17 | 0.0 | 0.0 | 102 |
| 283 | 20.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 284 | 41.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 285 | 31.7 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 286 | 50.7 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 287 | 37.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 288 | 25.3 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 289 | 9.6 | 3.60 | 0.0 | 2.42 | 1.95 | 0.0 | 102 |

CHG 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 290 | 24.2 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 292 | 54.5 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 152 |
| 293 | 45.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 294 | 32.4 | 5.20 | 4.06 | 3.48 | 0.0 | 1.90 | 102 |
| 295 | 42.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 296 | 25.3 | 3.50 | 2.54 | 0.0 | 0.0 | 0.0 | 102 |
| 297 | 47.2 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 152 |
| 298 | 31.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 299 | 60.3 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 300 | 57.0 | 4.70 | 2.97 | 0.0 | 0.0 | 0.0 | 102 |
| 301 | 52.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 302 | 32.0 | 3.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 303 | 56.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 304 | 56.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 308 | 36.2 | 3.40 | 2.86 | 2.28 | 1.70 | 0.0 | 102 |
| 309 | 26.8 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 670 | 57.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 671 | 51.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 672 | 35.5 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 673 | 13.3 | 3.80 | 2.67 | 2.18 | 0.0 | 0.0 | 102 |
| 674 | 62.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 675 | 5.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 676 | 4.1 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 677 | 30.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 678 | 60.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 679 | 59.7 | 6.30 | 4.53 | 4.07 | 3.65 | 0.78 | 102 |
| 680 | 35.2 | 5.20 | 4.12 | 3.63 | 3.25 | 0.59 | 132 |
| 681 | 53.8 | 3.70 | 3.23 | 2.86 | 0.0 | 0.0 | 102 |
| 682 | 47.5 | 3.70 | 0.0 | 2.89 | 0.0 | 0.0 | 132 |
| 683 | 65.1 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 684 | 65.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 685 | 21.4 | 3.70 | 3.12 | 2.75 | 0.0 | 0.0 | 102 |
| 686 | 72.0 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 701 | 44.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 702 | 30.7 | 5.50 | 5.16 | 5.04 | 4.61 | 0.0 | 102 |
| 703 | 29.3 | 3.80 | 0.0 | 2.65 | 0.0 | 0.0 | 132 |
| 704 | 66.6 | 5.20 | 4.82 | 4.46 | 4.58 | 0.80 | 102 |
| 705 | 30.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 706 | 59.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 707 | 66.5 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 232 |
| 708 | 12.5 | *4.50 | 3.95 | 3.86 | 3.97 | 0.0 | 102 |
| 709 | 32.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 710 | 47.9 | 4.30 | 3.94 | 3.30 | 2.64 | 0.0 | 102 |
| 711 | 20.7 | *5.30 | 4.59 | 4.45 | 3.69 | 2.78 | 102 |
| 712 | 29.1 | 4.30 | 3.50 | 0.0 | 0.0 | 0.0 | 102 |
| 713 | 57.1 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 714 | 66.7 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 715 | 50.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 716 | 21.7 | 5.50 | 4.62 | 4.56 | 3.76 | 0.45 | 102 |

CHG 01/01/72 - 12/31/72

| EVNT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|-------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 717 | 69.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 718 | 39.1 | 4.70 | 4.46 | 4.07 | 3.72 | 0.76 | 132 |
| 719 | 63.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 720 | 53.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 721 | 39.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 322 |
| 722 | 29.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 723 | 59.4 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 724 | 49.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 232 |
| 725 | 45.2 | 3.90 | 0.0 | 3.08 | 2.69 | 0.0 | 102 |
| 726 | 22.7 | 4.10 | 3.73 | 3.34 | 0.0 | 0.0 | 102 |
| 727 | 43.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 728 | 64.3 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 729 | 29.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 730 | 67.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 731 | 49.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 732 | 5.9 | 4.40 | 4.01 | 3.47 | 0.0 | 0.0 | 102 |
| 733 | 67.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 734 | 69.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 735 | 50.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 736 | 48.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 737 | 57.8 | 4.60 | 3.81 | 0.0 | 3.02 | 0.0 | 102 |
| 738 | 48.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 739 | 52.7 | 4.00 | 0.0 | 3.09 | 0.0 | 0.26 | 132 |
| 741 | 68.5 | *4.80 | 0.0 | 3.17 | 2.40 | 0.0 | 132 |
| 742 | 44.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 102 |
| 743 | 27.3 | 4.00 | 3.17 | 2.78 | 0.0 | 0.77 | 102 |
| 744 | 21.7 | 5.70 | 5.56 | 5.11 | 0.0 | 0.44 | 102 |
| 745 | 21.0 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 746 | 47.3 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 232 |
| 747 | 62.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 748 | 29.1 | 4.00 | 2.99 | 2.73 | 0.0 | 0.0 | 102 |
| 749 | 27.1 | 4.00 | 0.0 | 3.16 | 2.50 | 0.0 | 102 |
| 750 | 25.6 | 4.90 | 3.72 | 0.0 | 3.26 | 0.0 | 102 |
| 751 | 68.2 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 753 | 50.2 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 754 | 44.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 755 | 42.8 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 232 |
| 756 | 57.0 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 757 | 14.3 | 3.90 | 0.0 | 3.26 | 2.36 | 0.0 | 102 |
| 758 | 41.7 | 5.10 | 4.19 | 3.56 | 0.0 | 0.0 | 102 |
| 759 | 68.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 760 | 42.3 | 5.60 | 3.95 | 3.35 | 2.94 | 0.0 | 102 |
| 761 | 56.9 | 5.20 | 3.68 | 3.50 | 3.34 | 0.0 | 102 |
| 762 | 74.1 | 4.90 | 0.0 | 3.94 | 0.0 | 0.0 | 102 |
| 763 | 44.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 764 | 58.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 765 | 64.2 | 4.80 | 4.05 | 3.56 | 2.75 | 0.0 | 102 |
| 766 | 59.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 767 | 65.6 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |

CHG 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 768 | 29.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 769 | 29.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 770 | 60.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 771 | 134.5 | *4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 501 |
| 771 | 74.2 | *4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 772 | 58.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 800 | 50.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 773 | 74.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 774 | 43.8 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 102 |
| 775 | 39.8 | 5.40 | 5.25 | 4.75 | 4.38 | 0.40 | 102 |
| 776 | 59.3 | 4.80 | 3.82 | 3.27 | 3.09 | 0.50 | 102 |
| 777 | 40.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 778 | 64.7 | 5.10 | 4.04 | 3.96 | 3.27 | 0.0 | 102 |
| 779 | 40.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 780 | 45.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 781 | 29.0 | 5.00 | 3.85 | 3.50 | 2.96 | 0.99 | 102 |
| 782 | 46.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 783 | 58.3 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 784 | 49.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 785 | 32.0 | 5.30 | 4.92 | 4.11 | 0.0 | 0.0 | 102 |
| 786 | 64.7 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 787 | 40.0 | 3.70 | 0.0 | 3.14 | 2.84 | 0.82 | 102 |
| 788 | 28.8 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 789 | 40.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 790 | 40.0 | 4.70 | 3.54 | 3.54 | 0.0 | 0.0 | 102 |
| 791 | 28.8 | 3.70 | 0.0 | 3.16 | 0.0 | 0.89 | 132 |
| 792 | 84.6 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 793 | 31.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 794 | 21.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 795 | 55.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 796 | 63.2 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 797 | 35.2 | 5.70 | 3.51 | 3.81 | 3.01 | 0.83 | 102 |
| 799 | 49.1 | 6.00 | 6.02 | 5.34 | 4.73 | 0.85 | 102 |
| 801 | 48.6 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 802 | 49.0 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 803 | 48.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 804 | 49.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 805 | 68.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 806 | 50.5 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 807 | 49.1 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 808 | 48.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 809 | 50.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 810 | 50.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 811 | 51.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 812 | 49.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 813 | 49.0 | 4.80 | 4.22 | 3.41 | 0.0 | 0.41 | 102 |
| 814 | 48.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 815 | 57.8 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 816 | 68.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |

CHG 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 817 | 45.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 818 | 50.0 | 5.70 | 4.54 | 3.75 | 3.41 | 0.74 | 102 |
| 819 | 30.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 820 | 66.6 | *4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 821 | 50.5 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 822 | 49.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 823 | 69.9 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 824 | 47.9 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 825 | 49.0 | 4.70 | 4.41 | 3.95 | 3.24 | 1.33 | 102 |
| 826 | 64.7 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 827 | 66.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 828 | 48.9 | 5.70 | 6.08 | 5.40 | 0.0 | 0.0 | 102 |
| 829 | 49.0 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 830 | 49.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 831 | 49.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 832 | 49.0 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 833 | 48.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 834 | 49.1 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 835 | 47.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 836 | 49.0 | 4.60 | 3.71 | 3.54 | 0.0 | 0.96 | 102 |
| 837 | 49.0 | 4.90 | 3.14 | 3.50 | 4.12 | 1.63 | 102 |
| 838 | 32.4 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 839 | 68.2 | 4.00 | 3.81 | 3.34 | 3.05 | 1.42 | 102 |
| 840 | 49.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 841 | 50.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 842 | 65.6 | 4.70 | 3.81 | 3.47 | 3.15 | 0.25 | 102 |
| 843 | 57.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 844 | 64.2 | 4.60 | 4.40 | 4.22 | 3.89 | 0.0 | 102 |
| 845 | 31.3 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 846 | 56.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 847 | 27.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 848 | 59.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 849 | 73.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 302 |
| 850 | 60.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 851 | 60.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 852 | 54.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 853 | 7.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 854 | 21.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 855 | 28.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |
| 856 | 64.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 857 | 59.5 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 202 |
| 858 | 49.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 602 |
| 859 | 57.4 | 5.70 | 5.37 | 5.07 | 4.70 | 0.51 | 102 |
| 860 | 59.0 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 502 |

APPENDIX II-D
BASIC DATA FOR FBK

FBK 01/01/72 - 03/20/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 3 | 32.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 4 | 39.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 5 | 76.8 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 6 | 65.7 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 7 | 29.6 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 8 | 29.4 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 9 | 36.1 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 10 | 26.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 11 | 69.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 12 | 24.9 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 13 | 69.7 | *4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 14 | 53.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 15 | 44.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 16 | 40.8 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 17 | 66.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 18 | 72.4 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 19 | 21.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 603 |
| 20 | 25.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 21 | 69.8 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 22 | 68.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 23 | 83.7 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 24 | 73.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 25 | 70.5 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 503 |
| 26 | 71.4 | 4.70 | 6.17 | 3.84 | 0.0 | 0.35 | 103 |
| 27 | 70.5 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 28 | 25.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 29 | 24.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 30 | 39.2 | 3.80 | 3.69 | 0.0 | 0.0 | 0.0 | 103 |
| 31 | 71.8 | 5.00 | 5.90 | 4.64 | 6.11 | 1.43 | 103 |
| 32 | 24.9 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 33 | 23.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 34 | 41.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 35 | 77.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 503 |
| 36 | 79.9 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 38 | 25.1 | 4.00 | 3.48 | 0.0 | 0.0 | 0.50 | 103 |
| 39 | 27.9 | 5.30 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 37 | 24.9 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 40 | 16.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 41 | 81.6 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 42 | 32.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 43 | 40.7 | 4.70 | 3.58 | 0.0 | 0.0 | 1.31 | 103 |
| 44 | 68.6 | 5.40 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 45 | 69.3 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 46 | 25.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 47 | 25.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 48 | 80.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 49 | 39.3 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 50 | 76.8 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 51 | 69.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |

FRK 01/01/72 - 03/20/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 52 | 78.4 | 4.80 | C.C | 0.0 | 0.0 | 0.0 | 303 |
| 53 | 71.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 54 | 33.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 55 | 77.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 56 | 29.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 503 |
| 57 | 25.3 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 303 |
| 58 | 30.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 59 | 27.3 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 60 | 70.3 | *4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 61 | 69.6 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 62 | 69.7 | 4.60 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 63 | 70.3 | *3.70 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 65 | 24.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 66 | 33.1 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 67 | 40.6 | 3.20 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 68 | 80.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 69 | 33.1 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 70 | 25.1 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 71 | 25.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 72 | 63.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 73 | 84.7 | 5.90 | C.C | 3.92 | 0.0 | 0.72 | 103 |
| 74 | 99.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 75 | 67.5 | 4.50 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 76 | 66.3 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 77 | 44.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 78 | 32.2 | 3.80 | 3.19 | 0.0 | 0.0 | 0.89 | 103 |
| 80 | 83.2 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 81 | 54.3 | 3.90 | 0.0 | 3.37 | 0.0 | 2.44 | 103 |
| 82 | 25.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 83 | 26.0 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 84 | 25.6 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 85 | 38.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 87 | 75.9 | 4.60 | 0.0 | 3.54 | 0.0 | 0.67 | 103 |
| 88 | 73.6 | 5.10 | 0.0 | 0.0 | 4.40 | 0.0 | 103 |
| 89 | 76.8 | 4.50 | 4.38 | 0.0 | 0.0 | 1.82 | 103 |
| 90 | 70.3 | *4.50 | C.C | 3.66 | 0.0 | 0.50 | 103 |
| 92 | 70.2 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 93 | 34.3 | 4.80 | 3.53 | 0.0 | 0.0 | 0.93 | 103 |
| 94 | 70.2 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 95 | 76.3 | 5.20 | 0.0 | 4.81 | 3.95 | 0.87 | 103 |
| 96 | 99.8 | 4.50 | 0.0 | 3.65 | 0.0 | 0.0 | 103 |
| 97 | 70.3 | *4.10 | 3.37 | 3.11 | 0.0 | 0.78 | 103 |
| 98 | 70.3 | *4.30 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 99 | 70.3 | *4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 100 | 69.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 101 | 70.3 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 102 | 71.0 | *3.70 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 103 | 70.9 | *4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 104 | 70.2 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |

FRK C1/01/72 - 03/20/72

| EVENT NO. | DISTANCE (DEGREES) | MP | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/IP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 105 | 70.4 | *4.10 | 3.72 | 0.0 | 0.0 | 0.0 | 103 |
| 106 | 70.1 | *4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 107 | 76.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 108 | 66.5 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 109 | 63.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 110 | 70.3 | *2.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 111 | 28.8 | 4.80 | 3.50 | 0.0 | 0.0 | 0.0 | 203 |
| 112 | 72.6 | 5.70 | 5.12 | 0.0 | 4.39 | 1.64 | 103 |
| 113 | 70.3 | *4.30 | 0.0 | 0.0 | 0.0 | 2.41 | 103 |
| 114 | 69.3 | 4.80 | 0.0 | 3.56 | 0.0 | 0.0 | 203 |
| 115 | 84.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.84 | 103 |
| 116 | 59.5 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 117 | 84.3 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 118 | 84.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 119 | 84.5 | 4.10 | 0.0 | 3.37 | 0.0 | 0.0 | 203 |
| 120 | 69.4 | 4.90 | 4.30 | 4.04 | 3.73 | 2.11 | 103 |
| 122 | 28.8 | 3.90 | 0.0 | 0.0 | 0.0 | 0.47 | 103 |
| 123 | 25.0 | 4.60 | 0.0 | 3.61 | 0.0 | 0.0 | 203 |
| 124 | 41.1 | 2.80 | 0.0 | 0.0 | 0.0 | 0.63 | 103 |
| 125 | 77.8 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 126 | 24.5 | 3.90 | 3.82 | 0.0 | 0.0 | 0.0 | 303 |
| 127 | 37.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 103 |
| 128 | 78.0 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 129 | 66.8 | 4.80 | 0.0 | 3.37 | 0.0 | 0.0 | 503 |
| 130 | 36.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.30 | 103 |
| 131 | 40.7 | 4.70 | 0.0 | 3.15 | 0.0 | 0.0 | 203 |
| 132 | 26.2 | 4.00 | 0.0 | 0.0 | 0.0 | 1.43 | 103 |
| 133 | 39.5 | 5.20 | 0.0 | 3.50 | 0.0 | 0.0 | 203 |
| 134 | 39.3 | 5.40 | 4.73 | 0.0 | 4.17 | 1.40 | 103 |
| 135 | 79.2 | 3.90 | 0.0 | 0.0 | 0.0 | 1.05 | 103 |
| 136 | 38.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 137 | 67.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 138 | 37.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 139 | 26.8 | 4.80 | 4.02 | 3.80 | 0.0 | 0.0 | 203 |
| 140 | 67.9 | 4.00 | 0.0 | 0.0 | 0.0 | 1.37 | 103 |
| 141 | 74.3 | 5.30 | 0.0 | 3.86 | 4.25 | 0.0 | 203 |
| 142 | 32.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.83 | 303 |
| 143 | 27.9 | 3.40 | 3.21 | 0.0 | 0.0 | 0.0 | 203 |
| 144 | 74.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.99 | 103 |
| 145 | 40.4 | 4.80 | 0.0 | 3.50 | 0.0 | 0.0 | 203 |
| 146 | 39.9 | 4.70 | 3.46 | 0.0 | 0.0 | 2.59 | 103 |
| 147 | 40.2 | 4.90 | 3.52 | 0.0 | 0.0 | 0.92 | 103 |
| 148 | 38.6 | 3.70 | 0.0 | 0.0 | 0.0 | 1.28 | 103 |
| 149 | 24.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 150 | 73.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 151 | 72.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 152 | 25.7 | 3.70 | 0.0 | 3.10 | 0.0 | 1.22 | 103 |
| 153 | 29.3 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 603 |
| 154 | 37.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |

FRK 01/01/72 - 03/20/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|-----------|--------------------|------|---------------|---------------|---------------|----------------|---------|
| 155 | 35.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 156 | 33.2 | 5.00 | 4.33 | 0.0 | 0.0 | 0.95 | 103 |
| 157 | 33.4 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 303 |
| 158 | 28.0 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 303 |
| 159 | 33.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 160 | 33.4 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 203 |
| 161 | 33.1 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 162 | 39.1 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 203 |
| 163 | 65.0 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 203 |
| 164 | 32.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 165 | 32.7 | 4.90 | 4.23 | 0.0 | 0.0 | 1.64 | 103 |
| 166 | 79.6 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 203 |
| 167 | 36.1 | 4.90 | C.0 | 0.0 | 0.0 | 0.0 | 203 |
| 168 | 26.1 | 3.30 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 169 | 37.0 | 3.80 | 3.13 | 0.0 | 0.0 | 0.85 | 103 |
| 170 | 34.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 171 | 73.9 | 4.70 | 3.93 | 0.0 | 0.0 | 1.93 | 103 |
| 172 | 54.7 | 5.30 | 4.82 | 0.0 | 4.36 | 0.63 | 103 |
| 173 | 24.6 | 3.30 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 174 | 26.1 | 3.30 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 175 | 27.9 | 4.90 | 4.26 | 0.0 | 4.37 | 0.66 | 103 |
| 176 | 29.2 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 177 | 25.0 | 3.50 | C.0 | 0.0 | 0.0 | 0.0 | 203 |
| 178 | 30.4 | 4.50 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 179 | 27.9 | 4.40 | 3.24 | 3.14 | 0.0 | 0.0 | 103 |
| 180 | 66.8 | 4.00 | C.0 | 0.0 | 0.0 | 0.0 | 203 |
| 181 | 51.3 | 4.50 | C.0 | 0.0 | 0.0 | 0.0 | 203 |
| 182 | 38.7 | 4.20 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 183 | 73.8 | 4.20 | C.0 | 0.0 | 0.0 | 0.0 | 203 |
| 184 | 25.0 | 4.10 | C.0 | 0.0 | 0.0 | 0.0 | 203 |
| 185 | 27.2 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 186 | 55.0 | 3.90 | 3.14 | 0.0 | 0.0 | 0.97 | 103 |
| 187 | 82.3 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 188 | 82.3 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 189 | 84.5 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 190 | 82.9 | 4.20 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 191 | 47.1 | 4.50 | C.0 | 0.0 | 0.0 | 0.0 | 203 |
| 192 | 83.0 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 193 | 75.1 | 4.40 | C.0 | 0.0 | 0.0 | 0.0 | 203 |
| 194 | 84.2 | 4.70 | C.C | 0.0 | 0.0 | 0.0 | 303 |
| 195 | 86.4 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 303 |
| 196 | 83.8 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 303 |
| 197 | 80.2 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 303 |
| 198 | 81.7 | 3.40 | C.0 | 0.0 | 0.0 | 0.0 | 303 |
| 199 | 81.7 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 200 | 85.7 | 4.40 | C.C | 0.0 | 0.0 | 0.0 | 303 |
| 201 | 82.1 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 202 | 82.7 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 203 |
| 203 | 80.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |

FBK 01/01/72 - 03/20/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=2CSEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 204 | 82.8 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 205 | 24.4 | 3.60 | 3.26 | 0.0 | 0.0 | 7.47 | 103 |
| 206 | 84.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 207 | 83.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 208 | 84.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 209 | 85.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 210 | 81.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 211 | 25.2 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 212 | 24.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 213 | 85.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 214 | 71.0 | 4.00 | 3.76 | 0.0 | 0.0 | 0.0 | 103 |
| 216 | 28.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 217 | 78.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 218 | 26.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 219 | 25.7 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 220 | 28.9 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 221 | 73.3 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 222 | 25.3 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 223 | 41.4 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 224 | 83.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 225 | 66.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 226 | 39.5 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 227 | 28.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 228 | 37.1 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 229 | 28.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 230 | 24.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 231 | 39.5 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 232 | 69.9 | *4.40 | 0.0 | 3.18 | 0.0 | 1.73 | 103 |
| 233 | 32.2 | 4.50 | 0.0 | 3.42 | 0.0 | 0.81 | 103 |
| 234 | 36.5 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 603 |
| 235 | 68.6 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 236 | 65.8 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 237 | 73.8 | 3.60 | 3.14 | 0.0 | 0.0 | 1.14 | 103 |
| 238 | 71.7 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 239 | 73.7 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 240 | 88.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 241 | 27.6 | 3.90 | 2.93 | 2.73 | 0.0 | 0.78 | 103 |
| 242 | 38.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 243 | 35.1 | 5.40 | 0.0 | 4.17 | 0.0 | 1.15 | 103 |
| 245 | 61.6 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 247 | 71.8 | 2.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 248 | 85.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 249 | 83.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 250 | 79.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 251 | 33.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 252 | 32.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 253 | 73.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 254 | 38.3 | 4.20 | 0.0 | 3.18 | 0.0 | 0.68 | 103 |
| 255 | 85.5 | *4.60 | 0.0 | 3.49 | 0.0 | 1.87 | 103 |

FRK 01/01/72 - 03/20/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 256 | 74.1 | 3.50 | 3.43 | 0.0 | 0.0 | 2.92 | 103 |
| 257 | 31.0 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 258 | 36.6 | 3.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 259 | 27.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 260 | 59.9 | 5.50 | 3.54 | 3.41 | 0.0 | 0.0 | 103 |
| 261 | 38.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 262 | 76.3 | 4.90 | 4.30 | 0.0 | 0.0 | 0.31 | 103 |
| 263 | 64.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 264 | 24.9 | 3.80 | 3.25 | 0.0 | 0.0 | 0.0 | 103 |
| 265 | 72.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 266 | 23.4 | 3.60 | 3.31 | 3.42 | 0.0 | 0.68 | 103 |
| 267 | 74.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 268 | 36.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 269 | 28.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 270 | 85.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | ? |
| 271 | 32.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 272 | 73.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 273 | 75.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 274 | 24.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 275 | 73.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 276 | 85.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 277 | 27.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 278 | 75.8 | 5.40 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 279 | 53.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 280 | 71.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 281 | 76.4 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 282 | 76.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 283 | 61.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 284 | 87.3 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 285 | 77.3 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 286 | 32.2 | 4.50 | 3.67 | 3.80 | 0.0 | 1.66 | 103 |
| 287 | 86.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 288 | 71.3 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 289 | 74.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 290 | 70.0 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 291 | 38.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 292 | 32.9 | 5.20 | 4.00 | 3.39 | 0.0 | 1.67 | 103 |
| 293 | 85.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 294 | 70.9 | 5.20 | 4.51 | 0.0 | 4.12 | 0.74 | 103 |
| 295 | 85.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 296 | 77.5 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 297 | 39.8 | 5.00 | 0.0 | 3.92 | 0.0 | 0.90 | 103 |
| 298 | 61.8 | 3.60 | 3.71 | 0.0 | 0.0 | 0.0 | 103 |
| 299 | 24.3 | 3.60 | 3.20 | 2.53 | 0.0 | 0.0 | 103 |
| 300 | 31.5 | 4.70 | 3.48 | 3.28 | 0.0 | 0.29 | 103 |
| 301 | 31.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 302 | 69.9 | 3.20 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 303 | 72.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 503 |
| 304 | 31.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |

FBK 01/01/72 - 03/20/72

| EVENT NO. | DISTANCE (DFGRFES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 305 | 40.7 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 303 |
| 307 | 35.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |
| 308 | 82.4 | 3.40 | 0.0 | 3.90 | 0.0 | 0.92 | 103 |
| 309 | 68.6 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 203 |

APPENDIX II-E
BASIC DATA FOR TLO

TLO C1/C1/72 - C8/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 2 | 87.7 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 3 | 89.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 4 | 90.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 5 | 19.3 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 6 | 63.8 | 5.20 | 4.13 | 3.53 | 3.38 | 1.83 | 104 |
| 7 | 87.4 | 4.80 | 3.64 | 0.0 | 0.0 | 0.58 | 104 |
| 8 | 87.0 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 9 | 74.5 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 10 | 83.7 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 11 | 100.0 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 12 | 84.0 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 13 | 100.1 | *4.60 | 4.10 | 3.72 | 3.69 | 2.56 | 104 |
| 14 | 91.6 | 3.90 | 4.08 | 3.64 | 0.0 | 1.09 | 104 |
| 15 | 63.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 16 | 92.4 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 17 | 16.5 | 4.00 | 3.17 | 2.97 | 0.0 | 1.24 | 104 |
| 18 | 58.1 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 19 | 83.4 | 4.00 | 4.05 | 0.0 | 0.0 | 0.37 | 104 |
| 20 | 82.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 21 | 56.3 | 4.70 | 3.23 | 0.0 | 0.0 | 2.54 | 104 |
| 22 | 100.1 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 23 | 44.9 | 5.20 | 3.42 | 0.0 | 0.0 | 0.0 | 104 |
| 24 | 57.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 25 | 36.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 26 | 98.5 | 4.70 | 6.31 | 0.0 | 0.0 | 2.01 | 304 |
| 27 | 97.7 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 28 | 85.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 29 | 83.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 30 | 91.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 31 | 100.2 | 5.00 | 4.11 | 0.0 | 0.0 | 0.87 | 104 |
| 32 | 83.9 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 33 | 85.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 34 | 93.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 35 | 26.4 | 4.40 | 4.12 | 4.26 | 4.09 | 0.94 | 104 |
| 36 | 22.3 | 4.90 | 0.0 | 3.33 | 0.0 | 0.83 | 104 |
| 37 | 84.0 | 4.80 | 4.46 | 3.78 | 0.0 | 0.49 | 104 |
| 38 | 84.1 | 4.00 | 4.25 | 0.0 | 3.55 | 1.00 | 104 |
| 39 | 75.6 | 5.30 | 4.89 | 0.0 | 4.78 | 0.0 | 104 |
| 40 | 72.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 41 | 41.1 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 42 | 88.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 43 | 72.3 | 4.70 | 0.0 | 3.68 | 0.0 | 1.29 | 104 |
| 44 | 60.9 | 5.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 45 | 62.0 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 46 | 83.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 47 | 83.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 48 | 24.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 49 | 92.1 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 50 | 40.6 | 4.90 | 0.0 | 3.26 | 3.73 | 1.75 | 104 |

TLO C1/C1/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 2 | 87.7 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 3 | 89.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 4 | 90.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 5 | 19.3 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 6 | 63.8 | 5.20 | 4.13 | 3.53 | 3.38 | 1.83 | 104 |
| 7 | 87.4 | 4.80 | 3.64 | 0.0 | 0.0 | 0.58 | 104 |
| 8 | 87.0 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 9 | 74.5 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 10 | 83.7 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 11 | 100.0 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 12 | 84.0 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 13 | 100.1 | *4.60 | 4.10 | 3.72 | 3.69 | 2.56 | 104 |
| 14 | 91.6 | 3.90 | 4.08 | 3.64 | 0.0 | 1.09 | 104 |
| 15 | 63.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 16 | 92.4 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 17 | 16.5 | 4.00 | 3.17 | 2.97 | 0.0 | 1.24 | 104 |
| 18 | 58.1 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 19 | 83.4 | 4.00 | 4.05 | 0.0 | 0.0 | 0.37 | 104 |
| 20 | 82.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 21 | 56.3 | 4.70 | 3.23 | 0.0 | 0.0 | 2.54 | 104 |
| 22 | 100.1 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 23 | 44.9 | 5.20 | 3.42 | 0.0 | 0.0 | 0.0 | 104 |
| 24 | 57.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 25 | 36.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 26 | 98.5 | 4.70 | 6.31 | 0.0 | 0.0 | 2.01 | 304 |
| 27 | 97.7 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 28 | 85.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 29 | 83.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 30 | 91.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 31 | 100.2 | 5.00 | 4.11 | 0.0 | 0.0 | 0.87 | 104 |
| 32 | 83.9 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 33 | 85.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 34 | 93.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 35 | 26.4 | 4.40 | 4.12 | 4.26 | 4.09 | 0.94 | 104 |
| 36 | 22.3 | 4.90 | 0.0 | 3.33 | 0.0 | 0.83 | 104 |
| 37 | 84.0 | 4.80 | 4.46 | 3.78 | 0.0 | 0.49 | 104 |
| 38 | 84.1 | 4.00 | 4.25 | 0.0 | 3.55 | 1.00 | 104 |
| 39 | 75.6 | 5.30 | 4.89 | 0.0 | 4.78 | 0.0 | 104 |
| 40 | 72.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 41 | 41.1 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 42 | 88.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 43 | 72.3 | 4.70 | 0.0 | 3.68 | 0.0 | 1.29 | 104 |
| 44 | 60.9 | 5.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 45 | 62.0 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 46 | 83.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 47 | 83.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 48 | 24.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 49 | 92.1 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 50 | 40.6 | 4.90 | 0.0 | 3.26 | 3.73 | 1.75 | 104 |

TLO C1/C1/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=2CSFC | MS T=3CSEC | MS T=40SFC | LC/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 51 | 10.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 52 | 24.5 | 4.80 | 3.35 | 3.41 | 0.0 | 0.0 | 104 |
| 53 | 36.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 54 | 87.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 55 | 26.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 56 | 86.8 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 57 | 83.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 58 | 87.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 59 | 85.3 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 60 | 13.5 | *4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 61 | 100.0 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 62 | 100.3 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 63 | 13.5 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 65 | 83.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 66 | 89.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 67 | 87.8 | 3.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 68 | 24.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 69 | 89.5 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 70 | 84.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 71 | 83.7 | 3.80 | 0.0 | 3.15 | 0.0 | 1.69 | 104 |
| 72 | 98.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 73 | 58.8 | 5.90 | 0.0 | 3.79 | 0.0 | 0.0 | 104 |
| 74 | 50.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 75 | 62.3 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 76 | 59.0 | 4.40 | 0.0 | 3.19 | 0.0 | 0.0 | 104 |
| 77 | 87.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 78 | 89.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 79 | 62.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 80 | 54.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 81 | 84.6 | 3.90 | 3.71 | 3.27 | 0.0 | 4.31 | 104 |
| 82 | 83.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 83 | 79.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 84 | 83.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 85 | 89.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 86 | 88.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 87 | 19.5 | 4.60 | 3.61 | 3.45 | 0.0 | 1.00 | 104 |
| 88 | 39.4 | 5.10 | 4.42 | 0.0 | 3.72 | 0.87 | 104 |
| 89 | 86.8 | 4.50 | 0.0 | 4.32 | 0.0 | 0.71 | 104 |
| 90 | 13.5 | *4.50 | 3.17 | 0.0 | 0.0 | 6.58 | 104 |
| 92 | 13.4 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 93 | 89.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 94 | 13.4 | 4.40 | 3.79 | 3.00 | 2.90 | 1.27 | 104 |
| 95 | 70.1 | 5.20 | 3.56 | 0.0 | 0.0 | 1.95 | 604 |
| 96 | 54.4 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 97 | 13.5 | *4.10 | 2.82 | 0.0 | 0.0 | 6.38 | 104 |
| 98 | 13.5 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 99 | 13.5 | *4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 100 | 13.7 | 3.60 | 2.78 | 0.0 | 0.0 | 2.86 | 104 |
| 101 | 13.5 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |

TLD 01/01/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 102 | 13.7 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 103 | 13.6 | *4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 104 | 13.5 | *4.30 | 3.76 | 2.85 | 0.0 | 0.50 | 104 |
| 105 | 13.5 | *4.30 | 3.87 | 0.0 | 0.0 | 1.24 | 104 |
| 106 | 13.4 | *4.40 | 3.40 | 0.0 | 0.0 | 2.41 | 104 |
| 107 | 74.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 108 | 62.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 109 | 58.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 110 | 13.4 | *3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 111 | 86.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 112 | 102.4 | 5.70 | 5.14 | 0.0 | 4.43 | 1.28 | 104 |
| 113 | 13.5 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 114 | 100.1 | 4.80 | 0.0 | 3.80 | 0.0 | 0.99 | 104 |
| 115 | 45.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 116 | 56.5 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 117 | 45.5 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 118 | 45.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 119 | 45.6 | 4.10 | 0.0 | 3.62 | 0.0 | 0.51 | 104 |
| 120 | 60.1 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 122 | 86.8 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 123 | 83.4 | 4.60 | 0.0 | 4.09 | 0.0 | 0.93 | 104 |
| 124 | 92.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 125 | 22.0 | 4.50 | 3.44 | 3.23 | 0.0 | 3.12 | 104 |
| 126 | 84.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 278 | 25.6 | 5.40 | 4.71 | 4.39 | 0.0 | 0.52 | 104 |
| 279 | 88.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 280 | 57.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 281 | 70.0 | 5.30 | 0.0 | 3.25 | 0.0 | 0.0 | 104 |
| 282 | 26.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 283 | 77.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 284 | 54.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 285 | 58.9 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 286 | 85.6 | 4.50 | 0.0 | 4.45 | 0.0 | 1.27 | 104 |
| 287 | 52.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 288 | 65.3 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 289 | 79.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 290 | 64.1 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 291 | 94.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 292 | 89.4 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 293 | 49.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 294 | 54.7 | 5.20 | 4.21 | 0.0 | 3.45 | 0.37 | 104 |
| 295 | 48.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 296 | 62.4 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 297 | 88.6 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 298 | 59.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 299 | 82.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 300 | 88.0 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 301 | 83.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 302 | 55.9 | 3.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |

TLD C1/01/72 - CR/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|-----------|--------------------|-------|------------|------------|------------|-------------|---------|
| 303 | 31.5 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 304 | 89.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 305 | 92.2 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 306 | 55.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 307 | 91.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 308 | 53.0 | 3.40 | 3.32 | 0.0 | 0.0 | 2.46 | 104 |
| 309 | 61.8 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 354 | 58.1 | 4.50 | 3.56 | 3.29 | 3.06 | 0.0 | 104 |
| 355 | 93.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 356 | 40.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 357 | 86.1 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 358 | 89.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 359 | 90.5 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 360 | 92.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 361 | 40.5 | 5.40 | 4.42 | 4.35 | 3.68 | 3.67 | 104 |
| 362 | 40.4 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 363 | 86.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 364 | 40.5 | 5.10 | 3.81 | 3.70 | 3.12 | 0.0 | 304 |
| 365 | 84.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 366 | 42.1 | 4.70 | 3.41 | 3.38 | 2.74 | 0.0 | 304 |
| 369 | 45.7 | 3.50 | 0.0 | 2.66 | 2.19 | 0.0 | 104 |
| 370 | 50.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 372 | 13.5 | *4.30 | 3.01 | 2.57 | 0.0 | 0.0 | 104 |
| 373 | 20.3 | 4.90 | 3.66 | 3.67 | 0.0 | 0.0 | 104 |
| 374 | 85.9 | 3.50 | 3.50 | 3.49 | 2.03 | 0.0 | 104 |
| 375 | 24.8 | 3.30 | 2.93 | 2.98 | 2.52 | 0.0 | 104 |
| 376 | 83.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 377 | 56.2 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 378 | 85.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 379 | 39.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 380 | 15.7 | *4.20 | 2.78 | 0.0 | 0.0 | 0.0 | 104 |
| 381 | 92.5 | 4.60 | 0.0 | 3.54 | 0.0 | 0.0 | 304 |
| 382 | 67.5 | 4.30 | 3.44 | 3.36 | 2.68 | 0.0 | 104 |
| 383 | 90.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 384 | 57.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 385 | 26.9 | 4.40 | 2.60 | 2.54 | 0.0 | 0.0 | 104 |
| 386 | 85.5 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 387 | 93.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 388 | 93.5 | 4.50 | 3.54 | 3.13 | 2.90 | 3.34 | 104 |
| 389 | 90.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 403 | 59.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 404 | 48.7 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 405 | 16.0 | *4.50 | 3.28 | 2.63 | 2.38 | 5.49 | 104 |
| 408 | 58.2 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 409 | 15.3 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 410 | 56.4 | 4.70 | 3.60 | 3.49 | 3.21 | 0.0 | 104 |
| 411 | 85.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 412 | 100.0 | 5.00 | 4.00 | 3.80 | 3.16 | 0.0 | 104 |
| 413 | 52.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |

TLO 01/01/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|-----------|--------------------|-------|---------------|---------------|---------------|----------------|---------|
| 414 | 56.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | |
| 415 | 52.3 | 4.00 | 3.03 | 3.08 | 2.68 | 0.0 | 204 |
| 416 | 60.1 | 5.50 | 3.66 | 3.40 | 3.32 | 0.0 | 304 |
| 417 | 85.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 418 | 81.0 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 419 | 60.1 | *5.20 | 3.27 | 3.18 | 2.73 | 0.0 | 204 |
| 420 | 36.7 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 104 |
| 424 | 83.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 425 | 84.6 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 426 | 28.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 428 | 86.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 429 | 47.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 430 | 49.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 431 | 56.4 | *4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 432 | 51.3 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 433 | 98.0 | 4.90 | 4.38 | 4.00 | 3.42 | 1.03 | 304 |
| 435 | 85.7 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 104 |
| 436 | 45.2 | 5.40 | 4.83 | 4.42 | 4.06 | 1.22 | 204 |
| 437 | 45.3 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 104 |
| 438 | 45.2 | 5.00 | 3.67 | 3.33 | 3.00 | 0.0 | 304 |
| 439 | 57.5 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 104 |
| 440 | 47.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 441 | 42.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 442 | 45.4 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 443 | 89.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 444 | 28.0 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 445 | 48.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 446 | 84.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 447 | 88.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 448 | 48.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 449 | 60.2 | 4.60 | 3.94 | 3.60 | 2.91 | 0.64 | 204 |
| 450 | 63.6 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 104 |
| 451 | 65.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 452 | 43.3 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 453 | 45.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 454 | 20.2 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 455 | 47.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 456 | 56.1 | 4.40 | 3.17 | 2.99 | 0.0 | 0.0 | 304 |
| 457 | 50.0 | 3.10 | 0.0 | 0.0 | 0.0 | 0.0 | 104 |
| 458 | 59.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 459 | 91.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 460 | 83.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 461 | 85.8 | 5.00 | 4.67 | 4.45 | 3.81 | 0.0 | 304 |
| 462 | 80.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 104 |
| 463 | 20.9 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 464 | 91.9 | 4.90 | 4.07 | 0.0 | 0.0 | 0.0 | 204 |
| 465 | 89.4 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 104 |
| 466 | 18.5 | 4.00 | 0.0 | 2.55 | 0.0 | 0.0 | 204 |
| 467 | 100.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 104 |
| | | | | | | | 204 |

TLD 01/01/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 468 | 97.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 469 | 85.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 470 | 65.5 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 471 | 57.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 472 | 89.7 | 5.20 | 3.96 | 3.89 | 3.33 | 1.53 | 104 |
| 473 | 84.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 474 | 51.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 475 | 38.9 | 4.70 | 3.91 | 3.23 | 2.67 | 3.00 | 104 |
| 476 | 89.0 | 5.20 | 4.12 | 3.78 | 3.20 | 0.0 | 104 |
| 477 | 60.4 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 478 | 84.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 479 | 20.4 | 4.10 | 3.29 | 2.59 | 0.0 | 0.0 | 104 |
| 480 | 89.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 481 | 72.8 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 482 | 92.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 483 | 55.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 484 | 13.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 485 | 100.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 486 | 27.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 487 | 45.2 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 488 | 45.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 489 | 45.4 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 490 | 99.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 491 | 59.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 492 | 100.3 | 5.10 | 4.09 | 3.77 | 3.19 | 1.37 | 104 |
| 493 | 90.5 | 4.40 | 3.12 | 3.03 | 2.79 | 0.0 | 104 |
| 494 | 85.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 495 | 90.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 496 | 76.5 | 5.20 | 4.75 | 4.21 | 3.80 | 0.0 | 104 |
| 497 | 36.3 | 4.90 | 4.43 | 4.31 | 3.97 | 2.05 | 104 |
| 498 | 76.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 499 | 98.6 | 4.60 | 3.57 | 3.43 | 2.75 | 0.93 | 104 |
| 500 | 92.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 501 | 85.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 502 | 83.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 503 | 87.8 | 4.20 | 0.0 | 3.13 | 0.0 | 0.0 | 104 |
| 504 | 27.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 505 | 84.1 | 5.30 | 0.0 | 3.74 | 3.16 | 2.26 | 104 |
| 506 | 82.4 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 508 | 93.6 | 4.10 | 3.87 | 3.67 | 2.73 | 0.0 | 104 |
| 509 | 84.0 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 510 | 60.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 511 | 48.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 513 | 91.5 | 5.00 | 4.07 | 3.82 | 3.15 | 0.0 | 104 |
| 514 | 87.3 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 515 | 82.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 516 | 55.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 517 | 76.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 518 | 45.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|-----------|--------------------|------|---------------|---------------|---------------|----------------|---------|
| 521 | 30.3 | 4.60 | 0.0 | 3.39 | 2.98 | 0.0 | 104 |
| 522 | 74.3 | 5.50 | 5.11 | 4.86 | 3.87 | 0.0 | 104 |
| 523 | 72.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 524 | 23.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 525 | 74.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 526 | 81.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 527 | 33.6 | 4.40 | 2.99 | 3.09 | 0.0 | 0.0 | 104 |
| 528 | 81.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 529 | 64.3 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 530 | 19.6 | 4.50 | 3.55 | 3.24 | 0.0 | 0.0 | 104 |
| 537 | 25.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 538 | 57.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 539 | 89.2 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 540 | 21.6 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 541 | 89.2 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 542 | 54.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 543 | 100.5 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 544 | 81.5 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 545 | 23.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 546 | 83.3 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 547 | 98.7 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 548 | 45.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 549 | 98.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 550 | 105.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 234 |
| 551 | 29.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 552 | 57.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 553 | 58.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 554 | 31.1 | 4.50 | 0.0 | 3.05 | 3.06 | 1.25 | 104 |
| 555 | 22.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 104 |
| 556 | 92.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 557 | 50.9 | 4.70 | 0.0 | 3.84 | 0.0 | 0.0 | 134 |
| 558 | 83.4 | 5.60 | 5.11 | 4.63 | 4.12 | 0.0 | 104 |
| 559 | 83.4 | 5.00 | 5.41 | 4.88 | 0.0 | 0.0 | 134 |
| 560 | 51.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 234 |
| 561 | 28.3 | 4.30 | 3.41 | 3.04 | 0.0 | 2.32 | 104 |
| 562 | 90.8 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 563 | 83.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 564 | 27.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 565 | 80.1 | 5.30 | 4.22 | 3.84 | 3.84 | 0.0 | 104 |
| 566 | 28.5 | 4.50 | 4.13 | 3.59 | 0.0 | 0.0 | 104 |
| 567 | 101.2 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 568 | 101.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 569 | 90.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 570 | 28.6 | 4.30 | 0.0 | 3.06 | 2.67 | 0.0 | 104 |
| 571 | 51.0 | 4.00 | 3.01 | 2.63 | 0.0 | 0.0 | 104 |
| 572 | 90.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 573 | 89.2 | 5.70 | 6.24 | 5.44 | 5.42 | 0.73 | 104 |
| 574 | 89.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 575 | 89.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |

110 01/01/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 576 | 47.8 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 577 | 89.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 578 | 89.5 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 579 | 89.4 | 4.90 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 580 | 89.4 | 4.30 | C.0 | 0.0 | 0.0 | 0.0 | 304 |
| 581 | 33.4 | 2.80 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 582 | 22.3 | 4.50 | 3.17 | 2.89 | 2.70 | 0.0 | 104 |
| 583 | 55.7 | 5.50 | 0.0 | 4.19 | 4.18 | 0.90 | 104 |
| 584 | 55.2 | 5.00 | C.0 | 0.0 | 0.0 | 0.0 | 204 |
| 585 | 26.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 234 |
| 586 | 43.9 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 587 | 24.6 | 4.00 | C.0 | 0.0 | 0.0 | 0.0 | 204 |
| 588 | 89.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 234 |
| 589 | 89.5 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 590 | 84.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 591 | 84.5 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 592 | 27.9 | 4.00 | 2.97 | 2.50 | 0.0 | 0.0 | 104 |
| 593 | 86.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 594 | 44.0 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 595 | 56.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 596 | 90.5 | 5.10 | 0.0 | 3.77 | 3.23 | 0.0 | 104 |
| 597 | 83.9 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 598 | 55.7 | 5.50 | 0.0 | 4.04 | 3.58 | 1.00 | 104 |
| 599 | 83.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 600 | 19.0 | 4.30 | C.C | 0.0 | 2.63 | 0.0 | 134 |
| 601 | 28.4 | 4.40 | 3.07 | 0.0 | 2.38 | 0.0 | 104 |
| 602 | 88.8 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 603 | 77.2 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 204 |
| 604 | 55.9 | 4.50 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 605 | 70.0 | 5.10 | 4.26 | 3.60 | 3.11 | 0.85 | 104 |
| 606 | 75.0 | 4.80 | 4.48 | 0.0 | 3.44 | 0.0 | 104 |
| 607 | 90.8 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 608 | 108.5 | 4.50 | 4.31 | 4.16 | 3.99 | 0.0 | 104 |
| 609 | 84.8 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 610 | 75.0 | 5.20 | 4.07 | 4.02 | 0.0 | 0.0 | 104 |
| 611 | 72.5 | 5.00 | 4.37 | 3.90 | 3.64 | 0.66 | 104 |
| 612 | 13.7 | 4.00 | 3.01 | 2.55 | 0.0 | 0.0 | 104 |
| 613 | 83.6 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 614 | 84.7 | 5.30 | 4.18 | 4.25 | 3.57 | 2.86 | 104 |
| 615 | 45.7 | 2.50 | C.C | 0.0 | 0.0 | 0.0 | 234 |
| 616 | 56.1 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 617 | 20.3 | *4.40 | 0.0 | 3.10 | 0.0 | 0.0 | 154 |
| 618 | 74.3 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 619 | 57.4 | 4.70 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 620 | 89.6 | 2.60 | C.0 | 0.0 | 0.0 | 0.0 | 324 |
| 621 | 89.0 | 2.60 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 622 | 90.5 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 623 | 85.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 624 | 90.3 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 304 |

APPENDIX II-F
BASIC DATA FOR EIL

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 262 | 32.6 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 263 | 27.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 264 | 85.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 265 | 30.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 266 | 63.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 267 | 35.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 268 | 88.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 269 | 80.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 270 | 19.0 | 4.10 | 1.83 | 1.61 | 0.0 | 0.0 | 155 |
| 271 | 86.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 272 | 30.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 273 | 12.4 | 3.80 | 1.32 | 1.13 | 0.0 | 0.0 | 155 |
| 274 | 85.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 275 | 41.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 276 | 55.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 277 | 67.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 278 | 10.8 | 5.40 | 1.63 | 1.63 | 0.0 | 0.0 | 155 |
| 279 | 73.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 280 | 32.4 | 3.70 | 0.0 | 2.35 | 0.0 | 0.0 | 155 |
| 281 | 43.0 | 5.30 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 282 | 10.4 | 3.70 | 1.61 | 1.64 | 0.0 | 0.0 | 155 |
| 283 | 57.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 284 | 19.1 | 3.60 | 2.61 | 2.80 | 0.0 | 0.0 | 155 |
| 285 | 31.3 | 3.50 | 2.29 | 2.01 | 0.0 | 0.0 | 155 |
| 286 | 82.0 | 4.50 | 3.07 | 2.64 | 0.0 | 0.0 | 155 |
| 287 | 20.7 | 3.80 | 1.95 | 2.02 | 0.0 | 0.0 | 155 |
| 288 | 40.5 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 289 | 53.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 290 | 40.0 | 3.50 | 3.74 | 3.55 | 0.0 | 0.0 | 155 |
| 291 | 112.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 294 | 30.6 | 5.20 | 3.36 | 3.21 | 0.0 | 0.0 | 155 |
| 295 | 17.1 | 3.90 | 2.19 | 1.54 | 0.0 | 0.0 | 155 |
| 296 | 34.7 | 3.50 | 2.23 | 2.27 | 0.0 | 0.0 | 155 |
| 297 | 80.7 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 298 | 39.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 299 | 83.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 300 | 85.7 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 301 | 79.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 302 | 32.5 | 3.20 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 310 | 85.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 311 | 34.6 | 3.60 | 3.65 | 0.0 | 0.0 | 0.0 | 105 |
| 312 | 55.2 | 3.70 | 3.62 | 0.0 | 3.28 | 0.0 | 105 |
| 313 | 13.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 314 | 85.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 315 | 16.0 | 4.10 | 3.03 | 2.70 | 0.0 | 0.0 | 105 |
| 316 | 83.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 317 | 40.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 318 | 40.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 319 | 39.4 | 3.50 | 0.0 | 3.64 | 3.29 | 0.0 | 105 |

FIL 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 320 | 39.3 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 321 | 48.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 322 | 53.1 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 323 | 79.5 | *5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 324 | 16.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 325 | 16.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 326 | 84.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 327 | 88.6 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 328 | 86.3 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 330 | 52.8 | 3.50 | 3.83 | 3.21 | 0.0 | 0.0 | 105 |
| 331 | 84.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 332 | 13.8 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 333 | 10.8 | 3.50 | 0.0 | 2.60 | 0.0 | 0.0 | 105 |
| 334 | 31.0 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 335 | 57.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 336 | 84.8 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 337 | 85.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 338 | 84.5 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 339 | 38.6 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 340 | 85.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 341 | 76.2 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 343 | 76.3 | 4.90 | 4.26 | 4.00 | 3.91 | 0.0 | 105 |
| 344 | 14.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 345 | 54.7 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 346 | 76.4 | 4.70 | 3.24 | 3.16 | 0.0 | 0.0 | 105 |
| 347 | 17.2 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 348 | 49.8 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 349 | 85.7 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 350 | 8.7 | 4.90 | 2.66 | 0.0 | 1.75 | 0.0 | 105 |
| 351 | 129.6 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 352 | 11.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 353 | 14.3 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 354 | 28.0 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 355 | 86.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 356 | 10.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 361 | 10.7 | 5.40 | 5.03 | 4.47 | 4.30 | 0.0 | 105 |
| 362 | 10.7 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 363 | 85.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 365 | 84.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 428 | 85.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 432 | 19.7 | 4.40 | 3.94 | 3.28 | 2.71 | 0.0 | 105 |
| 433 | 75.6 | 4.90 | 3.87 | 3.87 | 3.10 | 0.0 | 105 |
| 435 | 86.7 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 437 | 14.1 | 4.60 | 3.62 | 3.19 | 2.77 | 0.0 | 105 |
| 438 | 14.1 | 5.00 | 3.74 | 3.37 | 3.02 | 0.0 | 105 |
| 439 | 31.3 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 441 | 11.9 | 4.00 | 3.48 | 2.72 | 2.49 | 0.0 | 105 |
| 442 | 14.3 | 5.10 | 3.86 | 3.71 | 3.36 | 0.0 | 105 |
| 443 | 85.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |

FILE 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 444 | 11.7 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 445 | 17.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 446 | 84.8 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 447 | 83.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 449 | 39.6 | 4.60 | 3.57 | 3.13 | 0.0 | 0.0 | 105 |
| 450 | 43.0 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 451 | 44.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 452 | 13.7 | 3.40 | 3.67 | 2.97 | 0.0 | 0.0 | 105 |
| 453 | 15.2 | 4.00 | 3.27 | 2.91 | 0.0 | 0.0 | 105 |
| 454 | 13.3 | 4.70 | 3.10 | 2.54 | 2.02 | 0.0 | 105 |
| 455 | 16.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 456 | 38.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 457 | 18.2 | 3.10 | 2.70 | 2.52 | 0.0 | 0.0 | 105 |
| 458 | 49.3 | 4.30 | 3.67 | 3.37 | 0.0 | 0.0 | 105 |
| 459 | 83.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 460 | 84.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 461 | 57.6 | 5.00 | 4.59 | 4.56 | 3.83 | 0.0 | 105 |
| 462 | 57.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 463 | 15.1 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 464 | 87.1 | 4.50 | 3.96 | 3.58 | 0.0 | 0.0 | 105 |
| 465 | 84.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 466 | 14.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 467 | 81.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 469 | 25.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 470 | 44.9 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 471 | 32.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 472 | 85.6 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 473 | 84.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 474 | 22.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 475 | 11.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 476 | 85.4 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 477 | 32.9 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 478 | 26.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 479 | 13.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 481 | 46.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 482 | 85.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 483 | 24.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 484 | 22.2 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 485 | 78.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 486 | 7.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 487 | 14.1 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 488 | 14.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 489 | 14.2 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 490 | 81.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 491 | 37.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 492 | 78.9 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 499 | 76.0 | 4.60 | 3.74 | 3.28 | 2.80 | 0.0 | 505 |
| 500 | 85.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 105 |
| 501 | 85.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |

EIL 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LP RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 502 | 57.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 503 | 85.5 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 504 | 6.1 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 505 | 83.5 | 5.30 | 4.70 | 4.10 | 3.93 | 0.0 | 105 |
| 506 | 83.0 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 508 | 86.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 509 | 83.2 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 510 | 36.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 511 | 31.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 512 | 21.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 513 | 84.2 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 514 | 86.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 515 | 81.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 516 | 30.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 517 | 49.1 | 3.90 | 3.83 | 3.40 | 0.0 | 0.0 | 105 |
| 518 | 18.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 521 | 15.7 | 4.60 | 3.42 | 3.06 | 0.0 | 0.0 | 105 |
| 522 | 48.6 | 5.50 | 4.79 | 4.50 | 3.87 | 0.0 | 105 |
| 523 | 48.5 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 524 | 9.7 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 525 | 48.3 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 526 | 81.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 527 | 11.1 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 528 | 82.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 529 | 39.0 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 530 | 14.3 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 531 | 85.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 532 | 14.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 533 | 22.1 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 534 | 86.7 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 535 | 82.6 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 536 | 39.3 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 542 | 31.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 543 | 77.1 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 544 | 56.9 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 545 | 13.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 546 | 83.9 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 547 | 76.2 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 548 | 15.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 549 | 80.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 551 | 4.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 225 |
| 553 | 32.0 | 3.80 | 0.0 | 2.71 | 0.0 | 3.98 | 105 |
| 554 | 5.7 | 4.50 | 3.66 | 3.56 | 2.97 | 0.0 | 105 |
| 555 | 10.6 | 3.40 | 3.44 | 3.10 | 0.0 | 0.0 | 105 |
| 556 | 84.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 557 | 19.7 | 4.70 | 0.0 | 4.00 | 0.0 | 0.0 | 105 |
| 558 | 84.1 | 5.60 | 4.64 | 0.0 | 4.74 | 0.0 | 105 |
| 559 | 84.1 | 5.00 | 5.37 | 4.57 | 0.0 | 0.0 | 105 |
| 560 | 19.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |

FIL 06/C1/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 561 | 8.6 | 4.30 | 3.57 | 0.0 | 0.0 | 0.0 | 105 |
| 562 | 85.6 | 4.50 | 0.0 | 3.69 | 0.0 | 0.0 | 105 |
| 563 | 83.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 564 | 10.9 | 3.90 | 3.51 | 0.0 | 0.0 | 0.0 | 105 |
| 565 | 81.6 | 5.30 | 4.99 | 4.74 | 4.05 | 0.17 | 105 |
| 566 | 8.5 | 4.50 | 3.32 | 0.0 | 0.0 | 0.0 | 105 |
| 567 | 19.7 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 568 | 83.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 569 | 84.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 570 | 8.7 | 4.30 | 0.0 | 3.80 | 3.06 | 0.0 | 105 |
| 571 | 19.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 572 | 86.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 573 | 85.8 | 5.70 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 574 | 86.0 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 575 | 86.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 576 | 16.2 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 577 | 86.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 578 | 86.1 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 579 | 86.0 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 580 | 85.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 581 | 89.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 582 | 15.4 | 4.50 | 0.0 | 3.56 | 3.15 | 0.0 | 105 |
| 583 | 24.0 | 5.50 | 3.89 | 3.73 | 3.13 | 0.0 | 105 |
| 584 | 23.6 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 585 | 6.6 | 4.00 | 0.0 | 2.91 | 0.0 | 0.0 | 105 |
| 586 | 13.6 | 5.00 | 3.81 | 3.31 | 3.04 | 1.29 | 105 |
| 587 | 9.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 588 | 86.4 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 589 | 86.1 | 4.20 | 4.70 | 3.97 | 0.0 | 0.0 | 135 |
| 590 | 85.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 591 | 85.8 | 4.50 | 3.99 | 3.82 | 3.66 | 0.0 | 105 |
| 592 | 8.9 | 4.00 | 0.0 | 2.40 | 2.72 | 0.0 | 105 |
| 593 | 88.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 594 | 16.7 | 4.70 | 3.88 | 3.72 | 0.0 | 0.49 | 105 |
| 595 | 25.4 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 596 | 87.1 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 597 | 82.8 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 598 | 24.0 | 5.50 | 0.0 | 3.54 | 3.26 | 2.03 | 105 |
| 599 | 85.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 600 | 15.3 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 601 | 9.8 | 4.40 | 4.15 | 0.0 | 3.15 | 0.0 | 105 |
| 602 | 84.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 603 | 64.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 604 | 32.5 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 235 |
| 605 | 57.0 | 5.10 | 4.27 | 4.14 | 0.0 | 0.22 | 105 |
| 606 | 67.2 | 4.80 | 5.15 | 0.0 | 4.47 | 0.18 | 105 |
| 607 | 85.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 608 | 54.6 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 609 | 86.0 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |

FIL 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 610 | 50.1 | 5.20 | 4.03 | 3.88 | 3.51 | 1.10 | 105 |
| 611 | 54.4 | 5.00 | 4.24 | 4.20 | 3.84 | 0.46 | 105 |
| 612 | 20.4 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 613 | 84.5 | 3.30 | C.0 | 0.0 | 0.0 | 0.0 | 205 |
| 614 | 84.6 | 5.30 | 4.27 | 3.79 | 0.0 | 0.0 | 135 |
| 615 | 15.2 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 616 | 29.6 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 617 | 15.2 | *4.40 | C.0 | 3.85 | 0.0 | 0.0 | 105 |
| 618 | 49.5 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 619 | 31.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 620 | 86.4 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 621 | 84.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 622 | 85.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 623 | 84.3 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 624 | 84.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 625 | 85.2 | 3.40 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 626 | 38.6 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 235 |
| 627 | 13.9 | 3.50 | 3.47 | 2.79 | 0.0 | 0.0 | 105 |
| 628 | 85.2 | 3.60 | C.0 | 0.0 | 0.0 | 0.0 | 205 |
| 629 | 31.3 | 3.60 | 3.15 | 2.59 | 0.0 | 0.0 | 105 |
| 630 | 85.8 | 4.30 | 0.0 | 3.86 | 3.78 | 0.0 | 105 |
| 631 | 84.9 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 632 | 84.8 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 633 | 84.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 634 | 37.5 | 5.00 | C.C | 0.0 | 0.0 | 0.0 | 305 |
| 635 | 85.4 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 636 | 85.3 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 637 | 85.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 638 | 84.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 639 | 14.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 640 | 26.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 105 |
| 641 | 26.5 | 3.90 | 3.55 | 3.27 | 0.0 | 0.0 | 105 |
| 642 | 52.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 643 | 84.8 | 4.00 | 0.0 | 3.76 | 0.0 | 0.0 | 105 |
| 644 | 85.0 | 5.10 | C.C | 0.0 | 4.16 | 0.0 | 155 |
| 645 | 83.8 | 5.10 | C.0 | 0.0 | 0.0 | 0.0 | 205 |
| 646 | 83.8 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 647 | 53.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 648 | 12.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 649 | 84.6 | 4.30 | 0.0 | 3.95 | 0.0 | 1.03 | 105 |
| 650 | 84.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 235 |
| 651 | 85.3 | 4.90 | C.C | 0.0 | 0.0 | 0.0 | 305 |
| 652 | 22.7 | 5.70 | 0.0 | 0.0 | 3.55 | 0.0 | 175 |
| 653 | 86.9 | 5.20 | 4.28 | 4.53 | 4.35 | 0.0 | 105 |
| 654 | 83.6 | 4.50 | C.0 | 0.0 | 0.0 | 0.0 | 305 |
| 655 | 84.6 | 4.00 | 0.0 | 4.07 | 3.88 | 0.0 | 175 |
| 656 | 61.0 | 4.80 | 0.0 | 3.22 | 0.0 | 4.46 | 105 |
| 657 | 53.5 | 4.30 | C.0 | 0.0 | 0.0 | 0.0 | 205 |
| 658 | 46.7 | *4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 659 | 9.9 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 660 | 85.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 661 | 85.5 | 5.20 | 4.30 | 4.43 | 3.91 | 0.0 | 105 |
| 662 | 37.7 | 4.60 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 663 | 76.1 | 4.20 | C.C | 0.0 | 0.0 | 0.0 | 305 |
| 664 | 85.9 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 305 |
| 665 | 10.7 | 4.00 | 0.0 | 2.68 | 0.0 | 0.0 | 105 |
| 666 | 85.1 | 3.30 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 667 | 86.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 668 | 85.0 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 669 | 81.9 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 235 |
| 670 | 66.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 671 | 85.2 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 672 | 38.4 | 5.50 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 673 | 56.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 674 | 9.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 675 | 60.1 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 305 |
| 676 | 59.1 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 305 |
| 677 | 30.4 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 678 | 84.1 | 4.20 | 4.17 | 0.0 | 0.0 | 0.0 | 165 |
| 679 | 45.3 | 6.30 | 4.48 | 4.15 | 3.77 | 0.0 | 105 |
| 680 | 25.6 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 681 | 85.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 682 | 12.1 | 3.70 | C.C | 2.75 | 0.0 | 0.0 | 105 |
| 683 | 7.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 684 | 9.8 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 685 | 40.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 686 | 20.7 | *4.30 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 687 | 51.6 | 5.50 | 4.87 | 4.26 | 3.98 | 0.78 | 135 |
| 688 | 49.1 | 4.20 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 689 | 51.5 | 5.50 | 4.37 | 3.70 | 3.78 | 0.0 | 135 |
| 690 | 51.4 | 5.50 | 4.49 | 3.93 | 0.0 | 0.0 | 165 |
| 691 | 85.0 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 691 | 51.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 692 | 49.7 | 5.50 | 4.70 | 4.48 | 3.85 | 0.51 | 105 |
| 693 | 56.5 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 694 | 84.8 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 844 | 8.5 | 4.60 | 0.0 | 4.24 | 0.0 | 0.0 | 105 |
| 845 | 28.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 846 | 86.7 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 505 |
| 847 | 32.2 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 848 | 85.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 849 | 20.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 850 | 84.5 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 851 | 85.2 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 852 | 85.9 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 853 | 52.9 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 205 |
| 854 | 42.5 | 3.80 | C.C | C.C | 0.0 | 0.0 | 205 |
| 855 | 32.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |

FIL 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGRFES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 856 | 12.7 | 3.70 | 2.98 | 0.0 | 2.27 | 0.0 | 105 |
| 857 | 86.2 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 858 | 84.9 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 859 | 84.8 | 5.70 | 5.12 | 4.78 | 4.61 | 0.71 | 105 |
| 860 | 85.9 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 861 | 29.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 862 | 15.9 | 4.60 | 2.94 | 2.35 | 0.0 | 0.0 | 105 |
| 863 | 12.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 864 | 85.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 865 | 38.6 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 866 | 16.1 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 867 | 86.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 868 | 84.1 | 4.30 | 3.53 | 3.99 | 3.59 | 0.55 | 135 |
| 869 | 88.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 205 |
| 870 | 43.5 | 4.10 | 0.0 | 3.10 | 0.0 | 0.0 | 105 |
| 871 | 85.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 872 | 11.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 505 |
| 873 | 45.0 | 4.50 | 3.52 | 0.0 | 0.0 | 0.0 | 105 |
| 874 | 13.2 | 4.40 | 3.27 | 2.72 | 3.06 | 0.0 | 105 |
| P75 | 45.1 | 4.90 | 4.26 | 3.53 | 0.0 | 0.42 | 105 |

TLO 01/01/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LO/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 625 | 84.6 | 3.40 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 626 | 56.1 | 5.20 | 3.35 | 2.93 | 0.0 | 0.0 | 104 |
| 627 | 41.4 | 3.50 | 2.90 | 2.70 | 0.0 | 0.0 | 104 |
| 628 | 84.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 629 | 56.6 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 630 | 84.7 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 631 | 89.0 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 632 | 91.7 | 4.50 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 633 | 83.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 634 | 65.6 | 5.00 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 635 | 92.1 | 4.50 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 636 | 92.0 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 637 | 86.1 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 638 | 86.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 639 | 19.9 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 640 | 57.9 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 641 | 57.9 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 642 | 69.4 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 643 | 84.5 | 4.00 | 3.30 | 3.25 | 0.0 | 0.70 | 104 |
| 644 | 86.1 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 645 | 87.9 | 5.10 | 0.0 | 3.30 | 3.15 | 0.0 | 104 |
| 646 | 87.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 647 | 81.9 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 648 | 21.0 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 649 | 92.9 | 4.30 | 3.50 | 3.34 | 0.0 | 0.0 | 104 |
| 650 | 91.7 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 651 | 93.0 | 4.90 | 4.33 | 3.57 | 3.31 | 0.0 | 104 |
| 652 | 37.6 | 5.70 | 2.81 | 2.58 | 0.0 | 0.0 | 104 |
| 653 | 88.0 | 5.20 | 3.90 | 3.59 | 0.0 | 3.14 | 104 |
| 654 | 83.6 | 4.50 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 655 | 90.3 | 4.00 | C.C | 3.08 | 0.0 | 0.0 | 134 |
| 656 | 46.7 | 4.80 | 3.20 | 3.10 | 0.0 | 0.0 | 104 |
| 657 | 81.9 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 658 | 74.4 | *4.50 | C.C | 0.0 | 0.0 | 0.0 | 304 |
| 659 | 23.4 | 4.00 | 2.55 | 2.47 | 0.0 | 0.0 | 104 |
| 660 | 90.8 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 661 | 88.4 | 5.20 | 4.50 | 4.00 | 3.85 | 0.0 | 104 |
| 662 | 61.6 | 4.60 | C.C | 0.0 | 0.0 | 0.0 | 324 |
| 663 | 98.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 664 | 89.4 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 665 | 25.4 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 666 | 87.6 | 3.30 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 667 | 88.9 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 324 |
| 668 | 86.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 669 | 88.5 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 234 |
| 670 | 65.9 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 671 | 90.5 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 672 | 55.9 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 673 | 80.2 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 204 |

TLN 01/01/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 674 | 26.4 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 204 |
| 675 | 86.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 676 | 86.2 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 677 | 56.8 | 3.60 | 0.0 | 3.16 | 0.0 | 0.0 | 164 |
| 678 | 83.5 | 4.20 | 0.0 | 0.0 | 3.12 | 0.0 | 164 |
| 679 | 43.4 | 6.30 | 5.22 | 4.23 | 3.61 | 0.0 | 104 |
| 680 | 52.5 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 304 |
| 681 | 89.2 | 3.70 | 0.0 | 2.91 | 0.0 | 4.86 | 104 |
| 682 | 41.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 683 | 25.7 | 4.40 | 3.18 | 2.81 | 2.50 | 0.0 | 104 |
| 684 | 23.9 | 3.60 | 3.64 | 3.43 | 2.72 | 0.0 | 104 |
| 685 | 66.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 686 | 15.6 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 687 | 74.3 | 5.50 | 4.59 | 4.28 | 3.65 | 0.0 | 104 |
| 688 | 70.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 689 | 74.3 | 5.50 | 4.54 | 4.16 | 3.55 | 0.0 | 104 |
| 690 | 74.2 | 5.50 | 4.39 | 4.23 | 3.79 | 0.0 | 104 |
| 691 | 86.1 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 504 |
| 691 | 73.2 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 692 | 64.5 | 5.50 | 4.50 | 4.08 | 3.62 | 0.0 | 104 |
| 693 | 71.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |
| 694 | 84.5 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 204 |

APPENDIX II-G
BASIC DATA FOR KON

KON 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 1 | 57.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 2 | 66.3 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 3 | 67.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 24 | 45.1 | 3.90 | 0.0 | 4.24 | 0.0 | 0.0 | 106 |
| 25 | 26.4 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 26 | 80.3 | 4.70 | 6.27 | 5.60 | 0.0 | 0.0 | 306 |
| 27 | 79.5 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 28 | 64.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 29 | 62.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 30 | 69.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 31 | 81.9 | 5.00 | 4.77 | 4.77 | 4.39 | 1.26 | 106 |
| 32 | 62.8 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 33 | 64.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 34 | 71.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 35 | 25.5 | 4.40 | 4.26 | 4.05 | 4.07 | 0.62 | 106 |
| 36 | 26.3 | 4.90 | 3.52 | 3.73 | 3.41 | 0.48 | 106 |
| 37 | 62.9 | 4.80 | 4.27 | 0.0 | 3.62 | 1.23 | 106 |
| 38 | 63.0 | 4.00 | 4.24 | 0.0 | 3.64 | 1.09 | 106 |
| 39 | 54.1 | 5.30 | 5.40 | 0.0 | 4.68 | 0.34 | 106 |
| 40 | 52.2 | 3.90 | 3.75 | 3.12 | 0.0 | 0.72 | 106 |
| 41 | 36.3 | 5.10 | 0.0 | 3.57 | 0.0 | 0.85 | 106 |
| 42 | 67.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 43 | 51.0 | 4.70 | 0.0 | 3.37 | 0.0 | 2.07 | 106 |
| 44 | 46.1 | 5.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 45 | 47.3 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 46 | 62.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 47 | 62.8 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 48 | 27.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 49 | 70.6 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 50 | 33.2 | 4.90 | 4.11 | 3.61 | 0.0 | 0.47 | 106 |
| 51 | 15.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 53 | 27.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 54 | 66.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 55 | 25.6 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 56 | 65.5 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 57 | 62.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 58 | 65.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 59 | 64.1 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 60 | 16.0 | *4.20 | 3.37 | 3.32 | 2.84 | 2.70 | 106 |
| 61 | 81.3 | 4.80 | 0.0 | 3.63 | 0.0 | 1.31 | 106 |
| 62 | 81.6 | 4.60 | 0.0 | 0.0 | 3.79 | 2.81 | 106 |
| 63 | 16.0 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 65 | 62.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 66 | 68.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 67 | 66.3 | 3.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 68 | 27.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 69 | 68.0 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 70 | 63.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 71 | 62.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |

KON 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 72 | 78.7 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 73 | 50.6 | 5.50 | 0.0 | 4.04 | 0.0 | 0.72 | 106 |
| 74 | 52.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 75 | 46.9 | 4.50 | 0.0 | 2.77 | 0.0 | 2.28 | 106 |
| 76 | 43.6 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 77 | 66.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 78 | 67.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 79 | 50.3 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 80 | 46.5 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 81 | 64.5 | 3.50 | 3.96 | 3.74 | 0.0 | 0.94 | 106 |
| 82 | 62.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 83 | 58.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 84 | 62.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 85 | 67.8 | 3.60 | 0.0 | 4.42 | 0.0 | 0.0 | 306 |
| 86 | 67.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 87 | 14.6 | 4.60 | 3.60 | 3.45 | 0.0 | 1.71 | 106 |
| 88 | 30.5 | 5.10 | 4.47 | 0.0 | 4.07 | 0.86 | 106 |
| 89 | 71.3 | 4.50 | 4.00 | 0.0 | 0.0 | 1.95 | 106 |
| 90 | 16.0 | *4.50 | 3.91 | 3.90 | 0.0 | 1.43 | 106 |
| 92 | 68.3 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 93 | 68.3 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 94 | 15.9 | 4.40 | 3.32 | 3.44 | 0.0 | 5.06 | 106 |
| 95 | 56.7 | 5.20 | 4.15 | 3.89 | 3.38 | 1.26 | 106 |
| 96 | 54.8 | 4.50 | 3.60 | 0.0 | 0.0 | 0.78 | 106 |
| 97 | 16.0 | *4.10 | 3.49 | 3.45 | 2.97 | 2.04 | 106 |
| 98 | 16.0 | *4.30 | 3.17 | 3.18 | 2.77 | 1.88 | 106 |
| 99 | 16.0 | *4.10 | 2.89 | 2.64 | 0.0 | 3.02 | 106 |
| 100 | 14.7 | 3.60 | 2.76 | 2.59 | 0.0 | 3.12 | 106 |
| 101 | 16.0 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 102 | 16.6 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 103 | 16.1 | *4.00 | 3.20 | 3.01 | 0.0 | 2.05 | 106 |
| 104 | 15.9 | *4.30 | 3.45 | 3.40 | 0.0 | 2.58 | 106 |
| 105 | 16.1 | *4.20 | 3.58 | 3.59 | 0.0 | 1.58 | 106 |
| 106 | 15.8 | *4.40 | 3.14 | 2.24 | 0.0 | 3.27 | 106 |
| 107 | 60.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 108 | 46.7 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 109 | 42.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 110 | 16.0 | *3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 111 | 65.6 | 4.80 | 4.31 | 4.10 | 0.0 | 1.80 | 106 |
| 112 | 84.0 | 5.70 | 4.80 | 0.0 | 4.45 | 0.93 | 106 |
| 113 | 16.0 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 114 | 81.3 | 4.80 | 0.0 | 3.70 | 0.0 | 0.0 | 106 |
| 115 | 41.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 116 | 39.1 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 117 | 40.8 | 4.50 | 3.69 | 0.0 | 0.0 | 3.46 | 106 |
| 118 | 40.8 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 119 | 40.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 506 |
| 120 | 45.6 | 4.90 | 4.52 | 0.0 | 3.31 | 0.89 | 106 |
| 122 | 65.6 | 3.50 | 0.0 | 3.69 | 0.0 | 2.40 | 106 |

KON 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LO/LR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 123 | 62.3 | 4.60 | 0.0 | 3.84 | 0.0 | 0.71 | 106 |
| 124 | 71.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 125 | 24.4 | 4.50 | 0.0 | 3.25 | 0.0 | 2.02 | 106 |
| 126 | 63.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 129 | 45.9 | 4.80 | 3.72 | 0.0 | 0.0 | 0.64 | 106 |
| 130 | 69.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 131 | 71.2 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 132 | 63.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 133 | 70.8 | 3.80 | 4.12 | 0.0 | 0.0 | 0.59 | 106 |
| 134 | 70.6 | 3.40 | 4.79 | 0.0 | 0.0 | 0.78 | 106 |
| 135 | 50.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 136 | 66.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 137 | 53.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 138 | 62.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 139 | 63.7 | 4.80 | 0.0 | 3.49 | 0.0 | 0.96 | 106 |
| 140 | 20.2 | 3.50 | 3.64 | 0.0 | 0.0 | 0.0 | 306 |
| 141 | 44.8 | 5.30 | 3.83 | 3.66 | 0.0 | 0.58 | 306 |
| 142 | 55.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 143 | 61.3 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 144 | 43.6 | 4.00 | 3.30 | 0.0 | 0.0 | 0.49 | 106 |
| 145 | 71.2 | 4.80 | 3.77 | 3.44 | 0.0 | 1.84 | 106 |
| 146 | 70.8 | 4.70 | 3.71 | 0.0 | 0.0 | 1.83 | 106 |
| 147 | 71.0 | 4.90 | 3.95 | 0.0 | 0.0 | 1.33 | 106 |
| 148 | 70.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 149 | 33.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 150 | 45.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 151 | 44.1 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 152 | 63.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 153 | 63.2 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 154 | 61.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 155 | 69.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 156 | 68.1 | 5.00 | 4.84 | 0.0 | 4.28 | 0.12 | 106 |
| 157 | 67.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 158 | 65.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 159 | 63.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 160 | 67.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 161 | 68.3 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 162 | 68.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 163 | 18.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 164 | 67.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 165 | 67.8 | 4.90 | 4.48 | 3.94 | 0.0 | 0.92 | 106 |
| 166 | 48.2 | 3.80 | 0.0 | 3.27 | 0.0 | 0.80 | 106 |
| 168 | 63.2 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 169 | 59.9 | 3.80 | 0.0 | 3.43 | 0.0 | 0.85 | 106 |
| 170 | 64.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 171 | 67.5 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 506 |
| 172 | 47.2 | 5.30 | 5.51 | 0.0 | 4.34 | 0.64 | 106 |
| 173 | 30.2 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |

KON 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 174 | 29.4 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 175 | 28.3 | 4.90 | 4.20 | 4.04 | 0.0 | 0.58 | 106 |
| 176 | 37.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 177 | 30.4 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 178 | 65.2 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 179 | 29.1 | 4.40 | 3.14 | 2.93 | 0.0 | 1.00 | 106 |
| 180 | 77.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 181 | 42.3 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 182 | 69.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 183 | 45.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 184 | 62.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 185 | 63.9 | 3.30 | C.C | 0.0 | 0.0 | 0.0 | 306 |
| 186 | 43.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 187 | 38.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 188 | 38.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 189 | 40.8 | 4.40 | 0.0 | 3.11 | 0.0 | 2.10 | 106 |
| 190 | 39.1 | 4.20 | C.C | 0.0 | 0.0 | 0.0 | 206 |
| 191 | 66.7 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 192 | 38.5 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 206 |
| 193 | 14.2 | 4.40 | 3.90 | 0.0 | 0.0 | 0.54 | 106 |
| 194 | 40.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 195 | 44.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 196 | 39.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 197 | 35.4 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 306 |
| 198 | 38.3 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 199 | 38.3 | 3.30 | C.C | 0.0 | 0.0 | 0.0 | 306 |
| 200 | 42.2 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 201 | 38.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 202 | 39.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 203 | 36.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 204 | 38.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 205 | 62.5 | 3.60 | 4.09 | 0.0 | 0.0 | 0.34 | 106 |
| 206 | 40.5 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 207 | 41.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 208 | 40.9 | 4.10 | 3.32 | 0.0 | 0.0 | 0.0 | 606 |
| 209 | 45.0 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 206 |
| 210 | 36.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 211 | 29.9 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 212 | 62.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 213 | 40.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 214 | 44.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 216 | 64.9 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 206 |
| 217 | 61.7 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 206 |
| 218 | 30.5 | 3.70 | 3.26 | 0.0 | 0.0 | 1.18 | 106 |
| 219 | 63.4 | 3.40 | C.C | 0.0 | 0.0 | 0.0 | 306 |
| 220 | 67.1 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 206 |
| 221 | 20.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 222 | 65.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 223 | 13.0 | *4.30 | 3.58 | 3.44 | 0.0 | 0.62 | 106 |

KON 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 224 | 35.4 | 4.00 | 3.32 | 0.0 | 0.0 | 1.13 | 106 |
| 225 | 42.6 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 226 | 69.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 227 | 64.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 228 | 69.1 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 229 | 35.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 230 | 62.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 506 |
| 231 | 69.4 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 245 | 57.9 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 247 | 18.0 | 2.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 248 | 44.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 249 | 67.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 250 | 67.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 251 | 65.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 252 | 68.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 253 | 53.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 254 | 67.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 255 | 45.2 | *4.60 | 3.77 | 0.0 | 0.0 | 0.40 | 106 |
| 256 | 20.6 | 3.50 | 3.34 | 3.20 | 0.0 | 0.21 | 106 |
| 257 | 66.2 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 258 | 68.8 | 3.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 259 | 65.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 260 | 38.9 | 5.50 | 3.43 | 3.33 | 0.0 | 0.56 | 106 |
| 261 | 70.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 262 | 47.9 | 4.90 | 3.92 | 0.0 | 0.0 | 0.45 | 106 |
| 263 | 9.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 264 | 63.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 265 | 43.3 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 266 | 35.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 267 | 48.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 268 | 71.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 269 | 61.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 270 | 43.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 271 | 68.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 272 | 44.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 273 | 22.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 274 | 63.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 275 | 53.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 276 | 72.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 277 | 101.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 278 | 23.9 | 5.40 | 4.76 | 4.51 | 0.0 | 2.22 | 106 |
| 279 | 68.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 280 | 44.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 281 | 56.6 | 5.30 | 3.64 | 3.38 | 0.0 | 1.55 | 106 |
| 282 | 24.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 283 | 59.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 284 | 46.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 285 | 46.5 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 286 | 64.2 | 4.50 | 5.02 | 0.0 | 0.0 | 1.30 | 106 |

KON 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 287 | 46.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 288 | 50.8 | 3.40 | 0.0 | 2.98 | 0.0 | 0.63 | 106 |
| 289 | 64.3 | 3.60 | 3.42 | 3.73 | 0.0 | 0.43 | 106 |
| 290 | 49.3 | 3.50 | 3.83 | 3.64 | 0.0 | 2.04 | 106 |
| 291 | 77.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 292 | 68.0 | 5.20 | 3.67 | 4.02 | 0.0 | 0.68 | 106 |
| 293 | 43.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 294 | 41.5 | 5.20 | 5.05 | 0.0 | 3.74 | 0.51 | 106 |
| 295 | 43.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 296 | 50.5 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 297 | 67.0 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 298 | 42.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 299 | 61.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 300 | 66.6 | 4.70 | 0.0 | 4.46 | 3.97 | 0.45 | 106 |
| 301 | 62.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 302 | 42.0 | 3.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 304 | 68.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 305 | 70.6 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 306 | 44.8 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 307 | 69.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 308 | 45.2 | 3.40 | 3.28 | 2.94 | 0.0 | 0.42 | 106 |
| 309 | 46.8 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 310 | 68.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 311 | 33.5 | 3.60 | 3.11 | 2.58 | 0.0 | 0.0 | 106 |
| 312 | 54.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 313 | 22.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 314 | 63.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 315 | 41.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 316 | 66.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 317 | 46.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 318 | 46.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 319 | 45.0 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 320 | 45.8 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 166 |
| 321 | 55.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 322 | 63.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 323 | 81.8 | *5.00 | 4.42 | 3.78 | 2.96 | 7.14 | 106 |
| 324 | 42.3 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 325 | 41.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 326 | 64.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 327 | 66.1 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 328 | 64.6 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 330 | 60.7 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 331 | 62.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 332 | 23.1 | 4.20 | 3.96 | 4.18 | 0.0 | 8.00 | 106 |
| 333 | 30.9 | 3.90 | 0.0 | 2.64 | 0.0 | 0.0 | 106 |
| 334 | 49.9 | 4.80 | 3.27 | 2.93 | 0.0 | 1.69 | 106 |
| 335 | 27.3 | 4.00 | 3.20 | 3.12 | 2.57 | 0.62 | 106 |
| 336 | 70.9 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 337 | 67.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |

KON 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 338 | 62.6 | 4.70 | 3.50 | 3.05 | 0.0 | 0.0 | 306 |
| 339 | 38.9 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 340 | 62.8 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 341 | 81.7 | 5.40 | 5.30 | 4.88 | 4.46 | 0.0 | 106 |
| 343 | 81.7 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 344 | 28.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 345 | 70.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 346 | 81.8 | 4.70 | 3.91 | 3.16 | 0.0 | 0.0 | 106 |
| 347 | 28.0 | 4.50 | 4.22 | 3.92 | 3.52 | 0.0 | 106 |
| 348 | 61.2 | 4.70 | 0.0 | 4.78 | 0.0 | 0.0 | 106 |
| 349 | 69.2 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 350 | 27.2 | 4.90 | 4.43 | 4.02 | 3.42 | 0.0 | 106 |
| 351 | 111.5 | 4.90 | 4.27 | 4.40 | 4.25 | 0.91 | 106 |
| 352 | 31.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 412 | 81.7 | 5.00 | 4.42 | 3.70 | 0.0 | 2.68 | 106 |
| 413 | 61.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 414 | 44.3 | 3.70 | 3.29 | 0.0 | 0.0 | 0.0 | 106 |
| 415 | 40.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 416 | 50.0 | 5.50 | 4.56 | 4.08 | 3.52 | 7.08 | 106 |
| 417 | 63.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 418 | 66.1 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 419 | 50.0 | 5.40 | 4.36 | 3.68 | 3.15 | 5.18 | 106 |
| 420 | 22.6 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 421 | 44.3 | 5.10 | 4.65 | 3.86 | 3.47 | 0.0 | 106 |
| 422 | 17.9 | *4.60 | 3.01 | 2.72 | 2.43 | 0.77 | 106 |
| 423 | 57.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 424 | 62.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 425 | 63.5 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 426 | 28.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 427 | 36.1 | 5.60 | 4.70 | 4.57 | 4.41 | 2.60 | 106 |
| 428 | 65.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 429 | 41.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 430 | 31.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 431 | 43.3 | *4.60 | 3.73 | 3.28 | 2.89 | 0.0 | 106 |
| 467 | 79.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 469 | 64.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 470 | 48.5 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 471 | 45.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 472 | 68.2 | 5.20 | 3.96 | 3.94 | 3.63 | 1.63 | 106 |
| 473 | 63.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 474 | 43.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 475 | 23.0 | 4.70 | 3.84 | 3.33 | 2.89 | 0.0 | 106 |
| 476 | 67.6 | 5.20 | 4.35 | 3.93 | 3.52 | 0.54 | 106 |
| 477 | 48.7 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 478 | 64.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 479 | 23.7 | 4.10 | 3.38 | 3.47 | 0.0 | 0.22 | 106 |
| 481 | 58.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 482 | 71.4 | 4.20 | 3.65 | 0.0 | 0.0 | 0.44 | 106 |
| 483 | 47.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |

KON 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| | | | | | | 0.0 | 206 |
| | | | | | | 0.0 | 306 |
| 484 | 16.0 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 485 | 82.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 486 | 27.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 487 | 40.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 488 | 40.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 489 | 40.5 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 490 | 78.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 512 | 15.0 | 4.00 | 2.63 | 3.19 | 2.68 | 0.0 | 106 |
| 603 | 29.0 | 4.40 | 3.14 | 3.10 | 0.0 | 0.94 | 106 |
| 604 | 25.9 | 3.60 | 3.45 | 3.10 | 2.70 | 0.70 | 106 |
| 685 | 52.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 686 | 16.1 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 687 | 57.5 | 5.50 | 4.99 | 4.67 | 3.86 | 3.40 | 106 |
| 688 | 53.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 689 | 57.5 | 5.50 | 4.79 | 3.96 | 0.0 | 0.57 | 106 |
| 690 | 57.4 | 5.50 | 4.61 | 3.67 | 0.0 | 7.71 | 106 |
| 691 | 64.9 | 4.60 | 3.39 | 3.34 | 3.00 | 0.0 | 166 |
| 691 | 56.2 | 4.30 | 3.35 | 3.18 | 0.0 | 0.58 | 136 |
| 692 | 45.1 | 5.50 | 4.24 | 4.17 | 0.0 | 0.51 | 106 |
| 693 | 52.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 694 | 63.4 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 696 | 40.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 106 |
| 697 | 75.8 | 4.40 | 3.88 | 3.26 | 0.0 | 0.0 | 206 |
| 698 | 71.0 | 4.80 | 0.0 | 3.88 | 0.0 | 0.0 | 106 |
| 699 | 39.1 | 6.20 | 3.78 | 3.11 | 0.0 | 0.0 | 306 |
| 700 | 43.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 536 |
| 701 | 40.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 106 |
| 702 | 45.4 | 5.50 | 5.50 | 4.87 | 4.41 | 0.0 | 136 |
| 703 | 45.8 | 3.80 | 2.70 | 2.78 | 0.0 | 0.0 | 106 |
| 704 | 26.5 | 5.20 | 4.15 | 0.0 | 0.0 | 0.77 | 106 |
| 705 | 44.5 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 706 | 29.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 707 | 27.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 708 | 61.5 | *4.50 | 3.70 | 3.74 | 0.0 | 1.08 | 106 |
| 709 | 42.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 236 |
| 710 | 70.9 | 4.30 | 4.23 | 3.37 | 0.0 | 1.09 | 106 |
| 711 | 80.5 | *5.30 | 4.72 | 4.37 | 0.0 | 2.76 | 106 |
| 712 | 45.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 713 | 64.6 | 4.50 | 4.61 | 0.0 | 0.0 | 0.0 | 136 |
| 714 | 26.7 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 715 | 68.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 716 | 79.8 | 5.50 | 5.73 | 4.83 | 0.0 | 1.19 | 106 |
| 717 | 22.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 718 | 43.3 | 4.70 | 0.0 | 3.56 | 0.0 | 0.0 | 136 |
| 720 | 66.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 721 | 60.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 326 |
| 722 | 44.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 723 | 62.8 | 4.80 | 4.84 | 3.87 | 0.0 | 6.28 | 106 |
| 724 | 69.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 236 |

KON 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 725 | 55.2 | 3.90 | C.C | 0.0 | 0.0 | | |
| 726 | 82.1 | 4.10 | 4.37 | 4.60 | 0.0 | 0.0 | 306 |
| 727 | 42.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.63 | 106 |
| 728 | 30.0 | 4.50 | 2.64 | 2.58 | 0.0 | 0.0 | 206 |
| 729 | 45.6 | 3.90 | 0.0 | 0.0 | 0.0 | 4.88 | 136 |
| 730 | 26.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 731 | 34.9 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 306 |
| 732 | 67.7 | 4.40 | 3.91 | 3.53 | 0.0 | 0.0 | 306 |
| 733 | 26.4 | 3.70 | C.C | 0.0 | 0.0 | 2.99 | 106 |
| 734 | 23.3 | 4.30 | 3.52 | 2.68 | 0.0 | 0.0 | 206 |
| 735 | 71.8 | 4.00 | C.C | 0.0 | 0.0 | 8.19 | 106 |
| 736 | 70.6 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 506 |
| 737 | 65.2 | 4.60 | 3.62 | 3.62 | 0.0 | 0.0 | 206 |
| 738 | 70.2 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 106 |
| 739 | 70.1 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 306 |
| 741 | 21.7 | *4.80 | 3.46 | 3.29 | 2.92 | 0.0 | 136 |
| 742 | 39.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 106 |
| 743 | 46.5 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 106 |
| 744 | 79.9 | 5.70 | 5.51 | 5.44 | 4.73 | 0.72 | 306 |
| 745 | 80.6 | 4.40 | C.C | 0.0 | 0.0 | 0.0 | 106 |
| 746 | 26.8 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 306 |
| 747 | 28.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 236 |
| 748 | 45.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 749 | 47.1 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 306 |
| 751 | 22.3 | 4.30 | 3.55 | 3.36 | 2.86 | 0.92 | 306 |
| 752 | 20.9 | 5.40 | 4.23 | 3.83 | 3.34 | 1.14 | 106 |
| 753 | 23.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 754 | 40.1 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 206 |
| 755 | 30.8 | 5.20 | C.C | 0.0 | 0.0 | 0.0 | 306 |
| 756 | 65.3 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 236 |
| 757 | 60.7 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 206 |
| 758 | 52.7 | 5.10 | 4.52 | 3.70 | 3.55 | 0.0 | 306 |
| 759 | 22.7 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 106 |
| 760 | 43.1 | 5.60 | 3.77 | 3.31 | 0.0 | 0.0 | 306 |
| 761 | 65.6 | 5.20 | 3.82 | 3.88 | 3.24 | 8.04 | 136 |
| 762 | 16.8 | 4.50 | 3.79 | 3.58 | 3.13 | 0.39 | 106 |
| 763 | 29.1 | 3.90 | C.C | 0.0 | 0.0 | 2.61 | 106 |
| 764 | 64.7 | 4.70 | C.C | 0.0 | 0.0 | 0.0 | 306 |
| 765 | 28.5 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 766 | 62.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 767 | 29.7 | 4.40 | C.C | 0.0 | 0.0 | 0.0 | 206 |
| 768 | 45.8 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 236 |
| 769 | 45.8 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 306 |
| 770 | 43.7 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 306 |
| 771 | 15.7 | *4.40 | 3.29 | 2.78 | 0.0 | 0.0 | 206 |
| 772 | 65.2 | 3.90 | C.C | 0.0 | 0.0 | 2.17 | 106 |
| 773 | 17.1 | 3.90 | 2.58 | 0.0 | 0.0 | 0.0 | 306 |
| 774 | 41.9 | 4.70 | C.C | 2.74 | 0.0 | 2.45 | 136 |
| 775 | 39.3 | 5.40 | 4.92 | 4.31 | 3.97 | 1.20 | 206 |
| | | | | | | | 106 |

KON 01/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 776 | 63.3 | 4.80 | 3.94 | 0.0 | 0.0 | 1.38 | 136 |
| 777 | 78.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 778 | 26.8 | 5.10 | 3.73 | 3.59 | 2.87 | 0.0 | 106 |
| 779 | 78.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 780 | 68.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 781 | 44.9 | 5.00 | 0.0 | 3.81 | 3.75 | 0.0 | 106 |
| 782 | 68.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 783 | 64.2 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 784 | 69.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 236 |
| 785 | 76.7 | 5.30 | 4.55 | 4.21 | 3.66 | 1.10 | 106 |
| 786 | 27.0 | 4.30 | 0.0 | 3.03 | 0.0 | 2.17 | 106 |
| 787 | 78.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 788 | 46.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 789 | 78.8 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 790 | 78.7 | 4.70 | 4.33 | 3.89 | 0.0 | 2.12 | 106 |
| 791 | 63.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 793 | 43.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 849 | 18.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 850 | 62.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 851 | 63.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 852 | 68.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 853 | 66.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 854 | 52.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 855 | 46.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 856 | 22.0 | 3.70 | 2.94 | 2.88 | 0.0 | 0.0 | 106 |
| 857 | 65.2 | 4.80 | 3.87 | 3.20 | 3.09 | 0.88 | 106 |
| 858 | 69.9 | 4.70 | 4.10 | 0.0 | 0.0 | 0.0 | 166 |
| 859 | 64.8 | 5.70 | 5.24 | 5.30 | 4.88 | 0.24 | 106 |
| 860 | 65.2 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 861 | 53.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 862 | 42.7 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 863 | 22.8 | 3.60 | 3.61 | 0.0 | 0.0 | 0.0 | 106 |
| 864 | 69.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 865 | 38.7 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 866 | 20.1 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 867 | 68.2 | 4.10 | 3.26 | 0.0 | 0.0 | 0.0 | 166 |
| 868 | 62.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 869 | 65.3 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 870 | 57.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 871 | 71.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 306 |
| 872 | 37.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 873 | 55.5 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 236 |
| 874 | 21.7 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 206 |
| 875 | 55.6 | 4.50 | 4.89 | 4.12 | 0.0 | 0.0 | 106 |

APPENDIX II-H
BASIC DATA FOR OGD

NGD 01/01/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 1 | 71.6 | 4.10 | 0.0 | 4.71 | 0.0 | 0.0 | 107 |
| 2 | 78.2 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 3 | 79.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 4 | 85.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 5 | 69.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 6 | 95.0 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 107 |
| 7 | 76.1 | 4.80 | 0.0 | 4.34 | 0.0 | 0.0 | 207 |
| 8 | 76.0 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 9 | 77.9 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 10 | 72.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 11 | 114.7 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 12 | 71.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 13 | 114.6 | *4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 14 | 98.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 15 | 78.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 16 | 87.2 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 17 | 61.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 18 | 95.8 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 19 | 68.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 20 | 71.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 21 | 92.9 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 22 | 113.5 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 23 | 95.2 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 24 | 96.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 25 | 79.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 107 |
| 26 | 115.7 | 4.70 | 6.13 | 6.10 | 0.0 | 1.61 | 107 |
| 27 | 114.7 | 4.60 | 0.0 | 4.39 | 3.73 | 1.07 | 107 |
| 28 | 72.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 29 | 71.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 30 | 85.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 107 |
| 31 | 116.5 | 5.00 | 4.07 | 4.05 | 3.65 | 0.0 | 207 |
| 32 | 71.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 33 | 70.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 34 | 87.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 35 | 75.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.30 | 107 |
| 36 | 73.2 | 4.90 | 4.08 | 0.0 | 3.27 | 1.33 | 107 |
| 37 | 71.4 | 4.80 | 4.23 | 0.0 | 3.25 | 1.55 | 107 |
| 38 | 71.6 | 4.00 | 4.23 | 0.0 | 4.49 | 2.02 | 107 |
| 39 | 71.7 | 5.30 | 5.10 | 4.94 | 0.0 | 1.27 | 307 |
| 40 | 60.7 | 3.90 | 3.66 | 0.0 | 0.0 | 0.0 | 307 |
| 41 | 88.6 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 42 | 79.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 43 | 80.7 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 44 | 95.2 | 5.40 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 45 | 96.3 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 46 | 71.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 47 | 71.6 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 48 | 75.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 49 | 85.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | |

NGD 01/01/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 50 | 85.9 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 51 | 58.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 52 | 74.4 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 55 | 75.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 56 | 76.4 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 57 | 71.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 58 | 76.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 59 | 73.8 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 60 | 61.7 | *4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 61 | 114.5 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 62 | 114.7 | 4.60 | 0.0 | 4.02 | 0.0 | 0.90 | 107 |
| 63 | 61.7 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 65 | 70.9 | 3.80 | 0.0 | 4.00 | 0.0 | 0.0 | 107 |
| 66 | 79.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 67 | 86.2 | 3.20 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 68 | 74.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 69 | 79.6 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 70 | 71.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 71 | 71.9 | 3.80 | 0.0 | 3.41 | 0.0 | 1.09 | 107 |
| 72 | 108.7 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 73 | 103.2 | 5.90 | 0.0 | 4.06 | 0.0 | 0.0 | 107 |
| 74 | 102.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 75 | 95.3 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 76 | 92.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 77 | 89.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 78 | 78.8 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 79 | 101.2 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 80 | 99.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 81 | 96.9 | 3.90 | 0.0 | 3.88 | 0.0 | 0.76 | 107 |
| 82 | 71.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 83 | 71.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 84 | 72.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 85 | 84.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 86 | 76.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 87 | 69.3 | 4.60 | 0.0 | 3.38 | 0.0 | 0.71 | 107 |
| 88 | 83.3 | 5.10 | 4.93 | 4.72 | 0.0 | 0.72 | 107 |
| 89 | 115.5 | 4.50 | 0.0 | 4.27 | 0.0 | 0.47 | 107 |
| 90 | 61.7 | *4.50 | 4.05 | 3.79 | 0.0 | 0.88 | 107 |
| 92 | 80.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 93 | 80.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 94 | 61.6 | 4.40 | 3.87 | 0.0 | 0.0 | 0.92 | 107 |
| 95 | 106.0 | 5.20 | 0.0 | 3.92 | 0.0 | 0.53 | 107 |
| 96 | 105.5 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 97 | 61.7 | *4.10 | 3.96 | 3.34 | 0.0 | 0.54 | 107 |
| 98 | 61.7 | *4.30 | 3.60 | 0.0 | 0.0 | 0.46 | 107 |
| 99 | 61.7 | *4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 100 | 60.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 101 | 61.7 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 102 | 62.2 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |

000 01/01/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 103 | 61.9 | *4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 104 | 61.6 | *4.30 | 3.71 | 0.0 | 0.0 | 0.68 | 107 |
| 105 | 61.8 | *4.20 | 3.82 | 0.0 | 0.0 | 0.78 | 107 |
| 106 | 61.5 | *4.40 | 0.0 | 3.50 | 0.0 | 0.72 | 107 |
| 107 | 108.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 108 | 94.7 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 109 | 90.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 110 | 61.6 | *3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 111 | 75.3 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 112 | 117.7 | 5.70 | 5.27 | 0.0 | 4.69 | 1.20 | 107 |
| 113 | 61.7 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 114 | 114.3 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 122 | 75.3 | 3.90 | 0.0 | 3.58 | 0.0 | 0.0 | 107 |
| 127 | 84.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 128 | 72.4 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 129 | 94.3 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 130 | 83.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 131 | 87.1 | 4.70 | 3.81 | 0.0 | 0.0 | 0.32 | 107 |
| 132 | 72.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 133 | 86.0 | 5.20 | 0.0 | 4.20 | 0.0 | 0.28 | 107 |
| 134 | 85.8 | 5.40 | 4.98 | 0.0 | 4.15 | 0.26 | 107 |
| 135 | 102.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 136 | 84.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 137 | 99.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 138 | 82.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 139 | 73.2 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 140 | 68.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 141 | 96.2 | 5.30 | 4.14 | 4.03 | 0.0 | 0.50 | 307 |
| 142 | 89.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 143 | 73.9 | 3.40 | 3.84 | 0.0 | 0.0 | 0.0 | 107 |
| 144 | 95.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 214 | 95.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 216 | 74.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 217 | 110.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 218 | 51.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 219 | 72.2 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 220 | 75.6 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 221 | 69.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 222 | 72.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 223 | 47.6 | *4.30 | 0.0 | 3.87 | 0.0 | 0.40 | 107 |
| 224 | 86.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 225 | 91.9 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 226 | 85.9 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 227 | 75.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 228 | 83.5 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 229 | 60.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 230 | 71.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 231 | 85.8 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 232 | 64.3 | *4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |

OGD C1/C1/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/IP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 233 | 78.7 | 4.50 | C.C | 0.0 | 0.0 | 0.0 | 607 |
| 234 | 83.1 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 235 | 95.7 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 236 | 94.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 237 | 68.0 | 3.60 | C.0 | 0.0 | 0.0 | 0.0 | 507 |
| 238 | 95.6 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 239 | 96.1 | *3.70 | C.0 | 0.0 | 0.0 | 0.0 | 507 |
| 240 | 111.0 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 241 | 74.1 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 242 | 85.1 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 243 | 81.1 | 5.40 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 245 | 98.9 | 4.50 | C.0 | 0.0 | 0.0 | 0.0 | 507 |
| 247 | 66.8 | 2.70 | C.0 | 0.0 | 0.0 | 0.0 | 507 |
| 248 | 97.2 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 249 | 116.3 | C.C | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 250 | 114.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 251 | 79.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 252 | 79.1 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 307 |
| 253 | 102.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 254 | 83.0 | 4.20 | C.0 | 0.0 | 0.0 | 0.0 | 507 |
| 255 | 97.9 | *4.60 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 256 | 69.2 | 3.50 | C.0 | 0.0 | 0.0 | 0.0 | 507 |
| 257 | 77.5 | 3.30 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 258 | 83.1 | 3.00 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 259 | 74.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 260 | 86.1 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 261 | 85.2 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 262 | 99.3 | 4.90 | C.C | 0.0 | 0.0 | 0.0 | 607 |
| 263 | 57.3 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 264 | 71.4 | 3.80 | C.C | C.C | 0.0 | 0.0 | 507 |
| 265 | 94.6 | 4.20 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 266 | 54.8 | 3.60 | C.0 | 0.0 | 0.0 | 0.0 | 507 |
| 267 | 99.3 | 4.10 | C.0 | 0.0 | 0.0 | 0.0 | 507 |
| 268 | 83.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 269 | 74.2 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 507 |
| 270 | 95.9 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 271 | 78.7 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 272 | 95.5 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 273 | 71.8 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 274 | 71.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 275 | 102.2 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 507 |
| 285 | 99.3 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 207 |
| 310 | 81.1 | 3.90 | C.0 | 0.0 | 0.0 | 0.0 | 507 |
| 321 | 102.0 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 207 |
| 339 | 86.1 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 340 | 70.3 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 307 |
| 341 | 116.3 | 5.40 | C.0 | 0.0 | 0.0 | 0.0 | 507 |
| 342 | 87.2 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 343 | 116.4 | 4.90 | C.0 | 0.0 | 0.0 | 0.0 | 507 |

OGD 01/01/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=2CSEC | MS T=3CSEC | MS T=40SEC | LC/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 348 | 108.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 349 | 82.3 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 350 | 75.2 | 4.90 | 3.47 | 3.10 | 2.46 | 10.80 | 107 |
| 351 | 58.7 | 4.90 | 4.07 | 3.69 | 3.48 | 0.0 | 107 |
| 352 | 83.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 353 | 92.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 354 | 101.9 | 4.50 | 3.39 | 2.96 | 2.51 | 6.57 | 107 |
| 355 | 86.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 356 | 88.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 357 | 74.8 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 358 | 81.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 359 | 82.7 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 360 | 86.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 361 | 88.0 | 5.40 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 362 | 88.0 | 5.10 | 4.10 | 3.98 | 3.36 | 10.04 | 107 |
| 363 | 74.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 365 | 72.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 366 | 85.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 367 | 88.0 | 5.30 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 369 | 92.7 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 370 | 98.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 371 | 61.8 | *4.50 | 4.18 | 4.13 | 3.95 | 0.17 | 107 |
| 373 | 70.3 | 4.90 | 4.27 | 4.20 | 3.75 | 0.0 | 107 |
| 374 | 70.5 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 375 | 74.1 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 376 | 72.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 377 | 96.1 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 378 | 75.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 379 | 87.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 380 | 60.1 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 381 | 86.1 | 4.60 | 0.0 | 3.43 | 0.0 | 0.0 | 107 |
| 383 | 81.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 384 | 93.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 157 |
| 385 | 75.2 | 4.40 | 3.01 | 2.50 | 2.36 | 0.0 | 107 |
| 386 | 70.3 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 157 |
| 388 | 85.6 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 389 | 79.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 390 | 94.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 391 | 84.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 392 | 101.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 402 | 88.1 | 4.60 | 2.83 | 0.0 | 0.0 | 0.0 | 307 |
| 403 | 97.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 404 | 96.1 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 405 | 63.9 | *4.50 | 3.41 | 3.04 | 0.0 | 0.0 | 107 |
| 407 | 96.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 408 | 95.8 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 409 | 63.1 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 410 | 96.1 | 4.70 | 4.38 | 3.93 | 3.33 | 3.07 | 107 |
| 411 | 74.0 | 4.10 | 4.13 | 3.53 | 3.42 | 0.52 | 107 |

OGD 01/01/72 - 08/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 412 | 116.3 | 5.00 | 4.60 | 4.29 | 3.98 | 0.0 | 107 |
| 413 | 73.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 414 | 96.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 415 | 92.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 416 | 102.1 | 5.50 | 4.63 | 4.27 | 4.13 | 0.0 | 207 |
| 417 | 74.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 418 | 112.2 | 4.40 | 3.93 | 3.61 | 0.0 | 0.0 | 107 |
| 419 | 102.1 | *5.20 | 4.31 | 3.79 | 3.54 | 0.0 | 107 |
| 420 | 74.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 421 | 95.5 | 5.10 | 4.26 | 3.99 | 3.66 | 0.0 | 107 |
| 422 | 66.5 | *4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |
| 423 | 104.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 424 | 70.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 425 | 71.8 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 428 | 74.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 429 | 94.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 507 |
| 430 | 74.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 207 |
| 431 | 94.2 | *4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 307 |

APPENDIX II-1
BASIC DATA FOR KIP

KIP C6/C1/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 310 | 46.5 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 311 | 95.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 312 | 81.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 313 | 119.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 314 | 43.9 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 50R |
| 315 | 120.6 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 50R |
| 316 | 48.4 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 50R |
| 317 | 95.8 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 50R |
| 318 | 95.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 319 | 95.8 | 3.50 | C.0 | 0.0 | 0.0 | 0.0 | 50R |
| 320 | 96.4 | 3.90 | C.0 | 0.0 | 0.0 | 0.0 | 50R |
| 321 | 92.4 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 50R |
| 323 | 69.8 | *5.00 | 4.37 | 4.04 | 0.0 | 0.0 | 10R |
| 324 | 121.4 | 4.20 | 3.81 | 0.0 | 0.0 | 0.0 | 10R |
| 326 | 46.0 | 4.00 | C.0 | 0.0 | 0.0 | 0.0 | 50R |
| 327 | 40.4 | 3.40 | C.0 | 0.0 | 0.0 | 0.0 | 50R |
| 328 | 42.9 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 50R |
| 329 | 122.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 330 | 90.2 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 50R |
| 331 | 45.0 | 4.00 | C.0 | 0.0 | 0.0 | 0.0 | 50R |
| 332 | 120.8 | 4.20 | 3.81 | 3.50 | 0.0 | 0.0 | 10R |
| 333 | 120.0 | 3.90 | C.0 | 0.0 | 0.0 | 0.0 | 50R |
| 334 | 110.8 | 4.80 | C.C | 0.0 | 0.0 | 0.0 | 50R |
| 335 | 71.9 | 4.00 | 3.61 | 3.55 | 0.0 | 0.0 | 10R |
| 336 | 49.6 | 3.40 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 337 | 46.2 | 3.60 | C.0 | 0.0 | 0.0 | 0.0 | 50R |
| 338 | 44.5 | 4.70 | 3.49 | 3.71 | 0.0 | 0.0 | 10R |
| 339 | 93.2 | 5.50 | C.0 | 0.0 | 0.0 | 0.0 | 30R |
| 340 | 43.6 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 30R |
| 341 | 75.2 | 5.40 | 5.64 | 5.28 | 0.0 | 0.22 | 10R |
| 342 | 119.9 | 4.90 | 4.63 | 0.0 | 0.0 | 0.0 | 10R |
| 343 | 75.2 | 4.90 | C.0 | 0.0 | 0.0 | 0.0 | 30R |
| 344 | 114.3 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 345 | 98.8 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 346 | 75.1 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 347 | 111.3 | 4.50 | C.C | 0.0 | 0.0 | 0.0 | 30R |
| 348 | 95.3 | 4.70 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 349 | 46.9 | 4.40 | 4.05 | 0.0 | 0.0 | 0.0 | 10R |
| 350 | 123.6 | 4.90 | C.0 | 3.68 | 0.0 | 0.0 | 10R |
| 351 | 57.4 | 4.90 | 5.17 | 5.08 | 4.49 | 4.38 | 10R |
| 352 | 118.0 | 4.00 | 3.88 | 3.57 | 3.66 | 0.0 | 10R |
| 353 | 120.6 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 354 | 114.4 | 4.50 | 3.77 | 3.51 | 3.14 | 5.77 | 10R |
| 355 | 48.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 356 | 120.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 357 | 44.9 | 3.30 | C.C | 0.0 | 0.0 | 0.0 | 30R |
| 358 | 47.8 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 10R |
| 359 | 47.5 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 360 | 49.6 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 20R |

KIP C6/C1/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 361 | 120.7 | 5.40 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 362 | 120.8 | 5.10 | 5.00 | 4.74 | 4.32 | 0.0 | 10R |
| 363 | 43.9 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 30R |
| 365 | 44.9 | 3.80 | 3.29 | 3.13 | 2.82 | 0.0 | 10R |
| 366 | 112.5 | 4.70 | C.0 | 3.96 | 0.0 | 0.0 | 10R |
| 367 | 120.9 | 5.30 | C.0 | 0.0 | 0.0 | 0.0 | 15R |
| 369 | 120.2 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 370 | 121.4 | 3.60 | C.0 | 0.0 | 0.0 | 0.0 | 20R |
| 371 | 114.4 | *4.50 | 4.20 | 3.65 | 3.51 | 0.0 | 10R |
| 373 | 120.3 | 4.90 | C.C | 0.0 | 0.0 | 0.0 | 15R |
| 374 | 41.0 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 375 | 120.3 | 3.30 | C.C | 0.0 | 0.0 | 0.0 | 30R |
| 376 | 45.9 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 377 | 107.3 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 378 | 46.5 | 3.60 | C.0 | 0.0 | 0.0 | 0.0 | 20R |
| 379 | 120.0 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 380 | 110.0 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 381 | 48.9 | 4.60 | C.0 | 0.0 | 0.0 | 0.0 | 50R |
| 382 | 46.5 | 3.90 | C.0 | 0.0 | 0.0 | 0.0 | 20R |
| 384 | 120.3 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 385 | 119.0 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 386 | 41.5 | 5.00 | 4.57 | 4.18 | 0.0 | 1.92 | 10R |
| 388 | 47.1 | 4.50 | 2.94 | 2.76 | 2.54 | 5.18 | 10R |
| 389 | 44.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 390 | 121.9 | 4.00 | 3.46 | 3.36 | 3.23 | 1.68 | 10R |
| 391 | 61.7 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 20R |
| 392 | 106.3 | 3.60 | 3.85 | 3.32 | 0.0 | 0.0 | 10R |
| 393 | 44.4 | 4.30 | 3.37 | 2.99 | 2.74 | 0.0 | 10R |
| 394 | 45.9 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 30R |
| 395 | 73.8 | 4.10 | C.0 | 0.0 | 0.0 | 0.0 | 20R |
| 396 | 44.9 | 4.30 | 3.03 | 2.75 | 2.46 | 3.9R | 10R |
| 397 | 118.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 398 | 114.3 | *3.80 | C.0 | 0.0 | 0.0 | 0.0 | 30R |
| 399 | 46.8 | 4.50 | 3.93 | 3.48 | 3.05 | 0.0 | 10R |
| 402 | 121.0 | 4.60 | 2.73 | 3.45 | 0.0 | 1.25 | 10R |
| 403 | 103.1 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 20R |
| 404 | 121.7 | 3.50 | C.0 | 0.0 | 0.0 | 0.0 | 20R |
| 405 | 114.7 | *4.50 | C.0 | 0.0 | 0.0 | 0.0 | 30R |
| 407 | 107.4 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 50R |
| 408 | 102.4 | 3.40 | C.0 | 0.0 | 0.0 | 0.0 | 20R |
| 409 | 114.3 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 410 | 106.8 | 4.70 | 4.05 | 3.45 | 3.01 | 4.63 | 10R |
| 411 | 45.4 | 4.10 | 3.50 | 3.46 | 0.0 | 0.0 | 10R |
| 412 | 75.1 | 5.00 | 4.40 | 4.32 | 0.0 | 0.0 | 10R |
| 413 | 47.4 | 3.60 | C.0 | 0.0 | 0.0 | 0.0 | 50R |
| 414 | 107.4 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 30R |
| 415 | 108.1 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 416 | 110.9 | 5.50 | 3.94 | 3.62 | 0.0 | 0.0 | 10R |
| 417 | 45.9 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 30R |

KIP 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 418 | 93.5 | 4.40 | C.0 | 0.0 | 0.0 | 0.0 | 20R |
| 419 | 110.9 | *5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 420 | 104.3 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 421 | 106.9 | 5.10 | C.0 | 0.0 | 0.0 | 0.0 | 30R |
| 422 | 115.6 | *4.60 | 3.92 | 3.92 | 3.59 | 0.0 | 10R |
| 423 | 94.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 424 | 44.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 425 | 43.9 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 426 | 122.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 427 | 129.7 | 5.60 | 5.06 | 5.14 | 5.11 | 0.26 | 10R |
| 429 | 120.6 | 3.90 | 4.0R | 3.79 | 3.52 | 2.6R | 10R |
| 430 | 94.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 431 | 104.0 | *4.60 | C.0 | 0.0 | 0.0 | 0.0 | 30R |
| 432 | 120.9 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 433 | 73.5 | 4.90 | 4.43 | 4.06 | 0.0 | 1.45 | 10R |
| 435 | 42.4 | 3.40 | C.0 | 0.0 | 0.0 | 0.0 | 20R |
| 436 | 121.5 | 5.40 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 437 | 121.6 | 4.60 | C.C | 0.0 | 0.0 | 0.0 | 30R |
| 438 | 121.5 | 5.00 | 4.19 | 3.66 | 3.42 | 0.0 | 10R |
| 439 | 106.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 440 | 120.6 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 441 | 121.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 442 | 121.5 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 443 | 45.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 444 | 116.7 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 445 | 121.7 | 3.90 | C.0 | 0.0 | 0.0 | 0.0 | 30R |
| 446 | 44.8 | 4.40 | 3.40 | 3.16 | 0.0 | 0.0 | 10R |
| 447 | 48.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 448 | 48.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 449 | 94.8 | 4.60 | 4.00 | 3.49 | 3.30 | 0.0 | 10R |
| 450 | 92.3 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 20R |
| 451 | 91.3 | 4.30 | 3.70 | 3.24 | 2.8R | 0.0 | 10R |
| 452 | 119.4 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 453 | 120.2 | 4.00 | C.0 | 0.0 | 0.0 | 0.0 | 50R |
| 454 | 121.7 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 455 | 120.1 | 4.10 | C.0 | 0.0 | 0.0 | 0.0 | 30R |
| 456 | 93.3 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 457 | 122.0 | 3.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 458 | 111.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 459 | 51.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 460 | 45.0 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 30R |
| 461 | 94.7 | 5.00 | 4.50 | 4.62 | 3.93 | 1.25 | 10R |
| 462 | 86.8 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 20R |
| 463 | 117.0 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 464 | 45.6 | 4.90 | 4.03 | 3.95 | 3.35 | 0.25 | 10R |
| 465 | 48.4 | 4.20 | C.0 | 0.0 | 0.0 | 0.0 | 20R |
| 466 | 122.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 467 | 64.3 | 4.10 | 3.63 | 3.27 | 0.0 | 0.0 | 10R |
| 469 | 44.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |

KIP C6/C1/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LR PATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 470 | 91.0 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 471 | 104.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 472 | 46.3 | 5.20 | 4.11 | 4.30 | 3.62 | 0.0 | 10R |
| 473 | 44.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 474 | 115.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 475 | 118.3 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 476 | 46.0 | 5.20 | 3.89 | 4.05 | 3.32 | 0.50 | 10R |
| 477 | 107.0 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 478 | 42.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 479 | 121.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 482 | 48.2 | 4.20 | 3.70 | 3.10 | 0.0 | 0.0 | 10R |
| 483 | 116.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 484 | 114.3 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 485 | 72.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 486 | 121.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 487 | 121.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 488 | 121.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 489 | 121.5 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 490 | 62.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 491 | 97.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 492 | 70.0 | 5.10 | 4.11 | 3.78 | 0.0 | 0.0 | 10R |
| 493 | 47.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 494 | 46.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 495 | 49.3 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 496 | 91.2 | 5.20 | 3.98 | 3.57 | 0.0 | 0.0 | 10R |
| 497 | 117.0 | 4.90 | 4.44 | 4.34 | 3.76 | 1.82 | 10R |
| 498 | 91.2 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 499 | 73.5 | 4.60 | 4.06 | 3.78 | 3.21 | 0.0 | 10R |
| 500 | 48.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 501 | 44.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 502 | 89.6 | 3.90 | 3.62 | 3.39 | 2.96 | 0.0 | 10R |
| 503 | 45.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 504 | 124.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 505 | 46.1 | 5.30 | 4.56 | 4.33 | 3.90 | 2.16 | 10R |
| 506 | 46.0 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 508 | 48.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 509 | 46.2 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 510 | 100.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 511 | 97.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 512 | 117.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 513 | 49.8 | 5.00 | 3.97 | 4.06 | 0.0 | 0.0 | 10R |
| 514 | 43.4 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 515 | 47.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 516 | 105.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 517 | 97.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 518 | 114.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 520 | 87.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 521 | 112.3 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 522 | 95.0 | 5.50 | 5.03 | 4.69 | 4.32 | 2.56 | 10R |

KIP 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DFGRFES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LP RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 523 | 95.1 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 524 | 125.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 525 | 95.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 526 | 47.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 527 | 116.9 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 528 | 46.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 529 | 100.3 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 530 | 119.9 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 531 | 48.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 532 | 114.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 533 | 114.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 534 | 44.1 | 5.10 | 4.49 | 3.94 | 3.57 | 0.0 | 10R |
| 535 | 64.9 | 5.10 | 4.49 | 4.23 | 0.0 | 0.0 | 10R |
| 537 | 121.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 538 | 110.8 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 539 | 45.5 | 4.80 | 3.95 | 3.78 | 3.18 | 0.0 | 10R |
| 540 | 118.6 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 541 | 45.5 | 5.10 | 4.77 | 4.63 | 0.0 | 0.50 | 10R |
| 542 | 103.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 543 | 74.2 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 544 | 88.3 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 545 | 117.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 546 | 45.1 | 4.80 | 3.61 | 3.47 | 3.21 | 0.0 | 10R |
| 547 | 73.2 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 548 | 120.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 549 | 63.6 | 3.70 | 3.27 | 2.92 | 0.0 | 0.0 | 10R |
| 550 | 105.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 551 | 124.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 552 | 103.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 553 | 105.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 554 | 122.2 | 4.50 | 0.0 | 3.33 | 0.0 | 0.0 | 15R |
| 555 | 123.5 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 23R |
| 556 | 50.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 557 | 120.0 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 558 | 44.9 | 5.60 | 5.47 | 5.29 | 4.89 | 0.52 | 10R |
| 559 | 44.9 | 5.00 | 5.31 | 5.28 | 0.0 | 0.50 | 10R |
| 560 | 120.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 561 | 120.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 562 | 47.1 | 4.50 | 3.40 | 3.32 | 0.0 | 0.0 | 10R |
| 563 | 45.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 564 | 117.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 565 | 46.9 | 5.30 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 566 | 120.0 | 4.50 | 3.75 | 3.57 | 3.72 | 0.0 | 10R |
| 567 | 120.0 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 35R |
| 568 | 62.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 569 | 48.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 570 | 119.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 571 | 120.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 572 | 45.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |

KIP C6/C1/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 470 | 91.0 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 471 | 104.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 472 | 46.3 | 5.20 | 4.11 | 4.30 | 3.62 | 0.0 | 10R |
| 473 | 44.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 474 | 115.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 475 | 118.3 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 476 | 46.0 | 5.20 | 3.89 | 4.05 | 3.32 | 0.50 | 10R |
| 477 | 107.0 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 478 | 42.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 479 | 121.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 482 | 48.2 | 4.20 | 3.70 | 3.10 | 0.0 | 0.0 | 10R |
| 483 | 116.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 484 | 114.3 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 485 | 72.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 486 | 121.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 487 | 121.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 488 | 121.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 489 | 121.5 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 490 | 62.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 491 | 97.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 492 | 70.0 | 5.10 | 4.11 | 3.78 | 0.0 | 0.0 | 10R |
| 493 | 47.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 494 | 46.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 495 | 49.3 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 496 | 91.2 | 5.20 | 3.98 | 3.57 | 0.0 | 0.0 | 10R |
| 497 | 117.0 | 4.50 | 4.44 | 4.34 | 3.76 | 1.82 | 10R |
| 498 | 91.2 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 499 | 73.5 | 4.60 | 4.06 | 3.78 | 3.21 | 0.0 | 10R |
| 500 | 48.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 501 | 44.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 502 | 89.6 | 3.90 | 3.62 | 3.39 | 2.96 | 0.0 | 10R |
| 503 | 45.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 504 | 124.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 505 | 46.1 | 5.30 | 4.56 | 4.33 | 3.90 | 2.16 | 10R |
| 506 | 46.0 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 508 | 48.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 509 | 46.2 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 510 | 100.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 511 | 97.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 512 | 117.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 513 | 49.8 | 5.00 | 3.97 | 4.06 | 0.0 | 0.0 | 10R |
| 514 | 43.4 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 515 | 47.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 516 | 105.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 517 | 97.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 518 | 114.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 520 | 87.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 521 | 112.3 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 522 | 95.0 | 5.50 | 5.03 | 4.69 | 4.32 | 2.56 | 10R |

KIP 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 573 | 45.6 | 5.70 | 7.15 | 5.88 | 5.25 | 0.63 | 10P |
| 574 | 45.4 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 575 | 45.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 576 | 122.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 577 | 45.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 578 | 45.4 | 4.70 | 3.77 | 3.51 | 0.0 | 0.0 | 10P |
| 579 | 45.4 | 4.90 | 4.57 | 0.0 | 0.0 | 0.0 | 10P |
| 580 | 45.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 581 | 46.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 582 | 113.2 | 4.50 | 0.0 | 4.21 | 0.0 | 0.0 | 16P |
| 583 | 119.9 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 584 | 119.6 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 585 | 124.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 586 | 120.4 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 587 | 122.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 588 | 45.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 589 | 45.3 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 23P |
| 590 | 43.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 35P |
| 591 | 43.1 | 4.50 | 3.56 | 3.56 | 3.0P | 1.13 | 10P |
| 592 | 119.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 593 | 40.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 594 | 115.4 | 4.70 | 4.01 | 3.61 | 0.0 | 1.65 | 10P |
| 595 | 118.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 596 | 44.6 | 5.10 | 4.11 | 4.00 | 0.0 | 1.50 | 10P |
| 597 | 46.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 598 | 120.0 | 5.50 | 4.44 | 4.02 | 0.0 | 2.76 | 10P |
| 599 | 43.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 23P |
| 600 | 119.1 | 4.30 | 0.0 | 4.45 | 0.0 | 0.0 | 17P |
| 601 | 118.7 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 602 | 47.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 603 | 69.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 604 | 102.2 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 23P |
| 605 | 75.6 | 5.10 | 4.26 | 3.53 | 0.0 | 2.13 | 10P |
| 606 | 63.9 | 4.80 | 3.92 | 3.35 | 0.0 | 3.11 | 10P |
| 607 | 46.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 608 | 28.0 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 609 | 43.0 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 610 | 93.1 | 5.20 | 4.20 | 3.66 | 3.43 | 0.0 | 10P |
| 611 | 81.1 | 5.00 | 4.20 | 3.7P | 0.0 | 3.12 | 10P |
| 612 | 117.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 613 | 44.5 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 614 | 44.9 | 5.30 | 5.13 | 5.02 | 4.51 | 0.20 | 10P |
| 615 | 120.2 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 50P |
| 618 | 93.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 619 | 105.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 40P |
| 620 | 45.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 32P |
| 621 | 46.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 622 | 47.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 30P |
| 623 | 45.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |

KIP 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LO/LR RATIO | COMMENT |
|-----------|--------------------|-------|---------------|---------------|---------------|----------------|---------|
| 624 | 48.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 625 | 43.9 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 508 |
| 626 | 93.2 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 258 |
| 627 | 117.1 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 238 |
| 628 | 43.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 629 | 104.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 538 |
| 630 | 43.2 | 4.30 | 3.60 | 3.20 | 0.0 | 2.64 | 108 |
| 631 | 46.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 632 | 49.1 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 538 |
| 633 | 45.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 634 | 105.6 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 635 | 48.9 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 636 | 48.4 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 637 | 44.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 638 | 45.6 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 639 | 118.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 640 | 118.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 641 | 118.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 642 | 81.8 | 4.00 | 3.83 | 3.79 | 3.26 | 0.0 | 108 |
| 643 | 44.4 | 4.00 | 3.75 | 3.27 | 0.0 | 0.0 | 108 |
| 644 | 45.0 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 645 | 47.7 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 646 | 47.7 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 647 | 97.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 648 | 120.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 649 | 50.4 | 4.30 | 3.46 | 3.61 | 3.09 | 2.30 | 108 |
| 650 | 49.1 | 3.50 | 3.16 | 2.80 | 0.0 | 0.0 | 138 |
| 651 | 49.3 | 4.90 | 4.00 | 3.79 | 3.39 | 1.14 | 108 |
| 652 | 105.3 | 5.70 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 653 | 43.2 | 5.20 | 4.11 | 4.18 | 0.0 | 0.45 | 108 |
| 654 | 45.6 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 655 | 48.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 656 | 99.8 | 4.80 | 3.47 | 3.00 | 3.00 | 2.55 | 168 |
| 657 | 97.5 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 658 | 99.8 | *4.50 | 0.0 | 0.0 | 3.39 | 0.0 | 138 |
| 659 | 123.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 660 | 46.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 661 | 45.5 | 5.20 | 4.31 | 4.20 | 0.0 | 0.0 | 108 |
| 662 | 98.8 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 508 |
| 663 | 73.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 664 | 45.6 | 3.70 | 0.0 | 2.89 | 0.0 | 0.0 | 158 |
| 665 | 119.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 328 |
| 666 | 45.7 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 667 | 44.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 668 | 44.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 508 |
| 669 | 51.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 670 | 61.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 671 | 47.5 | 3.60 | 3.68 | 3.13 | 2.78 | 0.0 | 108 |
| 672 | 93.2 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |

KIP 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LR RATIO | COMMENT |
|-----------|--------------------|-------|---------------|---------------|---------------|----------------|---------|
| 673 | 87.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 238 |
| 674 | 120.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 675 | 90.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 238 |
| 676 | 91.6 | 4.80 | 4.47 | 3.93 | 3.64 | 0.0 | 108 |
| 677 | 106.8 | 3.60 | 3.39 | 3.21 | 0.0 | 0.78 | 168 |
| 678 | 45.0 | 4.20 | 4.66 | 4.26 | 3.73 | 0.0 | 108 |
| 679 | 82.8 | 6.30 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 680 | 110.2 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 681 | 46.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 168 |
| 682 | 120.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 683 | 125.4 | 4.40 | 3.86 | 3.56 | 3.45 | 0.0 | 108 |
| 684 | 122.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 685 | 100.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 686 | 114.4 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 687 | 88.9 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 238 |
| 688 | 89.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 328 |
| 689 | 89.0 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 690 | 89.1 | 5.50 | 4.31 | 4.23 | 0.0 | 0.65 | 108 |
| 691 | 44.9 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 691 | 88.7 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 692 | 82.7 | 5.50 | 0.0 | 4.37 | 0.0 | 0.0 | 138 |
| 693 | 77.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 258 |
| 694 | 44.4 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 696 | 107.7 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 697 | 54.2 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 508 |
| 698 | 50.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 508 |
| 699 | 92.8 | 6.20 | 3.61 | 3.67 | 3.26 | 0.0 | 108 |
| 700 | 102.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 701 | 120.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 508 |
| 702 | 107.8 | 5.50 | 5.31 | 4.82 | 4.47 | 0.0 | 108 |
| 703 | 105.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 704 | 123.4 | 5.20 | 5.10 | 5.16 | 0.0 | 0.0 | 108 |
| 705 | 105.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 706 | 123.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 707 | 123.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 708 | 99.3 | *4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 709 | 105.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 238 |
| 710 | 49.6 | 4.30 | 3.74 | 3.62 | 2.90 | 0.45 | 108 |
| 711 | 74.3 | *5.30 | 4.25 | 4.11 | 3.73 | 1.11 | 108 |
| 712 | 104.4 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 713 | 45.1 | 4.50 | 3.63 | 3.02 | 0.0 | 0.0 | 138 |
| 714 | 123.6 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 715 | 48.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 716 | 73.1 | 5.50 | 5.02 | 4.64 | 0.0 | 0.60 | 108 |
| 717 | 120.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 508 |
| 718 | 118.0 | 4.70 | 4.08 | 3.99 | 3.57 | 0.0 | 138 |
| 719 | 118.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 720 | 47.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 721 | 62.6 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 328 |

KIP C6/C1/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MP | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 722 | 99.4 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 208 |
| 723 | 45.2 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 724 | 49.2 | 3.70 | C.C | C.C | 0.0 | 0.0 | 238 |
| 725 | 133.9 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 208 |
| 726 | 72.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 727 | 121.4 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 308 |
| 728 | 126.1 | 4.50 | C.C | 0.0 | 0.0 | 0.0 | 208 |
| 729 | 104.4 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 308 |
| 730 | 123.5 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 308 |
| 731 | 120.0 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 238 |
| 732 | 94.9 | 4.40 | 3.50 | 3.39 | 3.19 | 0.0 | 108 |
| 733 | 123.5 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 238 |
| 734 | 92.4 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 308 |
| 735 | 46.8 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 208 |
| 736 | 49.3 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 508 |
| 737 | 44.7 | 4.60 | 3.86 | 3.43 | 2.98 | 0.91 | 108 |
| 738 | 49.4 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 308 |
| 739 | 45.9 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 308 |
| 741 | 119.2 | *4.80 | C.C | 0.0 | 0.0 | 0.0 | 308 |
| 742 | 120.6 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 308 |
| 743 | 94.0 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 308 |
| 744 | 73.2 | 5.70 | 5.47 | 5.18 | 0.0 | 1.19 | 108 |
| 745 | 73.9 | 4.40 | C.C | 0.0 | 0.0 | 0.0 | 308 |
| 746 | 93.4 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 208 |
| 747 | 123.8 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 308 |
| 748 | 104.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 749 | 102.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 750 | 102.3 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 751 | 119.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 752 | 118.5 | 5.40 | 3.77 | 3.63 | 0.0 | 0.0 | 108 |
| 753 | 101.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 358 |
| 754 | 120.2 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 208 |
| 755 | 99.0 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |
| 756 | 45.2 | 3.40 | C.C | 0.0 | 0.0 | 0.0 | 258 |
| 757 | 90.2 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 758 | 66.1 | 5.10 | C.C | 0.0 | 0.0 | 0.0 | 308 |
| 759 | 120.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 238 |
| 760 | 121.5 | 5.60 | C.C | 0.0 | 0.0 | 0.0 | 238 |
| 761 | 45.2 | 5.20 | 3.86 | 3.79 | 3.46 | 0.0 | 108 |
| 762 | 115.1 | 4.90 | C.C | 0.0 | 0.0 | 0.0 | 508 |
| 763 | 98.0 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 208 |
| 764 | 44.4 | 4.70 | 3.77 | 3.62 | 3.24 | 1.14 | 108 |
| 765 | 124.5 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 766 | 45.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 767 | 126.2 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 208 |
| 768 | 105.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 238 |
| 769 | 105.6 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 508 |
| 770 | 60.8 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 208 |
| 771 | 114.0 | *4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 308 |

KIP C6/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 772 | 44.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 773 | 84.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 774 | 121.9 | 4.70 | 2.86 | 0.0 | 0.0 | 0.0 | 20R |
| 775 | 113.8 | 5.40 | 4.52 | 4.79 | 0.0 | 0.73 | 10R |
| 776 | 44.8 | 4.80 | 3.75 | 3.73 | 3.11 | 0.0 | 10R |
| 777 | 54.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 778 | 123.0 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 779 | 54.7 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 780 | 52.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 781 | 101.4 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 782 | 52.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 783 | 45.0 | 4.40 | 3.59 | 3.17 | 0.0 | 0.0 | 13R |
| 784 | 49.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 785 | 62.8 | 5.30 | 4.43 | 4.13 | 0.0 | 0.0 | 10R |
| 786 | 123.2 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 787 | 54.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 50R |
| 788 | 106.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 789 | 54.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 790 | 54.9 | 4.70 | 3.90 | 3.43 | 0.0 | 1.25 | 10R |
| 791 | 70.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 792 | 145.8 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 10R |
| 793 | 106.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 794 | 73.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 795 | 45.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 796 | 41.0 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 797 | 93.2 | 5.70 | 4.11 | 3.88 | 3.23 | 0.52 | 10R |
| 799 | 48.8 | 6.00 | 5.77 | 5.70 | 0.0 | 0.86 | 10R |
| 800 | 47.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 801 | 48.9 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 802 | 48.9 | 4.80 | 4.74 | 4.60 | 4.30 | 0.90 | 10R |
| 803 | 49.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 804 | 48.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 805 | 120.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 806 | 47.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 807 | 48.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 808 | 49.8 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 809 | 47.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 810 | 47.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 811 | 46.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 812 | 48.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 813 | 48.9 | 4.80 | 4.31 | 4.07 | 0.0 | 0.36 | 10R |
| 814 | 49.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 815 | 45.0 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 816 | 119.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 817 | 53.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 818 | 47.5 | 5.70 | 4.77 | 4.66 | 0.0 | 2.89 | 10R |
| 819 | 108.8 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 820 | 116.9 | *4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 821 | 47.9 | 4.60 | 3.20 | 3.25 | 2.88 | 0.0 | 16R |

KIP 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 822 | 48.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 823 | 120.4 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 824 | 49.6 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 825 | 48.8 | 4.70 | 4.42 | 4.18 | 3.77 | 0.0 | 10R |
| 827 | 70.6 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 828 | 48.9 | 5.70 | 5.81 | 5.75 | 0.0 | 0.53 | 10R |
| 829 | 48.9 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 830 | 48.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 831 | 48.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 832 | 48.9 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 833 | 49.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 834 | 48.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 835 | 49.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 836 | 48.9 | 4.60 | 3.42 | 3.69 | 0.0 | 0.70 | 10R |
| 837 | 48.8 | 4.90 | 3.93 | 3.93 | 0.0 | 0.95 | 10R |
| 838 | 106.0 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 839 | 69.4 | 4.00 | 3.57 | 3.27 | 3.10 | 0.92 | 10R |
| 840 | 48.1 | 3.80 | 3.99 | 0.0 | 0.0 | 0.0 | 10R |
| 841 | 47.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 842 | 124.1 | 4.70 | 0.0 | 3.73 | 3.30 | 0.0 | 10R |
| 843 | 43.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 844 | 122.8 | 4.60 | 4.01 | 3.70 | 0.0 | 0.0 | 10R |
| 845 | 112.1 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 846 | 44.1 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 847 | 108.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 848 | 44.4 | 4.20 | 3.07 | 0.0 | 0.0 | 0.0 | 20R |
| 849 | 116.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 850 | 44.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 851 | 43.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 852 | 45.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 26R |
| 853 | 96.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 854 | 97.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 855 | 106.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 856 | 117.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 857 | 43.5 | 4.80 | 3.68 | 3.59 | 3.19 | 0.16 | 10R |
| 858 | 48.7 | 4.70 | 3.62 | 3.52 | 3.26 | 0.0 | 10R |
| 859 | 45.2 | 5.70 | 5.23 | 5.30 | 4.84 | 0.54 | 10R |
| 860 | 43.9 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 861 | 116.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 862 | 122.0 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 863 | 119.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 864 | 47.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 865 | 93.1 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 866 | 117.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 867 | 45.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 868 | 45.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 30R |
| 869 | 40.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |
| 870 | 100.6 | 4.10 | 4.27 | 3.72 | 0.0 | 0.0 | 10R |
| 871 | 48.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20R |

KIP C6/C1/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LP RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 872 | 121.1 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 873 | 96.7 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 874 | 118.1 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 20P |
| 875 | 96.7 | 4.90 | 4.18 | 3.80 | 3.60 | 1.58 | 10P |

APPENDIX II-J
BASIC DATA FOR ALQ

ALQ C6/C1/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 310 | 70.4 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 509 |
| 311 | 93.0 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 509 |
| 312 | 96.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 313 | 93.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 314 | 61.8 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 509 |
| 315 | 112.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 316 | 70.5 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 509 |
| 317 | 102.7 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 509 |
| 318 | 102.7 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 509 |
| 319 | 101.8 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 320 | 102.9 | 3.50 | C.0 | 0.0 | 0.0 | 0.0 | 509 |
| 321 | 107.0 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 509 |
| 323 | 103.6 | *5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 324 | 113.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 539 |
| 326 | 65.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 327 | 59.7 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 328 | 61.6 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 329 | 104.2 | 4.10 | C.0 | 0.0 | 0.0 | 0.0 | 509 |
| 330 | 108.6 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 331 | 61.8 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 332 | 92.7 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 333 | 106.4 | 3.90 | C.0 | 0.0 | 0.0 | 0.0 | 509 |
| 334 | 115.2 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 335 | 58.0 | 4.00 | 3.21 | 3.03 | 2.78 | 0.46 | 109 |
| 336 | 76.1 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 337 | 69.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 338 | 61.6 | 4.70 | C.C | 0.0 | 0.0 | 0.0 | 509 |
| 339 | 95.2 | 5.50 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 340 | 60.4 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 309 |
| 341 | 108.6 | 5.40 | 4.37 | 4.27 | 4.05 | 1.16 | 109 |
| 342 | 106.4 | 4.90 | C.0 | 0.0 | 0.0 | 0.0 | 209 |
| 343 | 108.7 | 4.50 | 3.61 | 3.36 | 0.0 | 0.58 | 109 |
| 344 | 99.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 345 | 122.7 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 346 | 108.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 347 | 98.2 | 4.50 | C.C | 0.0 | 0.0 | 0.0 | 309 |
| 348 | 113.2 | 4.70 | C.C | 0.0 | 0.0 | 0.0 | 209 |
| 349 | 71.5 | 4.40 | C.C | 0.0 | 0.0 | 0.0 | 309 |
| 350 | 97.6 | 4.90 | 3.87 | 3.58 | 2.91 | 4.60 | 109 |
| 351 | 43.8 | 4.90 | 4.31 | 4.01 | 0.0 | 0.0 | 109 |
| 381 | 75.4 | 4.60 | C.C | 0.0 | 0.0 | 0.0 | 309 |
| 383 | 70.4 | 3.90 | C.0 | 0.0 | 0.0 | 0.0 | 509 |
| 384 | 105.1 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 509 |
| 385 | 96.3 | 4.40 | C.0 | 0.0 | 0.0 | 0.0 | 509 |
| 386 | 59.5 | 5.00 | 3.73 | 3.67 | 3.41 | 0.0 | 109 |
| 388 | 74.2 | 4.50 | C.0 | 0.0 | 0.0 | 0.0 | 509 |
| 389 | 68.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 390 | 112.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 391 | 79.6 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 509 |

ALQ 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MP | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 392 | 113.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 393 | 64.2 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 510 |
| 394 | 64.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 395 | 117.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 396 | 63.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 397 | 102.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 398 | 84.1 | *3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 399 | 69.9 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 402 | 107.5 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 403 | 108.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 404 | 114.4 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 405 | 86.0 | *4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 407 | 108.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 408 | 106.1 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 409 | 85.2 | *3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 410 | 108.7 | 4.70 | 3.67 | 3.50 | 3.09 | 0.0 | 109 |
| 411 | 64.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 453 | 111.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 454 | 93.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 455 | 112.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 470 | 100.5 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 471 | 108.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 472 | 70.0 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 473 | 62.3 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 474 | 111.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 475 | 104.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 476 | 69.0 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 477 | 112.1 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 478 | 59.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 479 | 93.3 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 482 | 74.9 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 483 | 116.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 484 | 84.1 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 485 | 106.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 486 | 98.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 487 | 111.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 488 | 111.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 489 | 111.7 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 490 | 94.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 491 | 102.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 492 | 103.0 | 5.10 | 3.01 | 2.82 | 0.0 | 0.0 | 509 |
| 493 | 72.1 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 494 | 66.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 495 | 74.4 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 496 | 109.4 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 497 | 101.6 | 4.90 | 4.06 | 3.77 | 3.35 | 0.0 | 109 |
| 498 | 109.3 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 499 | 105.9 | 4.60 | 3.04 | 2.73 | 0.0 | 0.0 | 509 |
| 500 | 74.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |

ALQ 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 501 | 62.6 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 502 | 112.8 | 3.90 | 3.08 | 2.67 | 0.0 | 0.0 | 509 |
| 503 | 66.7 | 4.20 | C.0 | 0.0 | 0.0 | 0.0 | 509 |
| 504 | 99.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 505 | 64.1 | 5.30 | 3.31 | 3.04 | 2.56 | 2.87 | 109 |
| 506 | 62.1 | 3.30 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 507 | 95.1 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 508 | 76.1 | 4.10 | C.0 | 0.0 | 0.0 | 0.0 | 209 |
| 509 | 64.1 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 510 | 106.0 | 4.00 | C.0 | 0.0 | 0.0 | 0.0 | 209 |
| 511 | 93.8 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 209 |
| 512 | 90.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 513 | 75.5 | 5.00 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 514 | 64.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 515 | 65.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 516 | 107.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 517 | 114.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 518 | 107.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 538 | 112.9 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 209 |
| 539 | 68.6 | 4.80 | 3.18 | 3.06 | 2.77 | 0.0 | 109 |
| 540 | 92.4 | 4.40 | C.0 | 0.0 | 0.0 | 0.0 | 509 |
| 541 | 68.6 | 5.10 | 3.81 | 3.75 | 3.28 | 0.0 | 109 |
| 542 | 104.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 543 | 107.9 | 4.90 | 2.99 | 2.69 | 2.67 | 0.0 | 509 |
| 544 | 110.1 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 545 | 92.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 546 | 61.9 | 4.80 | C.0 | 0.0 | 0.0 | 0.0 | 209 |
| 547 | 105.8 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 548 | 111.0 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 550 | 109.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 551 | 101.7 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 509 |
| 552 | 106.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 553 | 109.0 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 309 |
| 554 | 101.3 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 555 | 96.2 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 359 |
| 556 | 77.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 557 | 115.0 | 4.70 | C.0 | 0.0 | 0.0 | 0.0 | 309 |
| 558 | 61.8 | 5.60 | 4.29 | 4.02 | 0.0 | 0.0 | 109 |
| 559 | 61.8 | 5.00 | 4.62 | 4.01 | 0.0 | 0.0 | 139 |
| 560 | 115.1 | 4.20 | 0.0 | 3.10 | 0.0 | 0.0 | 159 |
| 561 | 97.0 | 4.30 | 2.70 | 2.48 | 2.56 | 0.0 | 179 |
| 563 | 62.5 | 4.00 | C.0 | 0.0 | 0.0 | 0.0 | 209 |
| 564 | 95.8 | 3.90 | C.0 | 0.0 | 0.0 | 0.0 | 309 |
| 565 | 60.6 | 5.30 | 3.96 | 3.40 | 0.0 | 0.0 | 109 |
| 566 | 98.1 | 4.50 | C.0 | 0.0 | 0.0 | 0.0 | 509 |
| 567 | 115.0 | 4.80 | C.0 | 0.0 | 0.0 | 0.0 | 209 |
| 568 | 95.7 | 4.00 | C.0 | 0.0 | 0.0 | 0.0 | 209 |
| 569 | 72.7 | 4.00 | C.0 | 0.0 | 0.0 | 0.0 | 209 |
| 570 | 98.0 | 4.30 | C.0 | 0.0 | 0.0 | 0.0 | 509 |

ALO 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 571 | 115.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 572 | 69.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 573 | 68.6 | 5.70 | 0.0 | 0.0 | 0.0 | 0.0 | 409 |
| 574 | 68.7 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 575 | 68.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 576 | 113.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 577 | 68.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 578 | 68.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 579 | 68.7 | 4.90 | 4.10 | 4.11 | 3.69 | 0.0 | 109 |
| 580 | 68.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 581 | 69.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 592 | 97.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 593 | 60.3 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 696 | 106.2 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 697 | 86.2 | 4.40 | 4.76 | 4.30 | 0.0 | 0.0 | 109 |
| 698 | 77.5 | 4.80 | 0.0 | 3.62 | 3.25 | 0.0 | 109 |
| 699 | 95.0 | 6.20 | 3.89 | 3.33 | 0.0 | 0.86 | 109 |
| 700 | 105.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 701 | 111.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 702 | 110.0 | 5.50 | 5.33 | 5.14 | 4.41 | 0.0 | 109 |
| 703 | 109.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 705 | 108.1 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 706 | 101.4 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 239 |
| 707 | 97.0 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 708 | 116.4 | *4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 709 | 106.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 239 |
| 710 | 76.1 | 4.30 | 3.79 | 2.93 | 0.0 | 3.18 | 139 |
| 711 | 107.0 | *5.30 | 0.0 | 0.0 | 0.0 | 0.0 | 139 |
| 712 | 108.1 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 713 | 64.6 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 714 | 96.6 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 715 | 72.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 716 | 105.6 | 5.50 | 4.20 | 4.34 | 3.84 | 2.44 | 109 |
| 717 | 92.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 239 |
| 718 | 113.1 | 4.70 | 0.0 | 3.65 | 0.0 | 0.0 | 139 |
| 719 | 94.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 720 | 69.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 721 | 81.8 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 329 |
| 722 | 104.0 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 723 | 62.6 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 724 | 74.6 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 239 |
| 725 | 127.0 | 2.90 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 726 | 106.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 727 | 113.2 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 728 | 100.4 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 729 | 108.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 730 | 96.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 731 | 106.4 | 2.90 | 0.0 | 0.0 | 0.0 | 0.0 | 239 |
| 732 | 117.3 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |

ALQ C6/C1/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LC/LP RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 733 | 96.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 239 |
| 734 | 121.2 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 735 | 73.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 736 | 75.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 737 | 64.7 | 4.60 | 3.50 | 3.45 | 0.0 | 0.91 | 109 |
| 738 | 75.4 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 741 | 91.6 | *4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 742 | 110.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 743 | 101.5 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 744 | 105.7 | 5.70 | 5.00 | 4.70 | 0.0 | 6.86 | 109 |
| 745 | 106.6 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 746 | 86.4 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 239 |
| 747 | 99.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 748 | 108.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 239 |
| 749 | 108.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 750 | 109.1 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 751 | 92.4 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 752 | 91.0 | 5.40 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 753 | 90.1 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 359 |
| 754 | 111.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 755 | 92.9 | 5.20 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 756 | 65.6 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 757 | 109.6 | 2.90 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 758 | 79.5 | 5.10 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 759 | 92.7 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 760 | 113.9 | 5.60 | 0.0 | 0.0 | 0.0 | 0.0 | 239 |
| 761 | 65.8 | 5.20 | 3.72 | 3.69 | 0.0 | 0.0 | 109 |
| 762 | 84.7 | 4.90 | 4.48 | 3.61 | 0.0 | 12.81 | 109 |
| 763 | 91.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 239 |
| 764 | 63.9 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 766 | 62.6 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 509 |
| 767 | 99.6 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 409 |
| 771 | 83.7 | *4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 409 |
| 772 | 64.4 | 2.90 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 773 | 15.4 | 2.90 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 774 | 112.9 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 775 | 108.2 | 5.40 | 5.27 | 4.73 | 5.03 | 1.97 | 109 |
| 776 | 62.9 | 4.80 | 3.38 | 3.29 | 0.0 | 1.09 | 109 |
| 777 | 86.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 778 | 97.4 | 5.10 | 4.45 | 4.21 | 3.63 | 1.77 | 109 |
| 779 | 87.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 780 | 77.2 | 2.90 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 781 | 105.6 | 5.00 | 4.18 | 3.96 | 3.48 | 0.0 | 109 |
| 782 | 76.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 783 | 64.1 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 784 | 75.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 785 | 93.8 | 5.30 | 0.0 | 0.0 | 0.0 | 0.0 | 009 |
| 786 | 97.6 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 787 | 87.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |

ALQ 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LO/LR RATIO | COMMENT |
|-----------|--------------------|-------|---------------|---------------|---------------|----------------|---------|
| 788 | 110.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 789 | 87.0 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 300 |
| 790 | 87.2 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 009 |
| 791 | 92.5 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 300 |
| 792 | 105.2 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 300 |
| 793 | 107.9 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 794 | 105.9 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 300 |
| 795 | 67.7 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 000 |
| 796 | 59.4 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 000 |
| 797 | 95.2 | 5.70 | 4.29 | 3.68 | 0.0 | 0.0 | 100 |
| 799 | 74.8 | 6.00 | 5.64 | 5.19 | 0.0 | 0.02 | 100 |
| 800 | 73.8 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 801 | 75.5 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 802 | 75.0 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 300 |
| 803 | 75.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 804 | 74.9 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 805 | 92.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 300 |
| 806 | 73.2 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 300 |
| 807 | 74.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 808 | 75.5 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 300 |
| 809 | 73.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 300 |
| 810 | 73.2 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 811 | 73.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 812 | 74.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 813 | 75.0 | 4.80 | 3.84 | 3.41 | 0.0 | 0.0 | 100 |
| 814 | 75.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 300 |
| 815 | 64.7 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 816 | 92.1 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 817 | 77.1 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 818 | 74.3 | 5.70 | 4.30 | 3.65 | 0.0 | 1.31 | 100 |
| 819 | 110.9 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 820 | 91.0 | *4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 300 |
| 821 | 73.2 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 822 | 74.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 823 | 91.7 | *4.30 | 3.94 | 3.42 | 0.0 | 4.85 | 100 |
| 824 | 76.1 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 825 | 75.0 | 4.70 | 3.88 | 3.65 | 0.0 | 0.50 | 100 |
| 826 | 57.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 827 | 59.4 | 4.40 | 4.05 | 3.82 | 0.0 | 0.0 | 100 |
| 828 | 75.0 | 5.70 | 5.77 | 5.25 | 0.0 | 0.89 | 100 |
| 829 | 75.0 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 300 |
| 830 | 73.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 230 |
| 831 | 74.4 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 832 | 75.0 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 833 | 75.0 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 834 | 74.9 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 230 |
| 835 | 76.1 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 836 | 75.0 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 200 |
| 837 | 75.0 | 4.50 | 3.74 | 3.04 | 0.0 | 0.0 | 100 |

ALQ 06/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 838 | 106.9 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 839 | 57.8 | 4.00 | 4.11 | 3.80 | 3.37 | 0.53 | 109 |
| 840 | 75.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 841 | 73.2 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 842 | 97.8 | 4.70 | 4.10 | 3.69 | 0.0 | 0.0 | 109 |
| 843 | 66.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 844 | 97.7 | 4.60 | 4.37 | 3.82 | 3.39 | 0.65 | 109 |
| 845 | 113.8 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 846 | 66.6 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 847 | 113.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 848 | 63.2 | 4.20 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 849 | 86.3 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 850 | 61.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 851 | 61.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 852 | 68.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 853 | 117.9 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 854 | 108.3 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 855 | 110.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 856 | 93.4 | 2.70 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 857 | 63.1 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 858 | 74.2 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 859 | 65.1 | 5.70 | 0.0 | 5.07 | 4.61 | 0.54 | 109 |
| 860 | 63.6 | 3.50 | 0.0 | 3.63 | 0.0 | 0.0 | 169 |
| 862 | 113.7 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 863 | 93.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 864 | 73.2 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 865 | 95.0 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 866 | 90.0 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 867 | 68.2 | 4.10 | 3.39 | 2.93 | 0.0 | 0.0 | 109 |
| 868 | 61.9 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |
| 869 | 59.5 | 4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 870 | 114.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 871 | 75.5 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 872 | 108.9 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 873 | 110.1 | 4.50 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 874 | 92.8 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 209 |
| 875 | 110.2 | 4.90 | 0.0 | 0.0 | 0.0 | 0.0 | 309 |

APPENDIX II-K
BASIC DATA FOR ZLP

ZLP 12/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LP RATIC | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 739 | 134.0 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 742 | 123.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 3010 |
| 743 | 144.4 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 3010 |
| 744 | 168.3 | 5.70 | 0.0 | 4.94 | 4.53 | 0.0 | 1010 |
| 745 | 169.2 | 4.40 | C.C | 0.0 | 0.0 | 0.0 | 3010 |
| 746 | 125.0 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 747 | 106.0 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 3010 |
| 748 | 140.1 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 5010 |
| 749 | 142.3 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 750 | 143.8 | 4.90 | C.C | 0.0 | 0.0 | 0.0 | 3010 |
| 751 | 100.6 | 4.30 | 0.0 | 3.41 | 2.07 | 0.0 | 1310 |
| 752 | 100.3 | 5.40 | C.C | 0.0 | 0.0 | 0.0 | 3010 |
| 753 | 120.6 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 5010 |
| 755 | 128.5 | 5.20 | C.C | 0.0 | 0.0 | 0.0 | 5010 |
| 763 | 126.9 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 764 | 126.9 | 4.70 | 0.0 | 3.67 | 0.0 | 0.50 | 1610 |
| 765 | 104.0 | 4.80 | 3.66 | 3.58 | 0.0 | 0.0 | 1310 |
| 767 | 102.5 | 4.40 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 768 | 139.7 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 2310 |
| 769 | 139.7 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 2310 |
| 770 | 120.2 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 2310 |
| 771 | 95.2 | *4.40 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 772 | 127.4 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 5010 |
| 773 | 95.0 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 5010 |
| 774 | 124.0 | 4.70 | C.C | 0.0 | 0.0 | 0.0 | 5010 |
| 775 | 128.6 | 5.40 | 5.39 | 4.80 | 5.21 | 0.80 | 1010 |
| 776 | 125.9 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 777 | 148.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 778 | 103.6 | 5.10 | C.C | 4.16 | 0.0 | 1.58 | 1010 |
| 779 | 148.9 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 780 | 140.2 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 5010 |
| 781 | 140.8 | 5.00 | C.C | 0.0 | 0.0 | 0.0 | 5010 |
| 782 | 139.6 | 4.00 | C.C | 0.0 | 0.0 | 0.0 | 5010 |
| 783 | 127.1 | 4.40 | C.C | 0.0 | 0.0 | 0.0 | 5010 |
| 784 | 138.5 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 5010 |
| 785 | 156.5 | 5.30 | C.C | 0.0 | 0.0 | 0.0 | 0010 |
| 786 | 103.7 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 787 | 149.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 788 | 140.0 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 789 | 148.9 | 4.20 | C.C | 0.0 | 0.0 | 0.0 | 3010 |
| 790 | 149.0 | 4.70 | C.C | 0.0 | 0.0 | 0.0 | 0010 |
| 791 | 153.8 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 3010 |
| 792 | 82.9 | 4.50 | C.C | 0.0 | 0.0 | 0.0 | 3010 |
| 793 | 137.1 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 794 | 168.6 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 3010 |
| 795 | 130.7 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 0010 |
| 796 | 122.4 | 3.50 | C.C | 0.0 | 0.0 | 0.0 | 0010 |
| 797 | 137.0 | 5.70 | 4.10 | 3.65 | 0.0 | 0.0 | 1010 |
| 799 | 137.7 | 6.00 | 5.83 | 5.63 | 5.24 | 0.97 | 1010 |

ZLP 12/01/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|-------|---------------|---------------|---------------|----------------|---------|
| 800 | 136.6 | 4.20 | C.0 | 0.0 | 0.0 | 0.0 | 3010 |
| 801 | 138.3 | 3.50 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 802 | 137.8 | 4.80 | 4.79 | 4.11 | 3.97 | 0.51 | 1010 |
| 803 | 138.5 | 3.60 | 0.0 | 0.0 | 0.0 | 0.0 | 3010 |
| 804 | 137.7 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 3010 |
| 805 | 100.2 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 3010 |
| 806 | 136.1 | 4.30 | C.0 | 0.0 | 0.0 | 0.0 | 3010 |
| 807 | 137.8 | 4.30 | C.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 808 | 138.5 | 3.90 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 809 | 136.1 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 3010 |
| 810 | 136.1 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 3010 |
| 811 | 135.8 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 812 | 137.8 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 3010 |
| 813 | 137.8 | 4.80 | C.C | 0.0 | 0.0 | 0.0 | 5010 |
| 814 | 137.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 3010 |
| 815 | 127.7 | 4.70 | C.C | 0.0 | 0.0 | 0.0 | 3010 |
| 816 | 100.3 | 3.90 | C.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 817 | 140.1 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 818 | 137.0 | 5.70 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 819 | 137.9 | 3.60 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 820 | 102.4 | *4.20 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 821 | 136.1 | 4.60 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 822 | 137.2 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 823 | 98.8 | *4.30 | 0.0 | 0.0 | 0.0 | 0.0 | 5010 |
| 824 | 139.0 | 3.40 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 825 | 137.8 | 4.70 | 4.12 | 3.91 | 3.34 | 0.68 | 1010 |
| 826 | 103.7 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 827 | 110.4 | 4.40 | C.C | 0.0 | 0.0 | 0.0 | 5010 |
| 828 | 137.9 | 5.70 | 5.77 | 5.64 | 5.01 | 0.46 | 1010 |
| 829 | 137.8 | 4.80 | 0.0 | 0.0 | 0.0 | 0.0 | 3010 |
| 830 | 136.7 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 831 | 137.2 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 832 | 137.8 | 4.70 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 833 | 137.8 | 4.10 | C.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 834 | 137.8 | 4.80 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 835 | 139.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 836 | 137.8 | 4.60 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 837 | 137.8 | 4.90 | 4.05 | 3.42 | 0.0 | 0.0 | 1010 |
| 838 | 136.8 | 3.40 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 839 | 109.4 | 4.00 | 3.74 | 3.59 | 3.26 | 1.60 | 1010 |
| 840 | 136.2 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 3010 |
| 841 | 136.1 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 842 | 102.7 | 4.70 | 3.83 | 3.58 | 3.29 | 0.0 | 1010 |
| 843 | 129.4 | 3.80 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 844 | 104.2 | 4.60 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 845 | 136.8 | 4.30 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 846 | 129.6 | 4.10 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 847 | 140.8 | 3.70 | C.C | 0.0 | 0.0 | 0.0 | 2010 |
| 848 | 126.2 | 4.20 | C.C | 0.0 | 0.0 | 0.0 | 2010 |

7LP 12/01/72 - 12/31/72

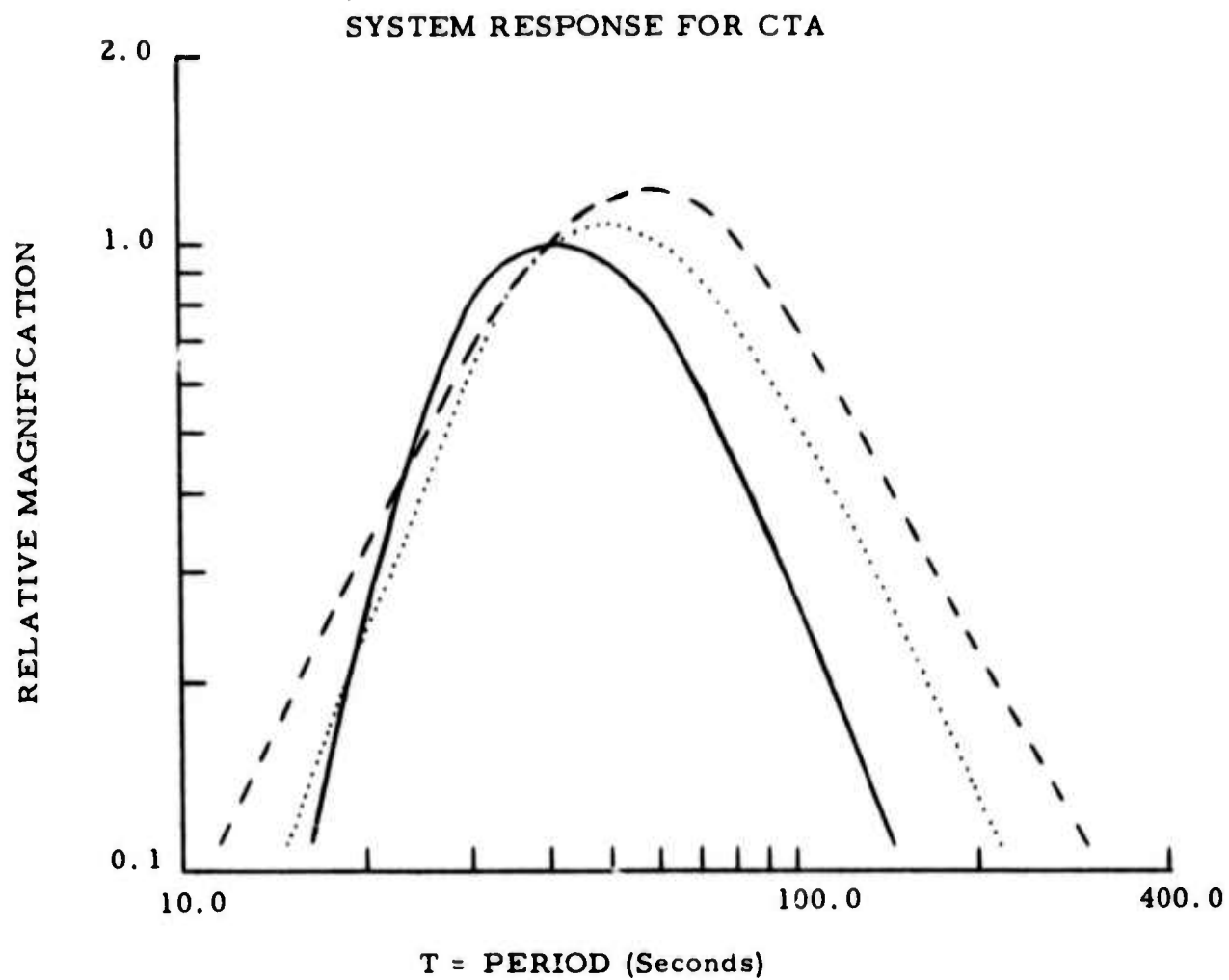
| EVENT NO. | DISTANCE (DEGREES) | MB | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/LR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 849 | 96.0 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 850 | 124.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 851 | 124.8 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 852 | 131.7 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 853 | 161.7 | 3.90 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 854 | 149.2 | 3.80 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 855 | 140.0 | 4.00 | 0.0 | 0.0 | 0.0 | 0.0 | 2010 |
| 856 | 104.8 | 3.70 | 0.0 | 0.0 | 0.0 | 0.0 | 5010 |

APPENDIX II- L
BASIC DATA FOR MAT

MAT 12/22/72 - 12/31/72

| EVENT NO. | DISTANCE (DEGREES) | MR | MS T=20SEC | MS T=30SEC | MS T=40SEC | LQ/IR RATIO | COMMENT |
|--------------|-----------------------|------|---------------|---------------|---------------|----------------|---------|
| 852 | 18.0 | 4.10 | C.0 | 0.0 | 0.0 | 0.0 | 2011 |
| 853 | 39.8 | 3.90 | C.0 | 0.0 | 0.0 | 0.0 | 5011 |
| 854 | 42.3 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 2011 |
| 855 | 52.6 | 4.00 | C.0 | 0.0 | 0.0 | 0.0 | 3011 |
| 856 | 80.2 | 3.70 | C.0 | 0.0 | 0.0 | 0.0 | 5011 |
| 857 | 23.9 | 4.80 | C.0 | 3.32 | 0.0 | 0.0 | 1011 |
| 858 | 12.5 | 4.70 | 3.35 | 5.12 | 0.0 | 0.0 | 1011 |
| 859 | 22.1 | 5.70 | 5.31 | 5.25 | 0.0 | 0.72 | 1011 |
| 860 | 23.4 | 3.50 | C.0 | 0.0 | 0.0 | 0.0 | 2011 |
| 861 | 61.4 | 3.60 | C.0 | 0.0 | 0.0 | 0.0 | 2011 |
| 862 | 70.7 | 4.60 | C.0 | 0.0 | 0.0 | 0.0 | 2011 |
| 863 | 82.6 | 3.60 | C.0 | 0.0 | 0.0 | 0.0 | 2011 |
| 864 | 13.5 | 4.00 | C.0 | 0.0 | 0.0 | 0.0 | 3011 |
| 865 | 44.5 | 4.50 | C.0 | 0.0 | 0.0 | 0.0 | 2011 |
| 866 | 83.8 | 3.50 | C.0 | 0.0 | 0.0 | 0.0 | 3011 |
| 867 | 18.5 | 4.10 | 3.55 | 0.0 | 0.0 | 0.0 | 1011 |
| 868 | 25.6 | 4.30 | C.0 | 0.0 | 0.0 | 0.0 | 5011 |
| 869 | 27.4 | 4.30 | C.0 | 0.0 | 0.0 | 0.0 | 2011 |
| 870 | 44.4 | 4.10 | 0.0 | 0.0 | 0.0 | 0.0 | 2011 |
| 871 | 11.1 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 5011 |
| 872 | 71.8 | 3.80 | C.0 | 0.0 | 0.0 | 0.0 | 5011 |
| 873 | 41.0 | 4.50 | 3.71 | 0.0 | 0.0 | 0.0 | 1011 |
| 874 | 81.2 | 4.40 | C.0 | 0.0 | 0.0 | 0.0 | 2011 |
| 875 | 41.0 | 4.90 | 3.55 | 3.36 | 3.12 | 0.0 | 1011 |

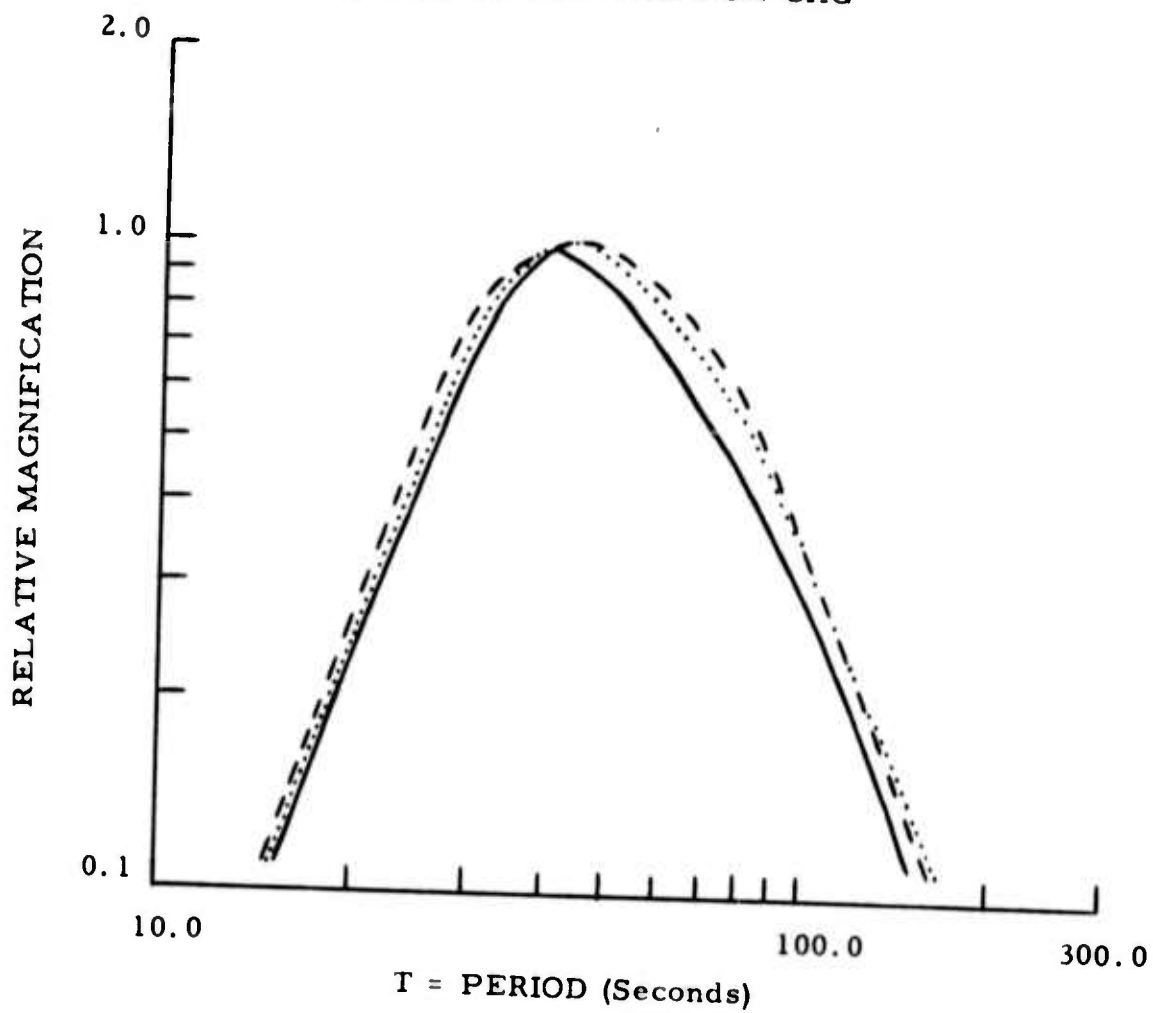
APPENDIX II-M
VLPE SYSTEM RESPONSE CURVES



Gain at T = 40.0 Sec.

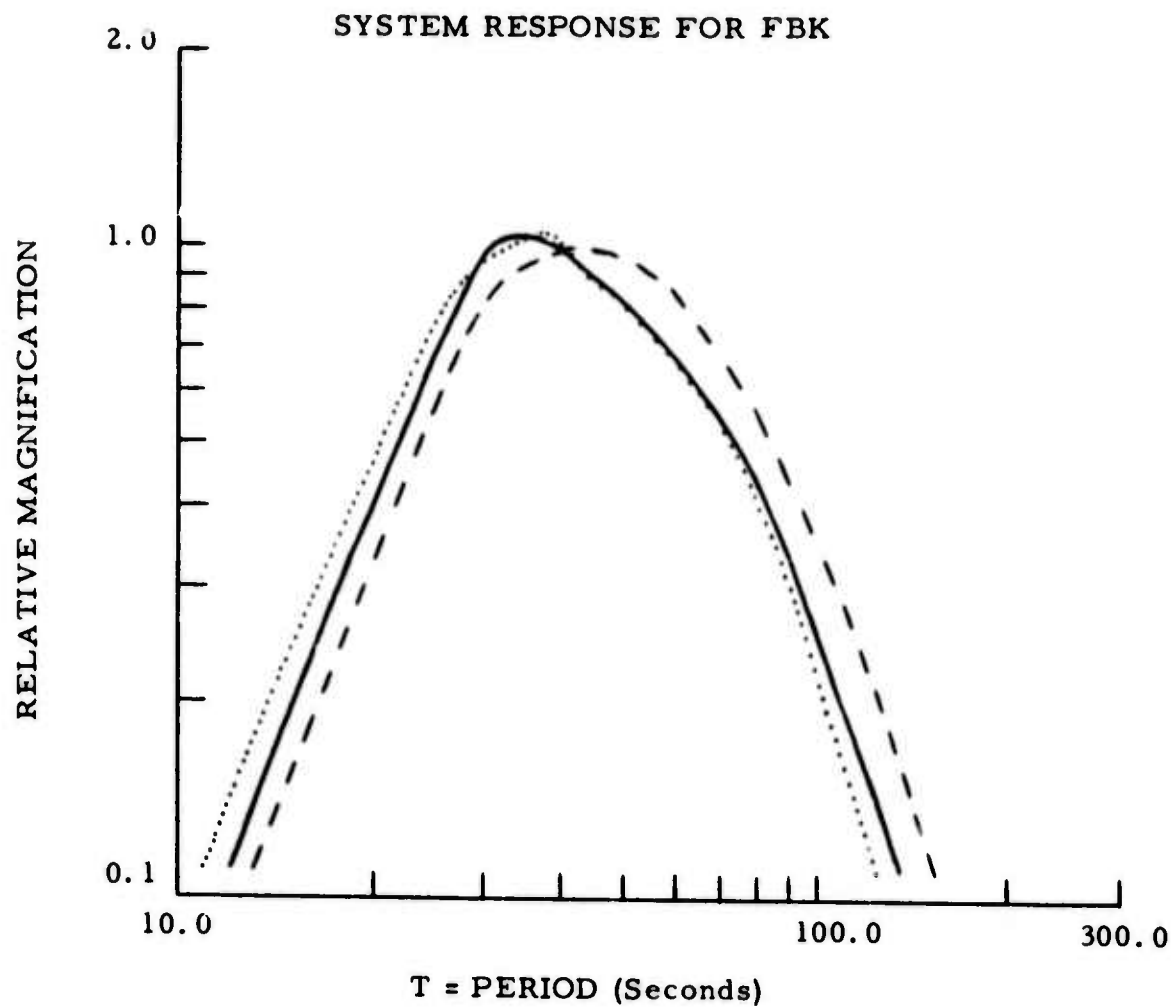
| | | |
|-------|---|---------------------|
| — | Z | 0.721 $m\mu$ /count |
| - - - | N | 1.48 $m\mu$ /count |
| | E | 1.28 $m\mu$ /count |

SYSTEM RESPONSE FOR CHG



Gain at T = 40.0 Sec.

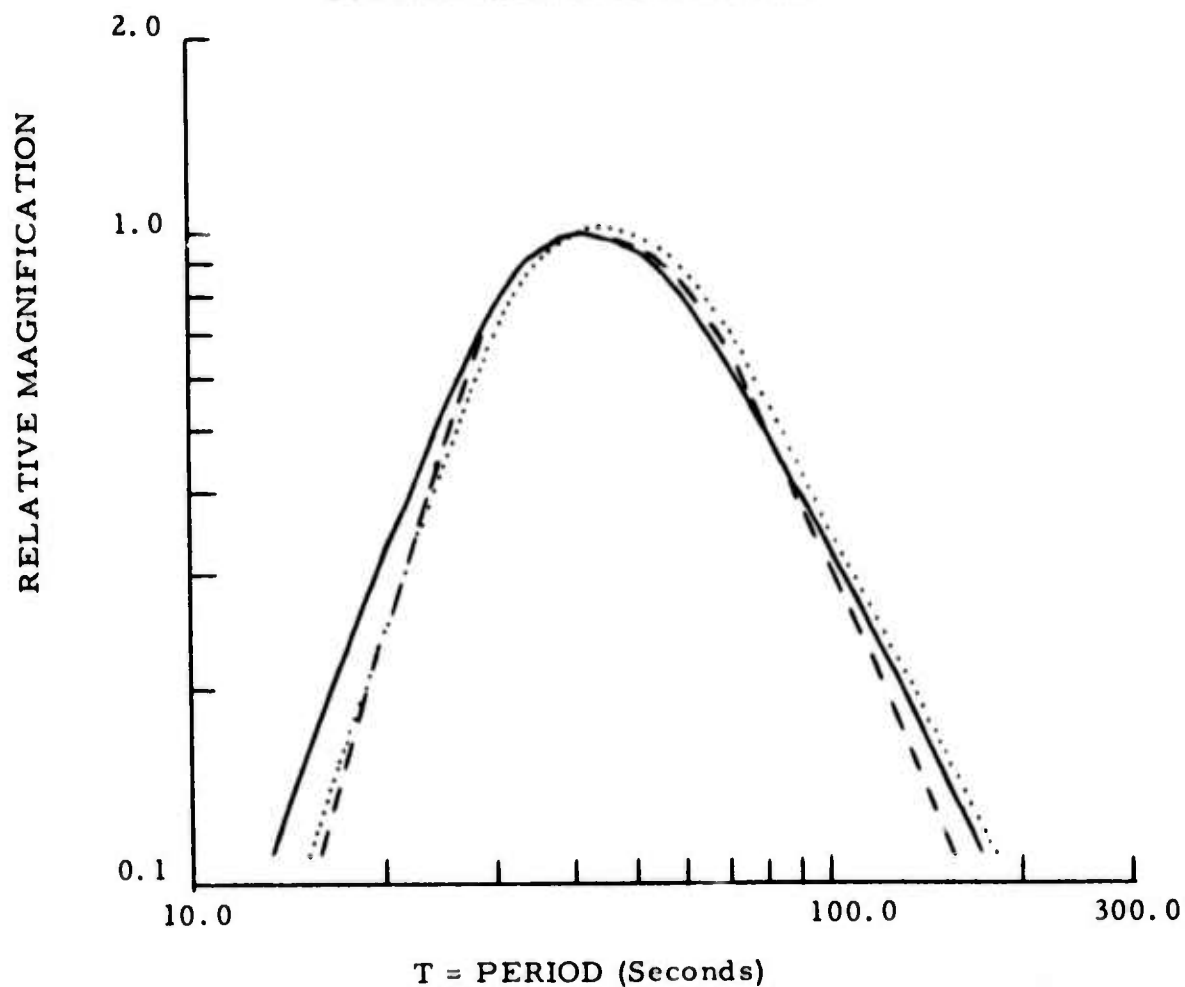
| | | |
|-------|---|----------------|
| — | Z | 0.806 mμ/count |
| - - - | N | 1.14 mμ/count |
| | E | 0.806 mμ/count |



Gain at T = 40.0 Sec.

| | | |
|---------|---|---------------|
| — | Z | 1.33 mμ/count |
| - - - | N | 1.64 mμ/count |
| | E | 1.26 mμ/count |

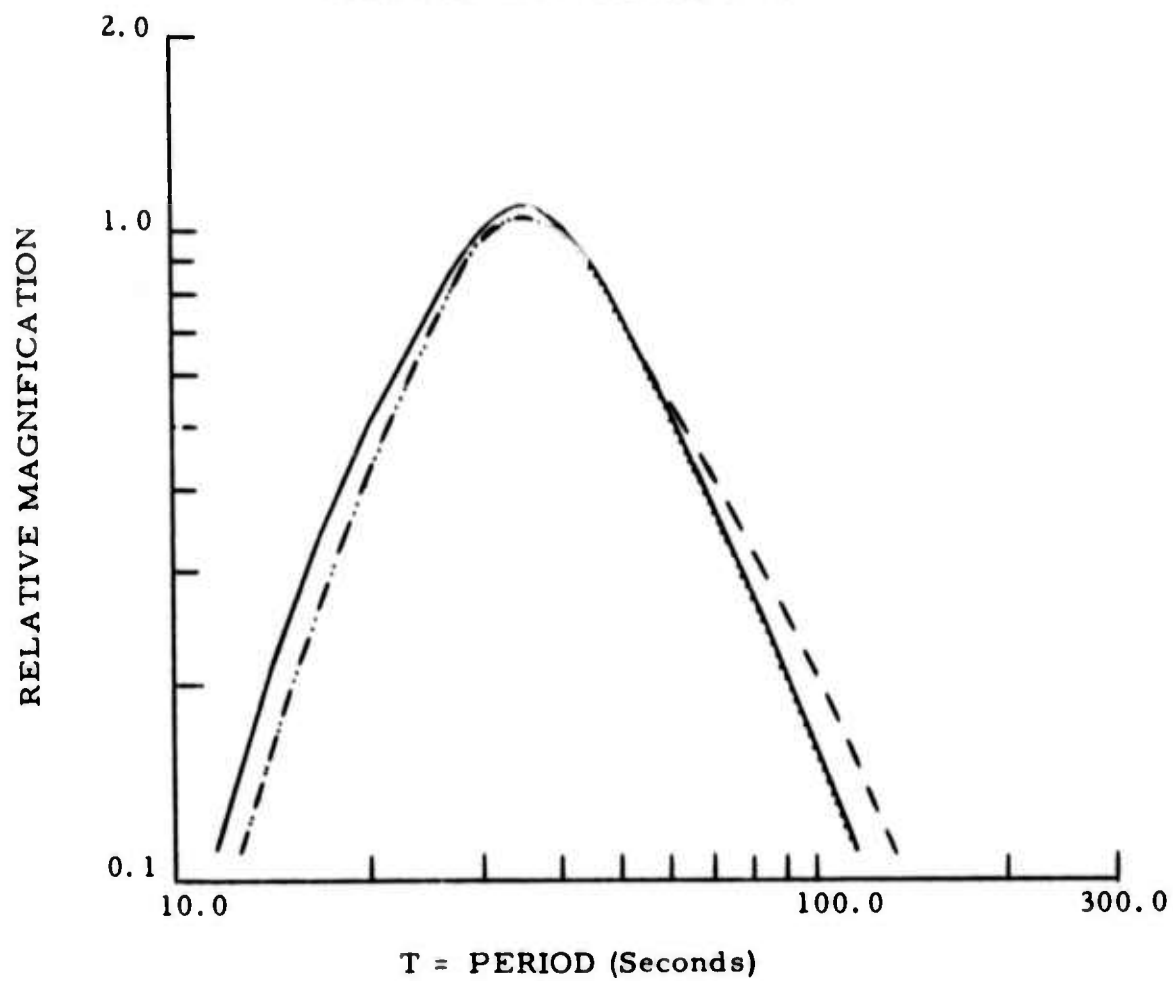
SYSTEM RESPONSE FOR TLO



Gain at T = 40.0 Sec.

| | | |
|-------|---|----------------|
| — | Z | 0.708 mμ/count |
| - - - | N | 0.625 mμ/count |
| | E | 0.584 mμ/count |

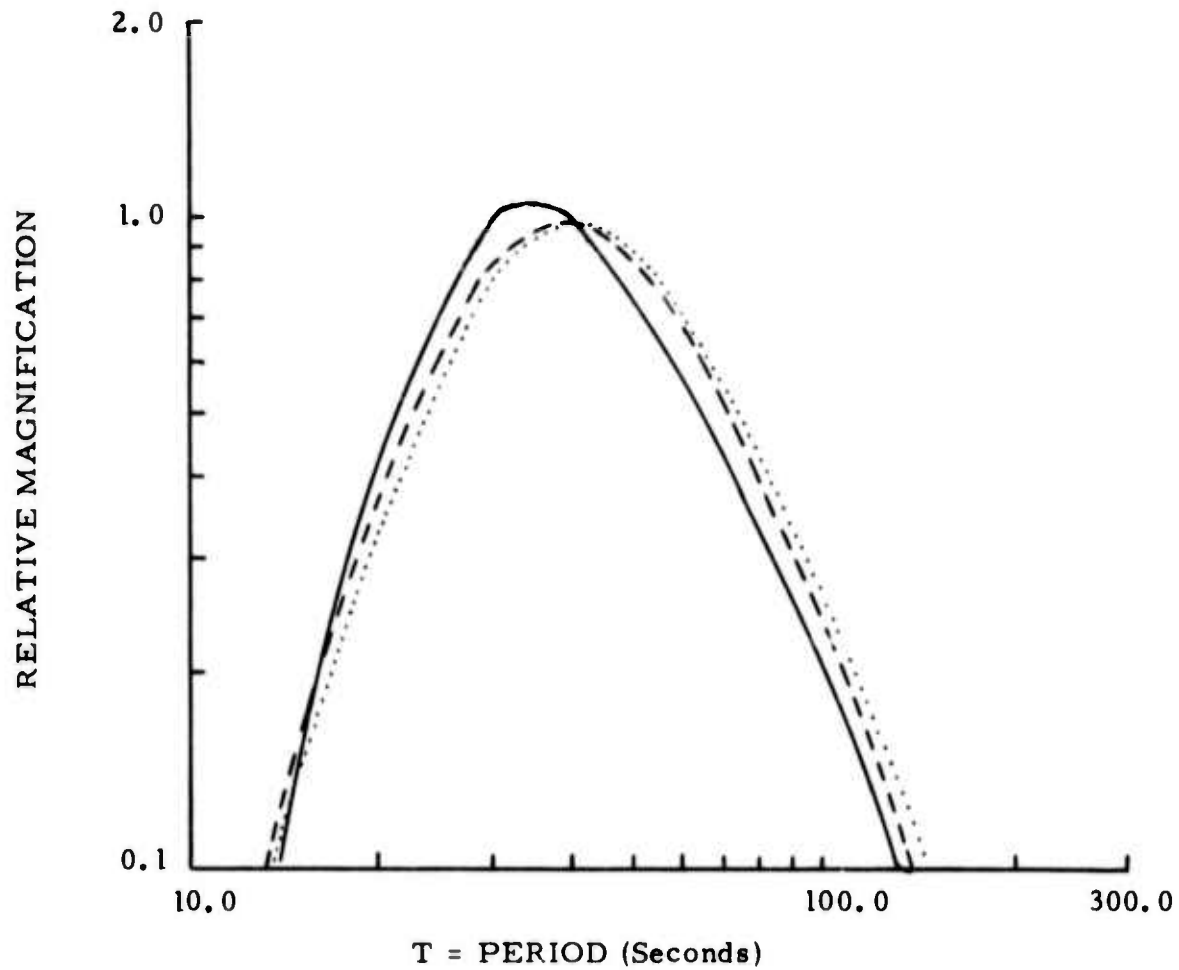
SYSTEM RESPONSE FOR EIL PRIOR TO NOVEMBER, 1972



Gain at T = 40.0 Sec.

| | | |
|---------|---|----------------|
| — | Z | 0.794 mμ/count |
| - - - | N | 1.34 mμ/count |
| | E | 1.75 mμ/count |

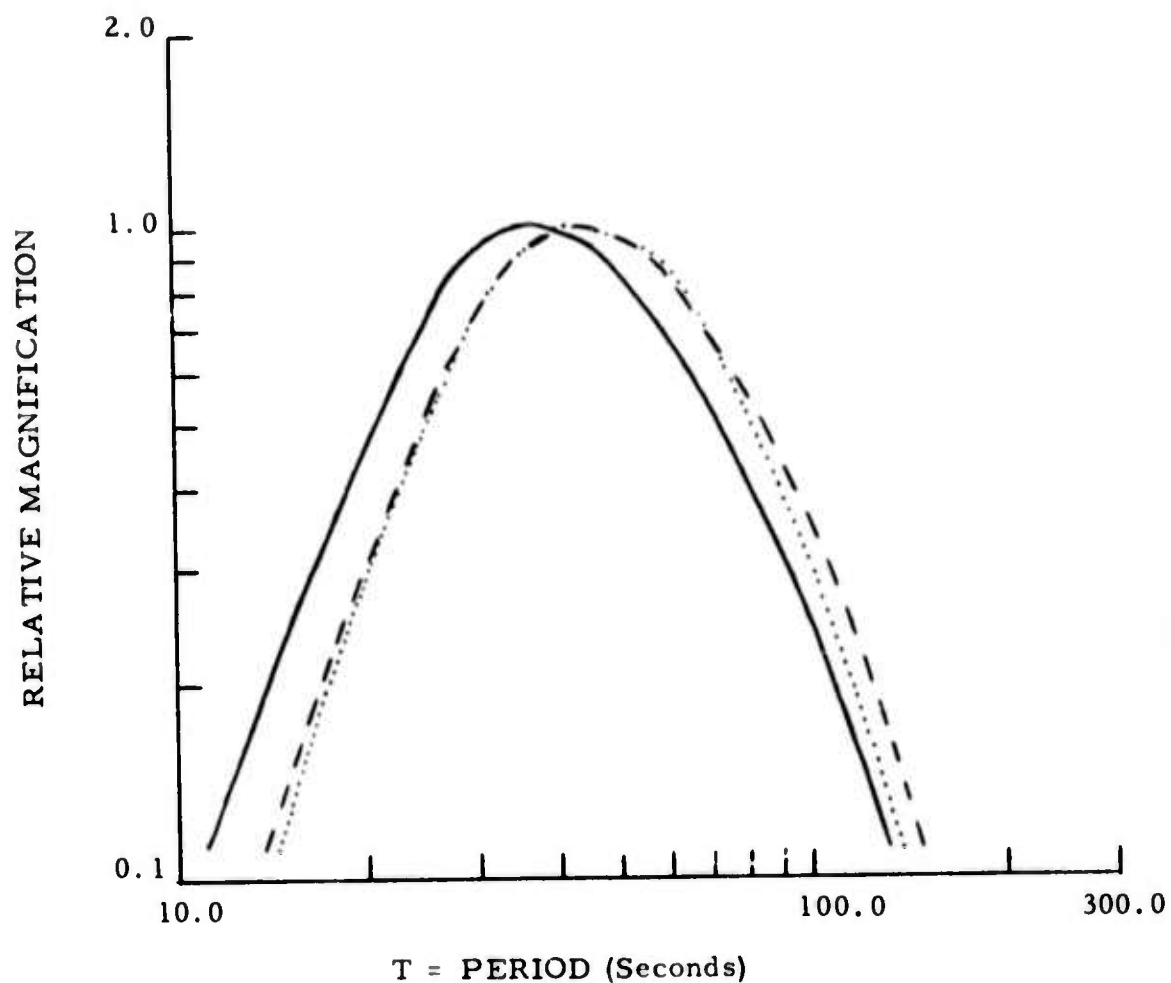
SYSTEM RESPONSE FOR EIL
NOVEMBER 1972 TO PRESENT



Gain at T = 40.0 Sec.

| | | |
|---------|---|----------------------|
| — | Z | 1.701 m μ /count |
| - - - | N | 1.441 m μ /count |
| | E | 1.774 m μ /count |

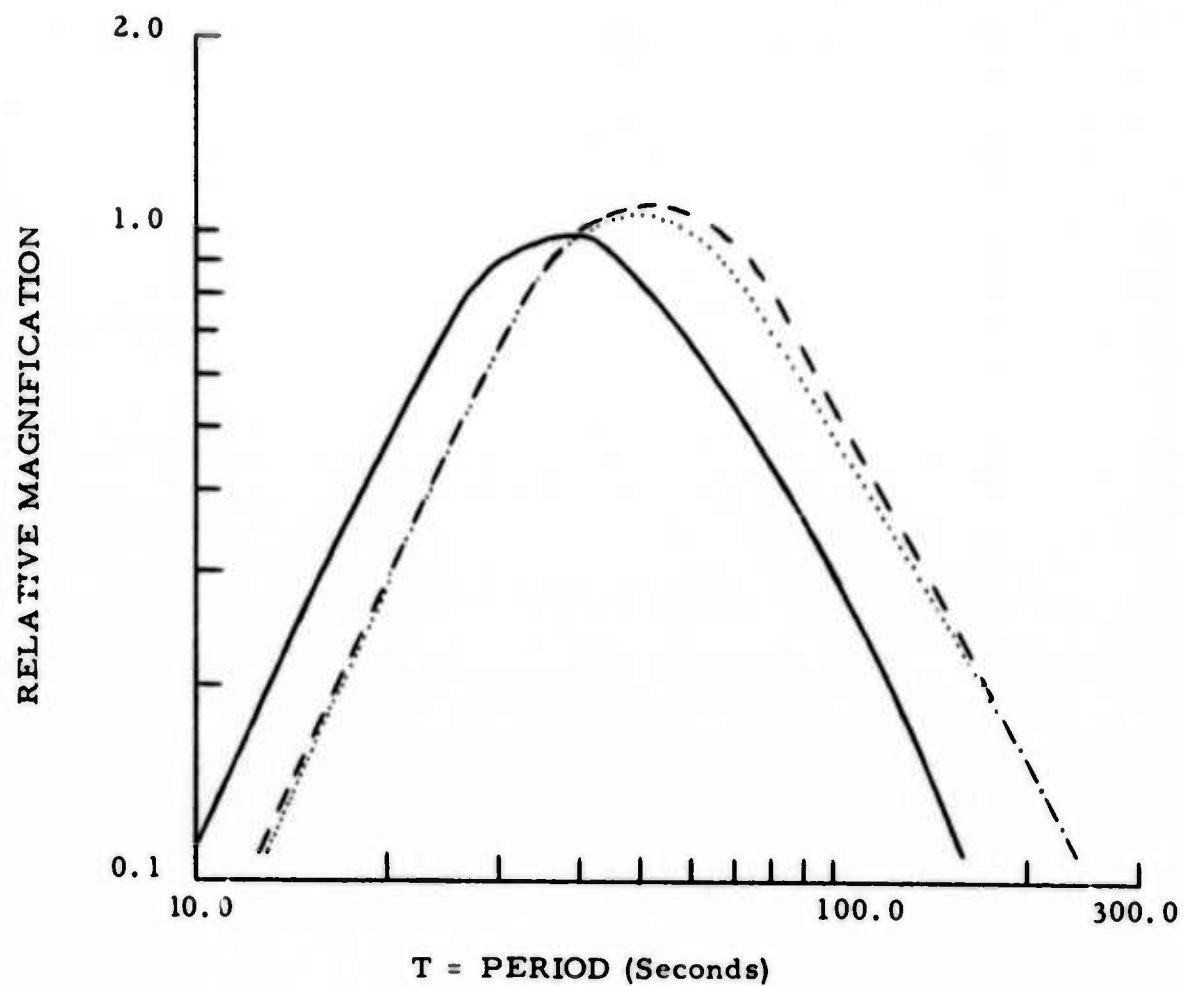
SYSTEM RESPONSE FOR KON



Gain at T = 40.0 Sec.

| | | |
|---------|---|----------------|
| — | Z | 0.656 mμ/count |
| - - - | N | 0.530 mμ/count |
| | E | 0.470 mμ/count |

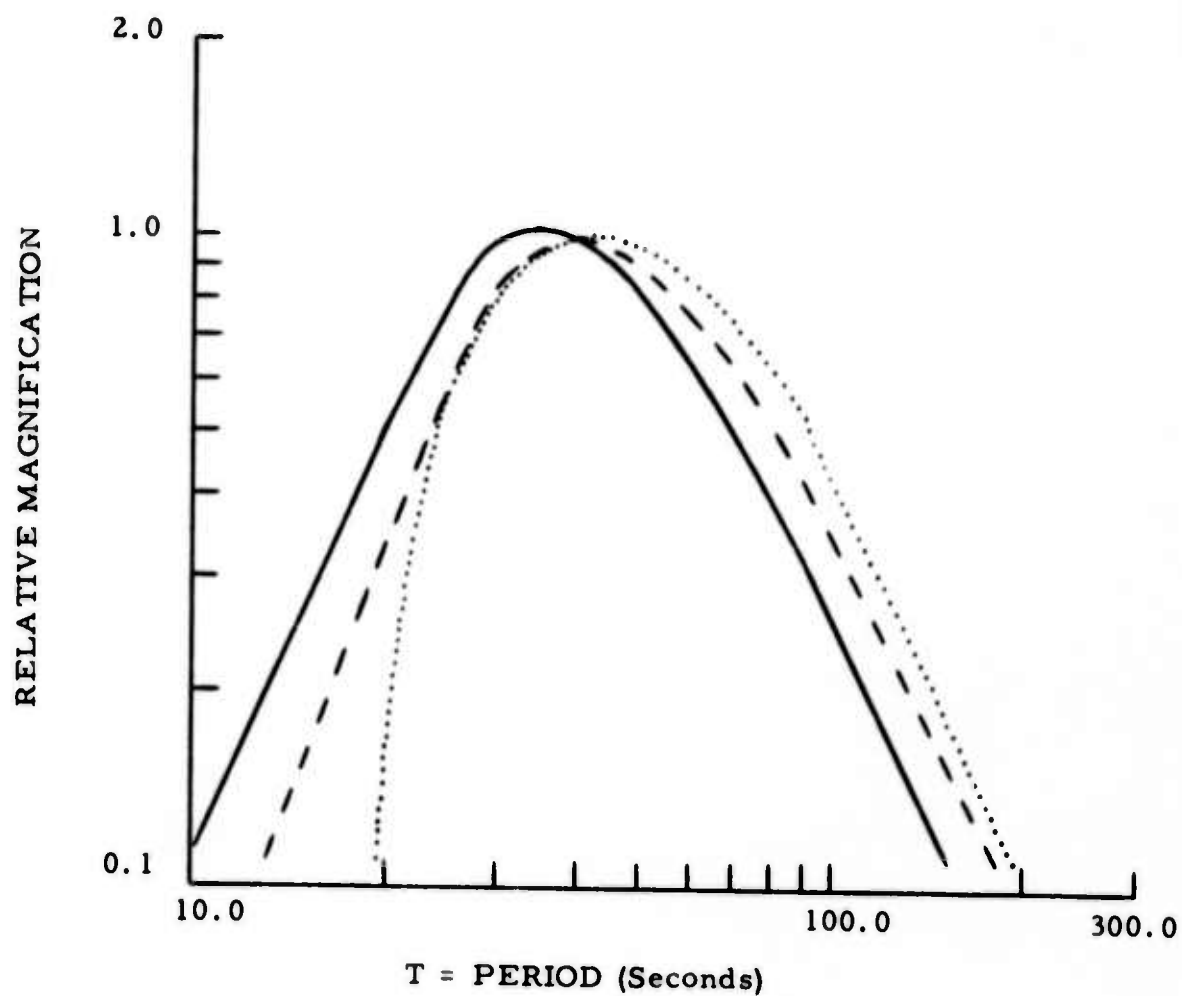
SYSTEM RESPONSE FOR OGD



Gain at T = 40.0 Sec.

| | | |
|---------|---|----------------|
| — | Z | 0.927 mμ/count |
| - - - | N | 0.355 mμ/count |
| | E | 0.397 mμ/count |

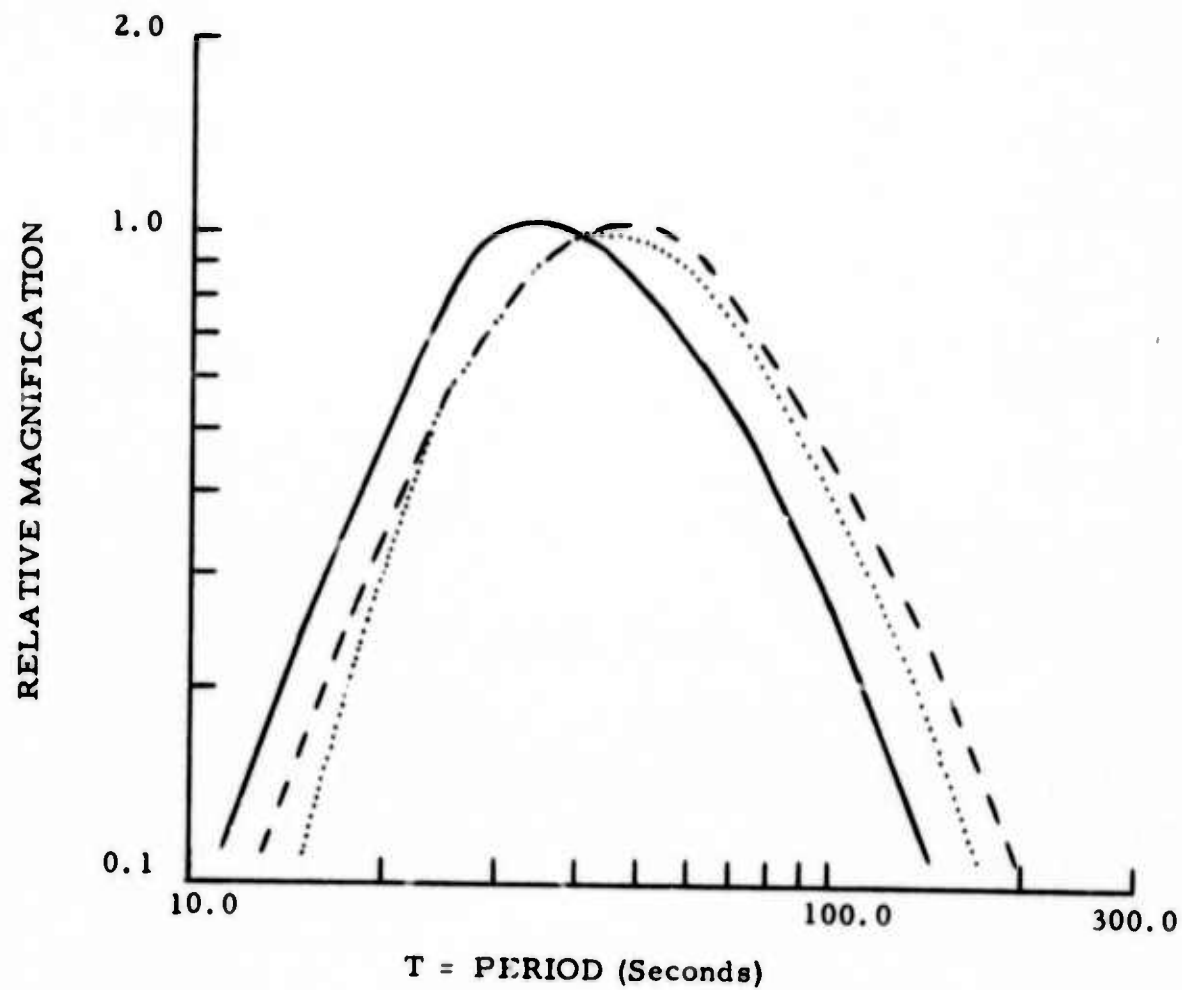
SYSTEM RESPONSE FOR KIP



Gain at T = 40.0 Sec.

| | | |
|-------|---|---------------|
| — | Z | 1.15 mμ/count |
| - - - | N | 1.41 mμ/count |
| | E | 1.14 mμ/count |

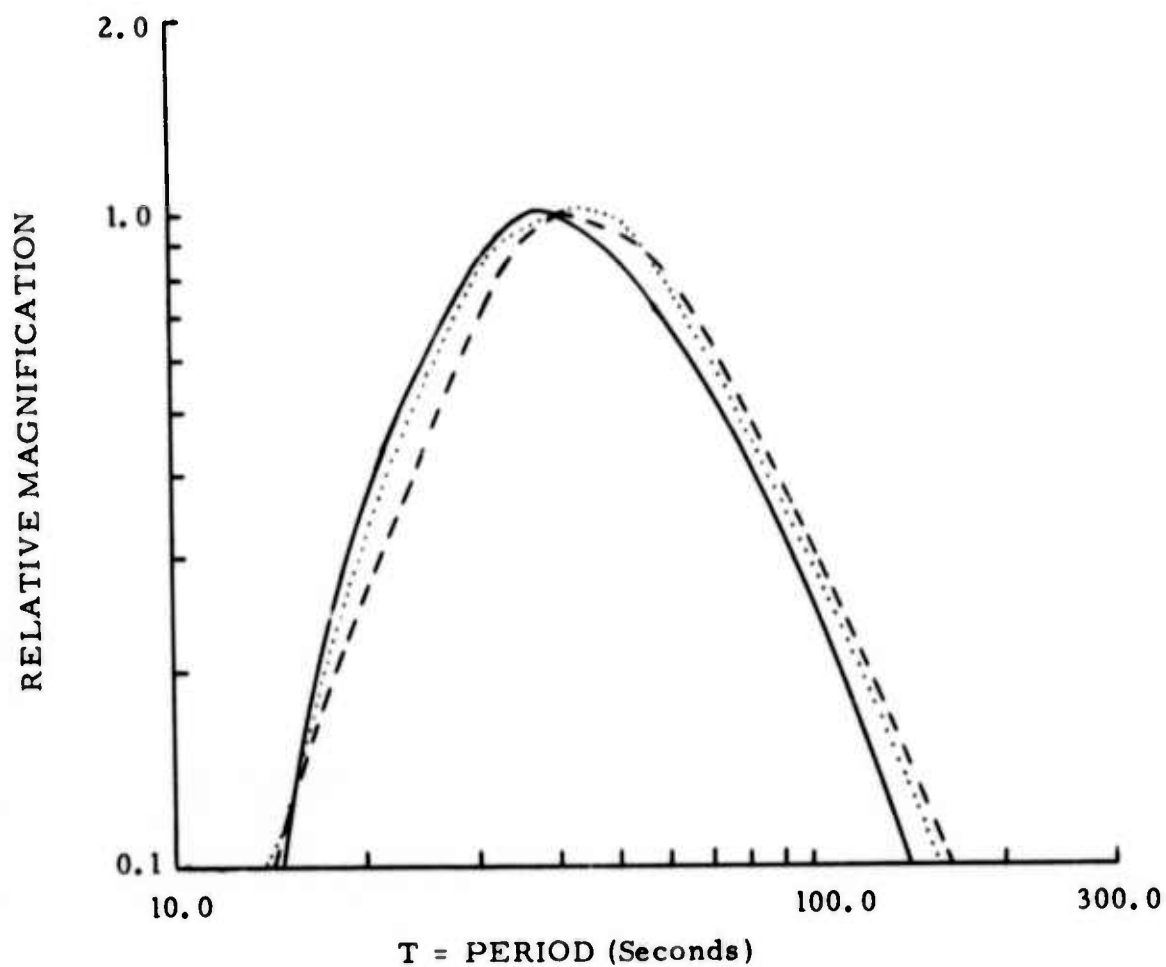
SYSTEM RESPONSE FOR ALQ



Gain at T = 40.0 Sec.

| | | |
|-------|---|----------------|
| — | Z | 1.12 mμ/count |
| - - - | N | 0.697 mμ/count |
| | E | 0.819 mμ/count |

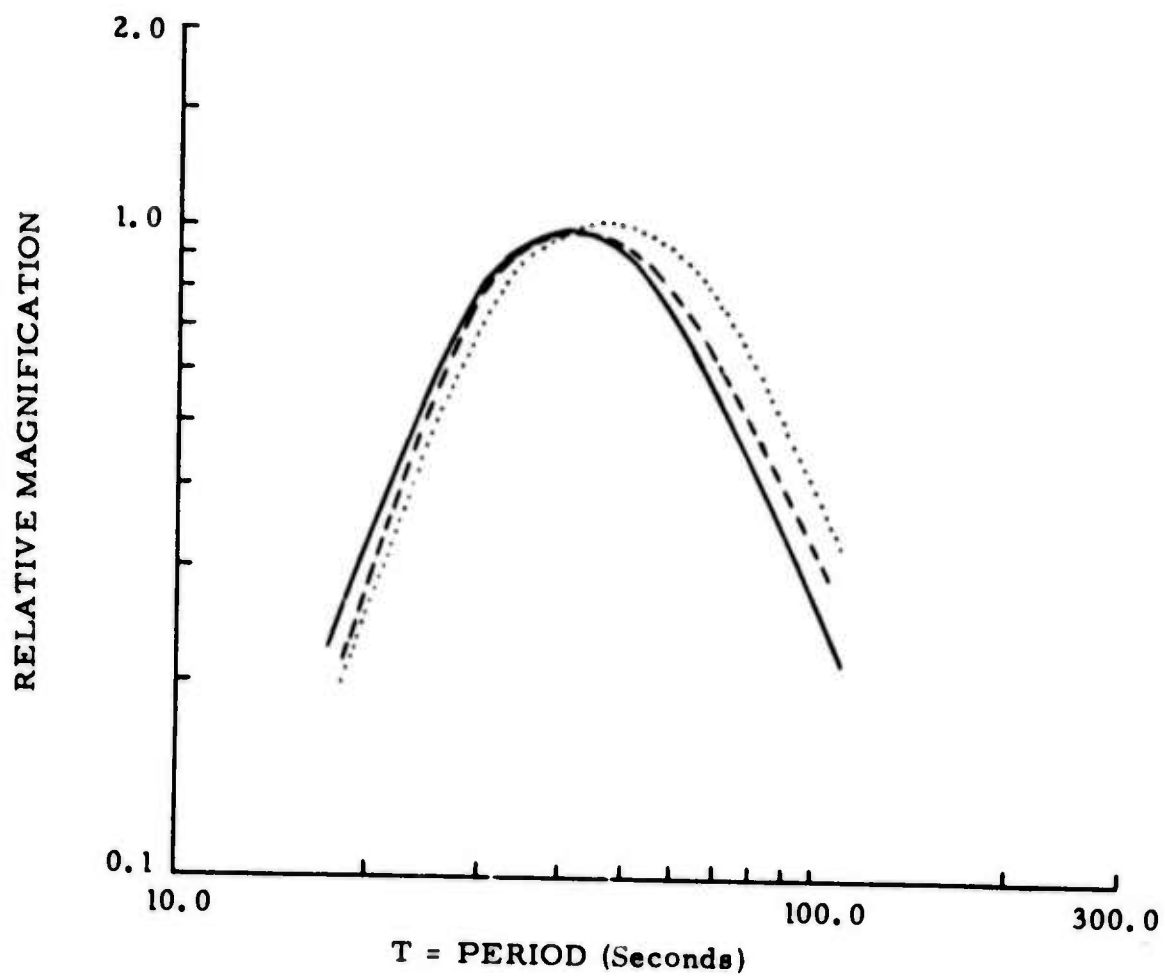
SYSTEM RESPONSE FOR ZLP



Gain at T = 40.0 Sec.

| | | |
|---------|---|----------------------|
| — | Z | 1.354 m μ /count |
| - - - | N | 1.372 m μ /count |
| | E | 1.187 m μ /count |

SYSTEM RESPONSE FOR MAT



Gain at T = 40.0 Sec.

| | | |
|---------|---|------------------|
| — | Z | 1.460 mμ / count |
| - - - | N | 0.786 mμ / count |
| | E | 1.120 mμ / count |

APPENDIXES FOR SECTION III
A THROUGH D

| EILAT, ISRAEL | | | | | | | | | | | | | | | | | |
|------------------------|--|-------|-------|-------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| NUMBER OF CONC SAMPLES | | 1F | | | | | | | | | | | | | | | |
| ZMEANS = | | 14.30 | 6.17 | 2.74 | 2.83 | 2.12 | 1.52 | 1.53 | 1.80 | 2.04 | 2.25 | 2.11 | 2.27 | 2.20 | 2.21 | 2.25 | 2.34 |
| ZSDV = | | 20.02 | 7.10 | 2.21 | 3.27 | 2.85 | 1.25 | 1.02 | 1.85 | 2.15 | 2.87 | 2.20 | 2.24 | 2.05 | 2.09 | 2.37 | 2.52 |
| SMEANS = | | 19.35 | 9.31 | 6.2F | 3.5C | 2.71 | 2.10 | 1.74 | 1.33 | 1.36 | 1.39 | 1.34 | 1.44 | 1.56 | 1.62 | 1.35 | 1.20 |
| SSDV = | | 31.9A | 14.36 | 10.01 | 5.66 | 3.51 | 2.52 | 1.94 | 1.21 | 1.25 | 1.2A | 1.41 | 1.74 | 2.01 | 1.73 | 1.58 | 1.19 |
| EMEANS = | | 23.10 | 13.15 | 7.14 | 5.51 | 4.63 | 4.50 | 4.34 | 3.46 | 3.80 | 4.82 | 3.7A | 4.06 | 3.71 | 3.86 | 3.02 | 2.59 |
| ESDV = | | 25.32 | 13.55 | 6.34 | 3.36 | 3.02 | 3. | 3.30 | 2.64 | 3.74 | 5.43 | 3.11 | 3.20 | 2.73 | 2.7A | 2.16 | 1.72 |

| ALBUQUERQUE, NEW MEXICO | | | | | | | | | | | | | | | | | |
|-------------------------|--|-------|-------|------|------|------|------|------|------|------|-------|-------|-------|-------|-------|-------|-------|
| NUMBER OF CONC SAMPLES | | 46 | | | | | | | | | | | | | | | |
| ZMEANS = | | 5.44 | 3.37 | 2.70 | 2.11 | 1.89 | 2.03 | 2.25 | 3.10 | 4.49 | 5.63 | 7.28 | 7.27 | 7.11 | 6.39 | 5.32 | 4.37 |
| ZSDV = | | 3.20 | 2.26 | 1.89 | 1.00 | 0.55 | 1.04 | 1.13 | 1.86 | 3.25 | 3.76 | 3.97 | 3.69 | 4.24 | 2.94 | 1.90 | 1.78 |
| SMEANS = | | 23.50 | 14.33 | 5.45 | 7.21 | 5.81 | 4.81 | 4.55 | 5.03 | 7.35 | 8.52 | 10.54 | 11.00 | 11.75 | 11.00 | 10.33 | 9.35 |
| SSDV = | | 2.56 | 13.01 | 9.64 | 6.53 | 4.76 | 2.97 | 2.97 | 2.55 | 5.15 | 4.44 | 5.81 | 5.75 | 5.44 | 5.89 | 5.76 | 3.97 |
| EMEANS = | | 14.23 | 5.65 | 6.70 | 5.26 | 4.24 | 3.55 | 4.10 | 5.43 | 7.50 | 10.02 | 12.49 | 14.23 | 15.16 | 15.19 | 14.34 | 11.64 |
| ESDV = | | 8.42 | 6.58 | 4.19 | 3.36 | 1.59 | 2.25 | 2.29 | 3.29 | 4.31 | 5.88 | 7.05 | 7.69 | 8.83 | 7.51 | 7.34 | 5.67 |

| LA PAZ, BOLIVIA | | | | | | | | | | | | | | | | | |
|-----------------|--|------------|------|------|------|------|------|------|------|------|------|------|-------|-------|-------|-------|------|
| NUMBER OF CONC | | SAMPLES 3F | | | | | | | | | | | | | | | |
| ZMEANS= | | 5.01 | 3.85 | 2.57 | 2.76 | 2.57 | 3.22 | 3.80 | 5.06 | 5.20 | 5.26 | 6.95 | 7.27 | 10.67 | 8.34 | 7.88 | 6.07 |
| ZSDV = | | 5.46 | 5.84 | 3.11 | 3.83 | 4.64 | 5.13 | 7.39 | 9.20 | 9.26 | 7.33 | 8.07 | 9.21 | 26.64 | 11.83 | 12.95 | 5.60 |
| SMEANS= | | 9.73 | 6.08 | 4.46 | 3.74 | 3.55 | 3.15 | 3.66 | 4.49 | 5.05 | 5.83 | 7.12 | 8.23 | 10.26 | 9.07 | 8.00 | 6.77 |
| SSDV = | | 11.87 | 7.68 | 5.23 | 4.20 | 4.71 | 4.03 | 4.52 | 7.64 | 5.68 | 7.66 | 5.78 | 7.25 | 17.63 | 11.54 | 9.31 | 5.07 |
| EMEANS= | | 13.17 | 6.93 | 4.57 | 3.41 | 2.52 | 3.00 | 3.45 | 4.00 | 4.49 | 4.54 | 5.28 | 6.76 | 10.00 | 7.16 | 6.51 | 5.45 |
| ESDV = | | 11.79 | 5.68 | 3.55 | 3.31 | 3.60 | 4.60 | 7.63 | 6.07 | 8.51 | 6.55 | 4.90 | 11.74 | 26.12 | 11.75 | 8.70 | 5.10 |

| MATSUSHIRO, JAPAN | | | | | | | | | | | | | | | | | | | |
|------------------------|--|--|--|-------|-------|-------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| NUMBER OF CONC SAMPLES | | | | 11 | | | | | | | | | | | | | | | |
| ZMEANS = | | | | 32.76 | 17.18 | 10.36 | 7.14 | 5.16 | 3.72 | 3.59 | 4.58 | 3.70 | 3.71 | 4.23 | 5.08 | 5.23 | 5.72 | 5.57 | 5.44 |
| ZSDV = | | | | 22.22 | 13.28 | 8.25 | 5.01 | 3.32 | 1.86 | 1.77 | 2.78 | 1.57 | 1.39 | 0.95 | 1.75 | 1.60 | 2.77 | 1.36 | 1.47 |
| SMEANS = | | | | 15.85 | 10.56 | 7.55 | 6.65 | 5.14 | 3.92 | 3.82 | 3.83 | 3.40 | 3.96 | 4.33 | 5.57 | 6.33 | 5.41 | 5.47 | 5.22 |
| SSDV = | | | | 12.16 | 6.71 | 5.90 | 5.67 | 4.22 | 2.09 | 2.62 | 1.62 | 1.32 | 2.60 | 1.36 | 1.78 | 2.75 | 1.97 | 1.07 | 1.26 |
| EMEANS = | | | | 7.89 | 5.64 | 4.71 | 3.28 | 2.15 | 2.63 | 2.77 | 2.84 | 3.11 | 3.59 | 5.31 | 6.50 | 6.40 | 5.81 | 7.12 | 6.18 |
| ESDV = | | | | 2.66 | 2.80 | 2.18 | 1.30 | 1.01 | 1.27 | 1.33 | 1.26 | 1.08 | 0.90 | 1.73 | 2.50 | 3.47 | 2.51 | 2.24 | 1.60 |
| <hr/> | | | | | | | | | | | | | | | | | | | |
| 13.5 | | | | | | | | | | | | | | | | | | | |

62.5

PERIOD (SECONDS)

APPENDIX III-A. MEANS AND STANDARD DEVIATIONS OF THREE-COMPONENT GROUND NOISE AMPLITUDES AT VLPE STATIONS. DATA GIVEN IN RMS MILLIMICRONS.

| NUMBER OF GOOD SAMPLES | | EILAT, ISRAEL | | | | | | | | | |
|------------------------|------|---------------|------|------|------|------|-------|-------|-------|-------|-------|
| | | 1A | 0.22 | 0.07 | 0.04 | 0.03 | 0.09 | 0.11 | 0.11 | 0.16 | 0.13 |
| ZMEANS = | 0.75 | 0.52 | 0.27 | 0.07 | 0.04 | 0.03 | 0.09 | 0.11 | 0.11 | 0.16 | 0.13 |
| ZSDV = | 0.64 | 0.53 | 0.45 | 0.47 | 0.46 | 0.31 | 0.34 | 0.43 | 0.45 | 0.46 | 0.51 |
| SMEANS = | 0.74 | 0.52 | 0.22 | 0.15 | 0.10 | 0.01 | -0.05 | -0.10 | -0.13 | -0.09 | -0.06 |
| SSDV = | 0.74 | 0.71 | 0.74 | 0.68 | 0.65 | 0.61 | 0.59 | 0.52 | 0.51 | 0.54 | 0.52 |
| FMEANS = | 1.04 | 0.51 | 0.65 | 0.62 | 0.54 | 0.40 | 0.39 | 0.40 | 0.42 | 0.44 | 0.44 |
| ESDV = | 0.52 | 0.44 | 0.41 | 0.37 | 0.34 | 0.41 | 0.42 | 0.42 | 0.42 | 0.44 | 0.43 |

| NUMBER OF GOOD SAMPLES | | ALBUQUERQUE, NEW MEXICO | | | | | | | | | |
|------------------------|------|-------------------------|------|------|------|------|------|------|------|------|------|
| | | 66 | 0.24 | 0.23 | 0.26 | 0.30 | 0.42 | 0.57 | 0.64 | 0.77 | 0.61 |
| ZMEANS = | 0.60 | 0.49 | 0.24 | 0.23 | 0.26 | 0.30 | 0.42 | 0.57 | 0.64 | 0.77 | 0.61 |
| ZSDV = | 0.18 | 0.17 | 0.14 | 0.21 | 0.14 | 0.20 | 0.26 | 0.26 | 0.23 | 0.17 | 0.16 |
| SMEANS = | 1.24 | 1.02 | 0.85 | 0.75 | 0.67 | 0.62 | 0.54 | 0.65 | 0.67 | 0.90 | 0.92 |
| SSDV = | 0.34 | 0.33 | 0.31 | 0.24 | 0.27 | 0.23 | 0.25 | 0.22 | 0.23 | 0.21 | 0.21 |
| FMEANS = | 1.10 | 0.52 | 0.76 | 0.64 | 0.59 | 0.54 | 0.67 | 0.61 | 0.94 | 1.00 | 1.02 |
| ESDV = | 0.21 | 0.22 | 0.23 | 0.24 | 0.19 | 0.21 | 0.23 | 0.23 | 0.24 | 0.23 | 0.20 |

| NUMBER OF GOOD SAMPLES | | LA PAZ, BOLIVIA | | | | | | | | | |
|------------------------|------|-----------------|------|------|------|------|------|------|------|------|------|
| | | 2A | 0.17 | 0.20 | 0.20 | 0.25 | 0.34 | 0.43 | 0.44 | 0.62 | 0.60 |
| ZMEANS = | 0.47 | 0.32 | 0.22 | 0.17 | 0.20 | 0.25 | 0.34 | 0.43 | 0.44 | 0.62 | 0.60 |
| ZSDV = | 0.64 | 0.67 | 0.73 | 0.64 | 0.66 | 0.69 | 0.72 | 0.55 | 0.66 | 0.65 | 0.54 |
| SMEANS = | 0.84 | 0.65 | 0.53 | 0.45 | 0.42 | 0.30 | 0.43 | 0.49 | 0.52 | 0.92 | 0.95 |
| SSDV = | 0.31 | 0.31 | 0.25 | 0.22 | 0.20 | 0.24 | 0.31 | 0.30 | 0.31 | 0.27 | 0.25 |
| FMEANS = | 0.89 | 0.63 | 0.46 | 0.33 | 0.27 | 0.25 | 0.36 | 0.39 | 0.44 | 0.54 | 0.61 |
| ESDV = | 0.55 | 0.52 | 0.40 | 0.50 | 0.44 | 0.45 | 0.47 | 0.47 | 0.44 | 0.43 | 0.34 |

| NUMBER OF GOOD SAMPLES | | MATSUSHIRO, JAPAN | | | | | | | | | |
|------------------------|------|-------------------|------|------|------|------|------|------|------|------|------|
| | | 11 | 0.70 | 0.65 | 0.53 | 0.51 | 0.60 | 0.54 | 0.54 | 0.62 | 0.72 |
| ZMEANS = | 1.45 | 1.15 | 0.57 | 0.70 | 0.65 | 0.51 | 0.60 | 0.54 | 0.54 | 0.62 | 0.72 |
| ZSDV = | 0.23 | 0.26 | 0.26 | 0.24 | 0.20 | 0.20 | 0.24 | 0.16 | 0.14 | 0.00 | 0.10 |
| SMEANS = | 1.12 | 0.57 | 0.87 | 0.71 | 0.62 | 0.54 | 0.51 | 0.55 | 0.54 | 0.61 | 0.71 |
| SSDV = | 0.24 | 0.25 | 0.28 | 0.31 | 0.29 | 0.21 | 0.24 | 0.19 | 0.22 | 0.15 | 0.14 |
| FMEANS = | 0.84 | 0.72 | 0.44 | 0.50 | 0.43 | 0.30 | 0.41 | 0.42 | 0.54 | 0.70 | 0.73 |
| ESDV = | 0.14 | 0.17 | 0.16 | 0.15 | 0.15 | 0.17 | 0.19 | 0.16 | 0.10 | 0.14 | 0.15 |

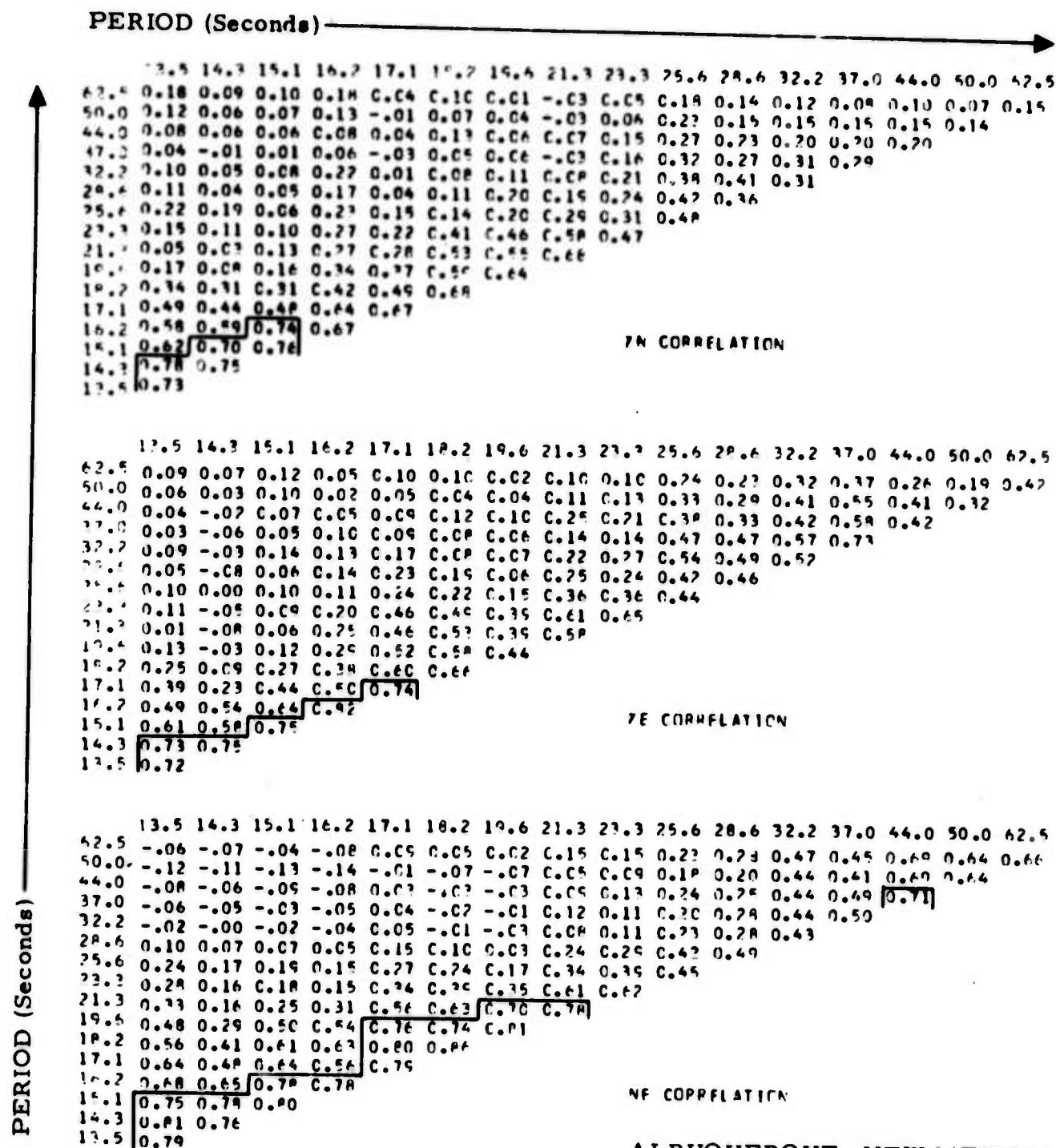
62.5

PERIOD (SECONDS)

APPENDIX III-B. MEANS AND STANDARD DEVIATION OF BASE 10 LOGARITHMS OF THREE-COMPONENT GROUND NOISE AMPLITUDES (MILLIMICRONS, RMS) AT VLPE STATIONS.

| PERIOD (Seconds) | PERIOD (Seconds) | | | | | | | | | | | | | | | |
|------------------|------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| | 12.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
| 12.5 | 0.35 | 0.31 | 0.32 | 0.44 | 0.31 | 0.23 | 0.17 | 0.18 | 0.15 | 0.36 | 0.47 | 0.53 | 0.46 | 0.49 | 0.45 | 0.49 |
| 14.3 | 0.29 | 0.26 | 0.24 | 0.36 | 0.24 | 0.21 | 0.11 | 0.12 | 0.11 | 0.26 | 0.37 | 0.43 | 0.39 | 0.38 | 0.36 | |
| 15.1 | 0.30 | 0.25 | 0.20 | 0.40 | 0.30 | 0.35 | 0.20 | 0.21 | 0.19 | 0.28 | 0.42 | 0.51 | 0.53 | 0.39 | | |
| 16.2 | -0.08 | -0.07 | -0.12 | -0.04 | -0.05 | -0.03 | -0.20 | -0.15 | -0.16 | -0.14 | -0.04 | -0.00 | 0.03 | | | |
| 17.1 | -0.13 | -0.12 | -0.16 | -0.11 | -0.15 | -0.07 | -0.22 | -0.23 | -0.18 | -0.20 | -0.12 | -0.09 | | | | |
| 18.2 | -0.03 | 0.03 | -0.07 | -0.02 | -0.06 | 0.10 | -0.13 | -0.14 | -0.06 | -0.12 | -0.01 | | | | | |
| 19.6 | 0.03 | 0.06 | -0.01 | 0.04 | -0.01 | 0.15 | -0.06 | -0.07 | -0.01 | -0.08 | | | | | | |
| 21.3 | -0.06 | -0.04 | -0.12 | -0.06 | -0.10 | 0.01 | -0.17 | -0.17 | -0.10 | | | | | | | |
| 23.3 | -0.05 | -0.02 | -0.18 | -0.10 | -0.08 | -0.01 | -0.14 | -0.05 | | | | | | | | |
| 25.6 | 0.10 | 0.17 | 0.01 | 0.05 | 0.05 | 0.10 | 0.21 | 0.07 | | | | | | | | |
| 28.6 | 0.22 | 0.32 | 0.15 | 0.15 | 0.17 | 0.41 | | | | | | | | | | |
| 32.2 | 0.29 | 0.38 | 0.23 | 0.18 | 0.15 | | | | | | | | | | | |
| 37.0 | 0.18 | 0.24 | 0.11 | 0.05 | | | | | | | | | | | | |
| 44.0 | 0.20 | 0.27 | 0.13 | | | | | | | | | | | | | |
| 50.0 | 0.32 | 0.34 | | | | | | | | | | | | | | |
| 62.5 | 0.24 | | | | | | | | | | | | | | | |
| ZN CORRELATION | | | | | | | | | | | | | | | | |
| 12.5 | -0.38 | -0.38 | -0.40 | -0.46 | -0.46 | -0.34 | -0.38 | -0.38 | -0.30 | -0.35 | -0.31 | -0.37 | -0.21 | -0.20 | 0.02 | 0.00 |
| 14.3 | -0.44 | -0.43 | -0.44 | -0.51 | -0.49 | -0.38 | -0.41 | -0.41 | -0.34 | -0.37 | -0.32 | -0.40 | -0.24 | -0.22 | -0.00 | |
| 15.1 | -0.26 | -0.32 | -0.25 | -0.35 | -0.34 | -0.22 | -0.41 | -0.35 | -0.25 | -0.23 | -0.15 | -0.17 | 0.06 | 0.10 | | |
| 16.2 | -0.40 | -0.32 | -0.37 | -0.40 | -0.44 | -0.35 | -0.37 | -0.39 | -0.34 | -0.34 | -0.31 | -0.31 | -0.11 | | | |
| 17.1 | -0.37 | -0.25 | -0.32 | -0.37 | -0.35 | -0.25 | -0.33 | -0.33 | -0.30 | -0.27 | -0.25 | -0.28 | | | | |
| 18.2 | -0.27 | -0.21 | -0.25 | -0.32 | -0.35 | -0.28 | -0.25 | -0.25 | -0.20 | -0.22 | -0.19 | | | | | |
| 19.6 | -0.23 | -0.23 | -0.22 | -0.24 | -0.23 | -0.21 | -0.23 | -0.21 | -0.14 | -0.13 | | | | | | |
| 21.3 | -0.28 | -0.18 | -0.15 | -0.22 | -0.23 | -0.14 | -0.11 | -0.12 | -0.12 | | | | | | | |
| 23.3 | 0.06 | 0.23 | 0.26 | 0.35 | 0.33 | 0.45 | 0.50 | | | | | | | | | |
| 25.6 | 0.07 | 0.29 | 0.44 | 0.63 | 0.55 | 0.68 | 0.62 | | | | | | | | | |
| 28.6 | 0.25 | 0.35 | 0.36 | 0.50 | 0.50 | 0.60 | | | | | | | | | | |
| 32.2 | 0.34 | 0.43 | 0.43 | 0.45 | 0.46 | | | | | | | | | | | |
| 37.0 | 0.32 | 0.44 | 0.44 | 0.53 | | | | | | | | | | | | |
| 44.0 | 0.50 | 0.63 | 0.58 | | | | | | | | | | | | | |
| 50.0 | 0.49 | 0.60 | | | | | | | | | | | | | | |
| 62.5 | 0.62 | | | | | | | | | | | | | | | |
| ZE CORRELATION | | | | | | | | | | | | | | | | |
| 12.5 | -0.02 | -0.12 | -0.06 | -0.15 | -0.05 | -0.01 | -0.08 | -0.03 | 0.17 | 0.00 | 0.08 | 0.27 | 0.30 | 0.44 | 0.41 | 0.24 |
| 14.3 | 0.00 | -0.10 | -0.02 | -0.13 | -0.07 | -0.00 | -0.08 | -0.05 | 0.15 | -0.03 | 0.07 | 0.27 | 0.28 | 0.48 | 0.45 | |
| 15.1 | 0.02 | -0.09 | -0.02 | -0.12 | -0.07 | 0.02 | -0.06 | -0.04 | 0.14 | -0.05 | 0.04 | 0.20 | 0.19 | 0.38 | | |
| 16.2 | 0.06 | -0.02 | 0.00 | -0.06 | -0.01 | 0.05 | 0.01 | 0.08 | 0.28 | 0.10 | 0.15 | 0.28 | 0.31 | | | |
| 17.1 | 0.09 | -0.00 | 0.02 | -0.06 | -0.02 | 0.11 | 0.01 | 0.08 | 0.25 | 0.09 | 0.16 | 0.21 | | | | |
| 18.2 | 0.13 | 0.04 | 0.08 | -0.02 | 0.02 | 0.13 | 0.02 | 0.08 | 0.26 | 0.09 | 0.18 | | | | | |
| 19.6 | 0.19 | 0.10 | 0.14 | 0.02 | 0.04 | 0.14 | 0.04 | 0.12 | 0.26 | 0.05 | | | | | | |
| 21.3 | 0.35 | 0.25 | 0.33 | 0.19 | 0.23 | 0.32 | 0.20 | 0.25 | 0.45 | | | | | | | |
| 23.3 | 0.26 | 0.18 | 0.22 | 0.17 | 0.18 | 0.23 | 0.15 | 0.24 | | | | | | | | |
| 25.6 | 0.30 | 0.18 | 0.23 | 0.15 | 0.18 | 0.24 | 0.13 | | | | | | | | | |
| 28.6 | 0.21 | 0.13 | 0.15 | 0.10 | 0.13 | 0.22 | | | | | | | | | | |
| 32.2 | 0.11 | 0.01 | 0.08 | 0.02 | 0.07 | | | | | | | | | | | |
| 37.0 | 0.03 | -0.07 | -0.01 | -0.08 | | | | | | | | | | | | |
| 44.0 | 0.21 | 0.09 | 0.10 | | | | | | | | | | | | | |
| 50.0 | 0.20 | 0.13 | | | | | | | | | | | | | | |
| 62.5 | 0.19 | | | | | | | | | | | | | | | |
| EILAT, ISRAEL | | | | | | | | | | | | | | | | |

APPENDIX III-C. INTER COMPONENT LINEAR CORRELATION COEFFICIENTS FOR RMS GROUND NOISE AMPLITUDES AT VLPE STATIONS AS A FUNCTION OF WAVE PERIOD. HORIZONTAL AXIS DATA LISTS SECOND COMPONENT.



APPENDIX III-C (cont'd)

PERIOD (Seconds) →

| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 42.5 | 0.11 | 0.09 | 0.14 | 0.13 | 0.28 | 0.25 | 0.22 | 0.24 | 0.15 | 0.20 | 0.23 | 0.24 | 0.36 | 0.55 | 0.78 | 0.91 |
| 50.0 | 0.28 | 0.25 | 0.32 | 0.30 | 0.43 | 0.44 | 0.40 | 0.41 | 0.37 | 0.38 | 0.41 | 0.43 | 0.54 | 0.78 | 0.87 | |
| 44.0 | 0.42 | 0.40 | 0.45 | 0.44 | 0.53 | 0.54 | 0.53 | 0.53 | 0.50 | 0.50 | 0.53 | 0.55 | 0.64 | 0.84 | | |
| 37.0 | 0.83 | 0.83 | 0.87 | 0.88 | 0.83 | 0.82 | 0.91 | 0.90 | 0.91 | 0.88 | 0.82 | 0.92 | 0.94 | | | |
| 32.2 | 0.92 | 0.93 | 0.95 | 0.97 | 0.89 | 0.84 | 0.95 | 0.94 | 0.97 | 0.94 | 0.98 | 0.97 | | | | |
| 28.6 | 0.88 | 0.91 | 0.92 | 0.94 | 0.84 | 0.83 | 0.94 | 0.95 | 0.97 | 0.95 | 0.97 | | | | | |
| 25.6 | 0.92 | 0.94 | 0.96 | 0.97 | 0.86 | 0.85 | 0.96 | 0.96 | 0.96 | 0.96 | | | | | | |
| 23.3 | 0.92 | 0.94 | 0.96 | 0.97 | 0.86 | 0.86 | 0.96 | 0.97 | | | | | | | | |
| 21.3 | 0.91 | 0.93 | 0.95 | 0.96 | 0.85 | 0.85 | 0.95 | | | | | | | | | |
| 19.6 | 0.91 | 0.93 | 0.94 | 0.95 | 0.87 | 0.85 | | | | | | | | | | |
| 18.2 | 0.90 | 0.91 | 0.94 | 0.94 | 0.90 | | | | | | | | | | | |
| 17.1 | 0.92 | 0.94 | 0.96 | 0.96 | 0.85 | | | | | | | | | | | |
| 16.2 | 0.94 | 0.97 | 0.98 | 0.99 | | | | | | | | | | | | |
| 15.1 | 0.95 | 0.96 | 0.97 | | | | | | | | | | | | | |
| 14.3 | 0.96 | 0.97 | | | | | | | | | | | | | | |
| 13.5 | 0.92 | | | | | | | | | | | | | | | |

7A CORRELATION

| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 62.5 | 0.13 | 0.24 | 0.14 | 0.13 | 0.17 | 0.23 | 0.22 | 0.15 | 0.13 | 0.11 | 0.16 | 0.15 | 0.15 | 0.10 | 0.12 | 0.14 |
| 50.0 | 0.32 | 0.47 | 0.34 | 0.31 | 0.36 | 0.40 | 0.41 | 0.38 | 0.32 | 0.30 | 0.35 | 0.34 | 0.33 | 0.17 | 0.17 | |
| 44.0 | 0.44 | 0.54 | 0.47 | 0.45 | 0.48 | 0.50 | 0.53 | 0.51 | 0.45 | 0.44 | 0.49 | 0.48 | 0.45 | 0.22 | | |
| 37.0 | 0.78 | 0.90 | 0.88 | 0.88 | 0.88 | 0.76 | 0.88 | 0.90 | 0.88 | 0.88 | 0.89 | 0.87 | 0.78 | | | |
| 32.2 | 0.86 | 0.95 | 0.96 | 0.97 | 0.95 | 0.78 | 0.93 | 0.97 | 0.96 | 0.97 | 0.96 | 0.93 | | | | |
| 28.6 | 0.95 | 0.93 | 0.94 | 0.94 | 0.94 | 0.77 | 0.94 | 0.95 | 0.94 | 0.96 | 0.96 | | | | | |
| 25.6 | 0.87 | 0.96 | 0.96 | 0.98 | 0.97 | 0.75 | 0.95 | 0.98 | 0.97 | 0.98 | | | | | | |
| 23.3 | 0.86 | 0.95 | 0.96 | 0.97 | 0.96 | 0.80 | 0.95 | 0.97 | 0.97 | | | | | | | |
| 21.3 | 0.87 | 0.95 | 0.96 | 0.97 | 0.96 | 0.80 | 0.95 | 0.97 | | | | | | | | |
| 19.6 | 0.85 | 0.93 | 0.93 | 0.94 | 0.94 | 0.75 | 0.94 | | | | | | | | | |
| 18.2 | 0.86 | 0.93 | 0.94 | 0.94 | 0.94 | 0.87 | | | | | | | | | | |
| 17.1 | 0.83 | 0.93 | 0.94 | 0.95 | 0.94 | | | | | | | | | | | |
| 16.2 | 0.84 | 0.95 | 0.97 | 0.95 | | | | | | | | | | | | |
| 15.1 | 0.85 | 0.93 | 0.95 | | | | | | | | | | | | | |
| 14.3 | 0.84 | 0.94 | | | | | | | | | | | | | | |
| 13.5 | 0.84 | | | | | | | | | | | | | | | |

7E CORRELATION

| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 62.5 | 0.34 | 0.48 | 0.41 | 0.41 | 0.43 | 0.42 | 0.46 | 0.46 | 0.40 | 0.35 | 0.43 | 0.40 | 0.37 | 0.15 | 0.12 | 0.17 |
| 50.0 | 0.61 | 0.75 | 0.70 | 0.70 | 0.71 | 0.64 | 0.73 | 0.74 | 0.60 | 0.53 | 0.71 | 0.69 | 0.62 | 0.23 | 0.20 | |
| 44.0 | 0.70 | 0.84 | 0.80 | 0.80 | 0.81 | 0.72 | 0.82 | 0.83 | 0.75 | 0.75 | 0.80 | 0.77 | 0.60 | 0.24 | | |
| 37.0 | 0.79 | 0.91 | 0.90 | 0.91 | 0.90 | 0.76 | 0.90 | 0.92 | 0.92 | 0.92 | 0.91 | 0.88 | 0.78 | | | |
| 32.2 | 0.84 | 0.94 | 0.95 | 0.96 | 0.95 | 0.78 | 0.93 | 0.96 | 0.96 | 0.96 | 0.95 | 0.92 | | | | |
| 28.6 | 0.83 | 0.94 | 0.95 | 0.96 | 0.95 | 0.77 | 0.93 | 0.96 | 0.95 | 0.97 | 0.95 | | | | | |
| 25.6 | 0.81 | 0.89 | 0.90 | 0.91 | 0.90 | 0.71 | 0.85 | 0.91 | 0.92 | 0.92 | | | | | | |
| 23.3 | 0.85 | 0.95 | 0.96 | 0.98 | 0.96 | 0.70 | 0.95 | 0.98 | 0.97 | | | | | | | |
| 21.3 | 0.79 | 0.91 | 0.92 | 0.94 | 0.93 | 0.78 | 0.92 | 0.95 | | | | | | | | |
| 19.6 | 0.82 | 0.92 | 0.93 | 0.95 | 0.93 | 0.77 | 0.91 | | | | | | | | | |
| 18.2 | 0.76 | 0.86 | 0.85 | 0.85 | 0.87 | 0.83 | | | | | | | | | | |
| 17.1 | 0.77 | 0.89 | 0.88 | 0.87 | 0.85 | | | | | | | | | | | |
| 16.2 | 0.82 | 0.94 | 0.96 | 0.98 | | | | | | | | | | | | |
| 15.1 | 0.85 | 0.95 | 0.96 | | | | | | | | | | | | | |
| 14.3 | 0.78 | 0.85 | | | | | | | | | | | | | | |
| 13.5 | 0.80 | | | | | | | | | | | | | | | |

7F CORRELATION

LA PAZ, BOLIVIA

APPENDIX III-C (cont'd)

PERIOD (Seconds) →

| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|------|------|
| 62.5 | -0.30 | -0.35 | -0.17 | -0.32 | -0.13 | -0.15 | -0.09 | -0.20 | -0.38 | -0.12 | 0.03 | 0.19 | 0.18 | 0.35 | 0.30 | 0.45 |
| 50.0 | -0.32 | -0.32 | -0.10 | -0.24 | -0.16 | -0.24 | -0.24 | -0.37 | -0.41 | -0.29 | -0.13 | -0.03 | 0.01 | 0.16 | 0.12 | |
| 44.0 | -0.33 | -0.35 | -0.15 | -0.34 | -0.23 | -0.30 | -0.27 | -0.35 | -0.46 | -0.30 | -0.14 | -0.03 | -0.01 | 0.16 | | |
| 37.0 | -0.40 | -0.33 | -0.28 | -0.47 | -0.33 | -0.44 | -0.40 | -0.52 | -0.58 | -0.41 | -0.23 | -0.15 | -0.10 | | | |
| 32.2 | -0.35 | -0.38 | -0.32 | -0.47 | -0.38 | -0.43 | -0.35 | -0.47 | -0.60 | -0.36 | -0.25 | -0.10 | | | | |
| 28.6 | -0.32 | -0.39 | -0.13 | -0.16 | -0.35 | -0.32 | -0.21 | -0.36 | -0.37 | -0.24 | -0.13 | | | | | |
| 25.6 | -0.13 | -0.15 | 0.30 | 0.41 | -0.27 | -0.06 | -0.06 | -0.18 | 0.04 | -0.19 | | | | | | |
| 23.3 | -0.02 | 0.16 | 0.15 | 0.32 | -0.24 | 0.16 | 0.05 | -0.01 | 0.49 | | | | | | | |
| 21.3 | 0.12 | -0.27 | 0.34 | 0.41 | -0.42 | -0.18 | 0.07 | -0.03 | | | | | | | | |
| 19.6 | -0.37 | 0.10 | 0.04 | 0.05 | -0.00 | 0.26 | -0.03 | | | | | | | | | |
| 18.2 | -0.11 | 0.14 | 0.11 | 0.09 | -0.12 | -0.14 | | | | | | | | | | |
| 17.1 | -0.49 | 0.14 | 0.27 | 0.38 | 0.45 | | | | | | | | | | | |
| 16.2 | -0.05 | 0.40 | 0.52 | 0.60 | | | | | | | | | | | | |
| 15.1 | 0.07 | 0.24 | 0.78 | | | | | | | | | | | | | |
| 14.3 | 0.42 | 0.63 | | | | | | | | | | | | | | |
| 13.5 | 0.63 | | | | | | | | | | | | | | | |

ZN CORRELATION FOR SITE NUMBER 11

| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 62.5 | -0.30 | -0.18 | -0.01 | -0.20 | -0.28 | -0.24 | -0.14 | -0.63 | -0.25 | -0.44 | -0.35 | -0.36 | -0.38 | -0.21 | -0.02 | -0.08 |
| 50.0 | -0.21 | -0.03 | 0.08 | -0.07 | -0.11 | -0.09 | 0.05 | -0.53 | -0.20 | -0.34 | -0.24 | -0.37 | -0.34 | -0.14 | -0.16 | |
| 44.0 | -0.22 | -0.11 | -0.00 | -0.18 | -0.21 | -0.18 | -0.00 | -0.55 | -0.25 | -0.39 | -0.30 | -0.40 | -0.35 | -0.15 | | |
| 37.0 | -0.26 | -0.26 | -0.13 | -0.25 | -0.27 | -0.23 | 0.01 | -0.53 | -0.33 | -0.42 | -0.32 | -0.43 | -0.24 | | | |
| 32.2 | -0.34 | -0.35 | -0.27 | -0.33 | -0.30 | -0.25 | 0.04 | -0.47 | -0.31 | -0.36 | -0.27 | -0.20 | | | | |
| 28.6 | -0.15 | -0.08 | -0.07 | -0.00 | -0.04 | -0.08 | 0.35 | -0.31 | 0.09 | 0.01 | 0.13 | | | | | |
| 25.6 | 0.04 | 0.32 | 0.27 | 0.55 | 0.51 | 0.35 | 0.75 | 0.15 | 0.59 | 0.62 | | | | | | |
| 23.3 | 0.29 | 0.26 | 0.01 | 0.43 | 0.43 | 0.27 | 0.65 | 0.71 | 0.74 | | | | | | | |
| 21.3 | 0.05 | 0.36 | 0.18 | 0.51 | 0.53 | 0.21 | 0.68 | 0.35 | | | | | | | | |
| 19.6 | 0.28 | 0.11 | 0.01 | 0.24 | 0.30 | 0.22 | 0.73 | | | | | | | | | |
| 18.2 | 0.10 | 0.29 | 0.25 | 0.25 | 0.23 | 0.26 | | | | | | | | | | |
| 17.1 | 0.43 | 0.55 | 0.68 | 0.52 | 0.42 | | | | | | | | | | | |
| 16.2 | 0.47 | 0.70 | 0.71 | 0.76 | | | | | | | | | | | | |
| 15.1 | 0.13 | 0.70 | 0.86 | | | | | | | | | | | | | |
| 14.3 | 0.17 | 0.53 | | | | | | | | | | | | | | |
| 13.5 | 0.68 | | | | | | | | | | | | | | | |

ZE CORRELATION FOR SITE NUMBER 11

| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|-------|------|------|------|
| 62.5 | -0.07 | -0.12 | 0.06 | -0.10 | -0.35 | -0.24 | -0.23 | -0.38 | -0.15 | -0.34 | -0.27 | 0.10 | -0.18 | 0.05 | 0.32 | 0.44 |
| 50.0 | -0.13 | -0.27 | 0.00 | -0.13 | -0.37 | -0.21 | -0.30 | -0.30 | -0.23 | -0.34 | -0.36 | 0.14 | -0.04 | 0.13 | 0.45 | |
| 44.0 | -0.32 | -0.26 | 0.01 | 0.03 | -0.23 | -0.16 | -0.24 | -0.32 | -0.01 | -0.19 | -0.20 | 0.29 | 0.02 | 0.09 | | |
| 37.0 | -0.39 | -0.28 | -0.01 | 0.17 | -0.08 | -0.03 | -0.16 | -0.12 | 0.15 | 0.01 | -0.05 | 0.34 | 0.04 | | | |
| 32.2 | -0.43 | -0.40 | -0.08 | -0.00 | -0.24 | -0.18 | -0.37 | -0.27 | 0.00 | -0.17 | -0.20 | 0.26 | | | | |
| 28.6 | -0.08 | -0.33 | -0.08 | 0.03 | -0.22 | -0.17 | -0.08 | 0.08 | 0.18 | 0.05 | -0.13 | | | | | |
| 25.6 | -0.16 | -0.34 | -0.31 | -0.05 | -0.26 | -0.25 | -0.12 | 0.25 | 0.31 | 0.15 | | | | | | |
| 23.3 | 0.27 | 0.11 | -0.05 | 0.18 | 0.04 | -0.10 | 0.22 | 0.65 | 0.67 | | | | | | | |
| 21.3 | -0.31 | -0.31 | -0.15 | 0.14 | -0.05 | -0.06 | -0.24 | 0.17 | | | | | | | | |
| 19.6 | -0.41 | -0.34 | -0.11 | 0.22 | 0.02 | 0.02 | -0.06 | | | | | | | | | |
| 18.2 | -0.14 | -0.23 | 0.03 | 0.30 | 0.11 | 0.26 | | | | | | | | | | |
| 17.1 | -0.25 | -0.10 | 0.42 | 0.43 | 0.31 | | | | | | | | | | | |
| 16.2 | -0.14 | 0.43 | 0.68 | 0.55 | | | | | | | | | | | | |
| 15.1 | -0.36 | 0.31 | 0.71 | | | | | | | | | | | | | |
| 14.3 | 0.22 | 0.07 | | | | | | | | | | | | | | |
| 13.5 | -0.03 | | | | | | | | | | | | | | | |

NE CORRELATION

MATSUSHIRO, JAPAN

APPENDIX III-C (cont'd)

| PERIOD (Seconds) | PERIOD (Seconds) | | | | | | | | | | | | | | | |
|------------------|------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.2 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
| | 42.5 | 0.08 | 0.05 | -0.01 | 0.12 | 0.03 | -0.00 | -0.10 | -0.04 | 0.03 | 0.04 | 0.13 | 0.15 | 0.13 | 0.11 | 0.21 |
| | 50.0 | 0.16 | 0.12 | 0.02 | 0.17 | 0.06 | 0.04 | -0.06 | -0.00 | 0.08 | 0.07 | 0.17 | 0.17 | 0.14 | 0.14 | 0.23 |
| | 44.0 | 0.14 | 0.14 | 0.00 | 0.15 | 0.08 | 0.04 | -0.00 | 0.08 | 0.12 | 0.11 | 0.21 | 0.22 | 0.24 | 0.21 | |
| | 37.0 | 0.01 | -0.03 | -0.16 | 0.01 | -0.07 | -0.06 | -0.18 | -0.11 | -0.02 | -0.05 | 0.06 | 0.06 | 0.04 | | |
| | 32.2 | -0.02 | -0.07 | -0.10 | -0.02 | -0.06 | -0.00 | -0.13 | -0.08 | 0.04 | -0.02 | 0.08 | 0.10 | | | |
| | 28.6 | 0.06 | 0.03 | -0.10 | 0.01 | -0.02 | 0.02 | -0.08 | -0.02 | 0.11 | 0.05 | 0.14 | | | | |
| | 25.6 | 0.21 | 0.17 | 0.09 | 0.19 | 0.19 | 0.25 | 0.15 | 0.20 | 0.32 | 0.35 | | | | | |
| | 23.2 | 0.12 | 0.10 | -0.04 | 0.11 | 0.09 | 0.16 | 0.01 | 0.04 | 0.20 | | | | | | |
| | 21.3 | 0.19 | 0.20 | -0.01 | 0.16 | 0.19 | 0.23 | 0.11 | 0.15 | | | | | | | |
| 7N CORRELATION | 19.6 | 0.34 | 0.36 | 0.18 | 0.30 | 0.36 | 0.40 | 0.31 | | | | | | | | |
| | 18.2 | 0.32 | 0.32 | 0.15 | 0.27 | 0.30 | 0.35 | | | | | | | | | |
| | 17.1 | 0.34 | 0.33 | 0.21 | 0.27 | 0.31 | | | | | | | | | | |
| | 16.2 | 0.24 | 0.22 | 0.12 | 0.20 | | | | | | | | | | | |
| | 15.1 | 0.26 | 0.25 | 0.18 | | | | | | | | | | | | |
| | 14.3 | 0.25 | 0.23 | | | | | | | | | | | | | |
| | 13.5 | 0.30 | | | | | | | | | | | | | | |
| PERIOD (Seconds) | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.2 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
| | 62.5 | -0.43 | -0.54 | -0.45 | -0.53 | -0.54 | -0.46 | -0.61 | -0.56 | -0.43 | -0.42 | -0.34 | -0.46 | -0.24 | -0.19 | 0.08 |
| | 50.0 | -0.44 | -0.53 | -0.44 | -0.53 | -0.54 | -0.45 | -0.54 | -0.56 | -0.41 | -0.42 | -0.33 | -0.46 | -0.29 | -0.17 | 0.08 |
| | 44.0 | -0.22 | -0.20 | -0.22 | -0.24 | -0.20 | -0.25 | -0.45 | -0.39 | -0.28 | -0.24 | -0.14 | -0.22 | -0.09 | 0.10 | |
| | 37.0 | -0.40 | -0.42 | -0.27 | -0.44 | -0.40 | -0.45 | -0.52 | -0.52 | -0.38 | -0.38 | -0.26 | -0.38 | -0.20 | | |
| | 32.2 | -0.29 | -0.30 | -0.26 | -0.32 | -0.39 | -0.34 | -0.44 | -0.40 | -0.27 | -0.22 | -0.21 | -0.25 | | | |
| | 28.6 | -0.19 | -0.20 | -0.18 | -0.23 | -0.24 | -0.24 | -0.33 | -0.26 | -0.19 | -0.17 | -0.15 | | | | |
| | 25.6 | 0.03 | -0.05 | 0.01 | -0.02 | -0.05 | -0.01 | -0.11 | -0.08 | 0.06 | 0.06 | | | | | |
| | 23.2 | -0.09 | -0.08 | -0.03 | -0.08 | -0.12 | -0.03 | -0.09 | -0.07 | 0.03 | | | | | | |
| | 21.3 | 0.15 | 0.22 | 0.23 | 0.21 | 0.16 | 0.27 | 0.27 | 0.25 | | | | | | | |
| 7E CORRELATION | 19.6 | 0.46 | 0.53 | 0.52 | 0.54 | 0.51 | 0.57 | 0.58 | | | | | | | | |
| | 18.2 | 0.32 | 0.36 | 0.36 | 0.34 | 0.38 | 0.43 | | | | | | | | | |
| | 17.1 | 0.33 | 0.40 | 0.39 | 0.40 | 0.39 | | | | | | | | | | |
| | 16.2 | 0.37 | 0.45 | 0.44 | 0.44 | | | | | | | | | | | |
| | 15.1 | 0.43 | 0.52 | 0.49 | | | | | | | | | | | | |
| | 14.3 | 0.43 | 0.53 | | | | | | | | | | | | | |
| | 13.5 | 0.47 | | | | | | | | | | | | | | |
| PERIOD (Seconds) | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.2 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
| | 62.5 | 0.56 | 0.42 | 0.51 | 0.43 | 0.45 | 0.52 | 0.39 | 0.45 | 0.51 | 0.52 | 0.59 | 0.52 | 0.58 | 0.52 | 0.49 |
| | 50.0 | 0.56 | 0.41 | 0.50 | 0.43 | 0.46 | 0.54 | 0.41 | 0.46 | 0.63 | 0.51 | 0.58 | 0.50 | 0.56 | 0.51 | 0.47 |
| | 44.0 | 0.60 | 0.46 | 0.54 | 0.47 | 0.51 | 0.54 | 0.47 | 0.50 | 0.51 | 0.53 | 0.59 | 0.52 | 0.55 | 0.51 | |
| | 37.0 | 0.64 | 0.49 | 0.55 | 0.51 | 0.55 | 0.61 | 0.50 | 0.55 | 0.70 | 0.58 | 0.64 | 0.56 | 0.59 | | |
| | 32.2 | 0.61 | 0.45 | 0.52 | 0.49 | 0.51 | 0.59 | 0.46 | 0.52 | 0.66 | 0.57 | 0.63 | 0.51 | | | |
| | 28.6 | 0.61 | 0.45 | 0.52 | 0.49 | 0.52 | 0.59 | 0.49 | 0.53 | 0.68 | 0.56 | 0.63 | | | | |
| | 25.6 | 0.60 | 0.44 | 0.51 | 0.47 | 0.51 | 0.56 | 0.46 | 0.54 | 0.64 | 0.54 | | | | | |
| | 23.2 | 0.60 | 0.42 | 0.51 | 0.46 | 0.55 | 0.57 | 0.50 | 0.58 | 0.66 | | | | | | |
| | 21.3 | 0.64 | 0.48 | 0.55 | 0.54 | 0.60 | 0.62 | 0.54 | 0.62 | | | | | | | |
| 7E CORRELATION | 19.6 | 0.64 | 0.45 | 0.53 | 0.52 | 0.59 | 0.61 | 0.55 | | | | | | | | |
| | 18.2 | 0.57 | 0.41 | 0.48 | 0.46 | 0.52 | 0.59 | | | | | | | | | |
| | 17.1 | 0.55 | 0.37 | 0.46 | 0.42 | 0.51 | | | | | | | | | | |
| | 16.2 | 0.43 | 0.26 | 0.36 | 0.31 | | | | | | | | | | | |
| | 15.1 | 0.53 | 0.34 | 0.40 | | | | | | | | | | | | |
| | 14.3 | 0.45 | 0.30 | | | | | | | | | | | | | |
| | 13.5 | 0.40 | | | | | | | | | | | | | | |
| EILAT, ISRAEL | | | | | | | | | | | | | | | | |

APPENDIX III-D. INTER COMPONENT LINEAR CROSS CORRELATION COEFFICIENTS OF LOG AMPLITUDE (RMS MILLIMICRONS) NOISE AS A FUNCTION OF PERIOD AT VLPE STATION. HORIZONTAL AXIS DATA LISTS SECOND COMPONENT.

PERIOD (Seconds)

| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 62.5 | 0.40 | 0.24 | 0.25 | 0.34 | 0.19 | 0.28 | 0.22 | 0.10 | 0.11 | 0.30 | 0.26 | 0.32 | 0.21 | 0.17 | 0.27 | 0.20 |
| 50.0 | 0.29 | 0.23 | 0.21 | 0.25 | 0.12 | 0.18 | 0.15 | 0.09 | 0.18 | 0.38 | 0.29 | 0.31 | 0.28 | 0.26 | 0.20 | |
| 44.0 | 0.28 | 0.22 | 0.22 | 0.23 | 0.20 | 0.37 | 0.26 | 0.29 | 0.34 | 0.49 | 0.46 | 0.43 | 0.42 | 0.40 | | |
| 37.0 | 0.30 | 0.06 | 0.06 | 0.13 | 0.06 | 0.22 | 0.33 | 0.09 | 0.22 | 0.38 | 0.34 | 0.51 | 0.35 | | | |
| 32.2 | 0.25 | 0.12 | 0.10 | 0.23 | 0.07 | 0.16 | 0.23 | 0.20 | 0.27 | 0.50 | 0.53 | 0.54 | | | | |
| 28.6 | 0.22 | 0.09 | 0.05 | 0.16 | 0.02 | 0.13 | 0.26 | 0.29 | 0.29 | 0.55 | 0.45 | | | | | |
| 25.6 | 0.33 | 0.27 | 0.10 | 0.25 | 0.19 | 0.25 | 0.30 | 0.45 | 0.43 | 0.61 | | | | | | |
| 21.3 | 0.38 | 0.24 | 0.22 | 0.33 | 0.29 | 0.50 | 0.60 | 0.59 | 0.50 | | | | | | | |
| 21.3 | 0.16 | 0.14 | 0.24 | 0.37 | 0.36 | 0.55 | 0.61 | 0.72 | | | | | | | | |
| 19.6 | 0.30 | 0.20 | 0.34 | 0.42 | 0.49 | 0.64 | 0.64 | 0.67 | | | | | | | | |
| 18.2 | 0.46 | 0.45 | 0.49 | 0.58 | 0.61 | 0.74 | | | | | | | | | | |
| 17.1 | 0.51 | 0.49 | 0.56 | 0.68 | 0.70 | | | | | | | | | | | |
| 16.2 | 0.61 | 0.52 | 0.58 | 0.63 | | | | | | | | | | | | |
| 15.1 | 0.62 | 0.69 | 0.69 | | | | | | | | | | | | | |
| 14.3 | 0.74 | 0.76 | | | | | | | | | | | | | | |
| 13.5 | 0.68 | | | | | | | | | | | | | | | |

ZN CORRELATION

| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
|------|------|-------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 62.5 | 0.26 | 0.17 | 0.30 | 0.24 | 0.30 | 0.27 | 0.24 | 0.28 | 0.22 | 0.35 | 0.37 | 0.30 | 0.45 | 0.18 | 0.19 | 0.34 |
| 50.0 | 0.27 | 0.18 | 0.30 | 0.16 | 0.15 | 0.14 | 0.18 | 0.23 | 0.27 | 0.46 | 0.46 | 0.52 | 0.51 | 0.46 | 0.51 | |
| 44.0 | 0.20 | 0.10 | 0.23 | 0.26 | 0.25 | 0.27 | 0.23 | 0.48 | 0.43 | 0.55 | 0.52 | 0.46 | 0.57 | 0.45 | | |
| 37.0 | 0.09 | -0.06 | 0.12 | 0.28 | 0.27 | 0.19 | 0.22 | 0.34 | 0.23 | 0.56 | 0.60 | 0.44 | 0.58 | | | |
| 32.2 | 0.18 | -0.01 | 0.21 | 0.24 | 0.23 | 0.10 | 0.22 | 0.35 | 0.32 | 0.64 | 0.43 | 0.60 | | | | |
| 28.6 | 0.09 | -0.06 | 0.14 | 0.21 | 0.22 | 0.20 | 0.23 | 0.36 | 0.36 | 0.64 | 0.65 | | | | | |
| 25.6 | 0.16 | 0.07 | 0.19 | 0.23 | 0.29 | 0.25 | 0.32 | 0.50 | 0.50 | 0.65 | | | | | | |
| 21.3 | 0.17 | 0.02 | 0.22 | 0.40 | 0.54 | 0.52 | 0.55 | 0.72 | 0.65 | | | | | | | |
| 21.3 | 0.04 | 0.01 | 0.15 | 0.36 | 0.49 | 0.55 | 0.51 | 0.65 | | | | | | | | |
| 19.6 | 0.24 | 0.10 | 0.21 | 0.35 | 0.55 | 0.62 | 0.56 | | | | | | | | | |
| 18.2 | 0.40 | 0.27 | 0.42 | 0.53 | 0.65 | 0.73 | | | | | | | | | | |
| 17.1 | 0.47 | 0.33 | 0.50 | 0.62 | 0.78 | | | | | | | | | | | |
| 16.2 | 0.47 | 0.46 | 0.52 | 0.68 | | | | | | | | | | | | |
| 15.1 | 0.68 | 0.62 | 0.75 | | | | | | | | | | | | | |
| 14.3 | 0.74 | 0.74 | | | | | | | | | | | | | | |
| 13.5 | 0.68 | | | | | | | | | | | | | | | |

ZF CORRELATION

| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
|------|-------|-------|-------|-------|------|-------|-------|------|------|------|------|------|------|------|------|------|
| 62.5 | -0.00 | 0.01 | 0.04 | 0.09 | 0.21 | 0.14 | 0.11 | 0.22 | 0.28 | 0.31 | 0.35 | 0.45 | 0.34 | 0.71 | 0.68 | 0.72 |
| 50.0 | -0.07 | -0.04 | -0.08 | -0.04 | 0.07 | -0.03 | -0.02 | 0.13 | 0.23 | 0.22 | 0.25 | 0.43 | 0.26 | 0.71 | 0.67 | |
| 44.0 | 0.02 | 0.03 | 0.00 | 0.12 | 0.21 | 0.13 | 0.10 | 0.25 | 0.30 | 0.35 | 0.37 | 0.50 | 0.42 | 0.74 | | |
| 37.0 | 0.02 | 0.04 | 0.09 | 0.10 | 0.18 | 0.10 | 0.09 | 0.23 | 0.27 | 0.40 | 0.45 | 0.54 | 0.48 | | | |
| 32.2 | 0.09 | 0.07 | 0.12 | 0.16 | 0.25 | 0.14 | 0.13 | 0.28 | 0.29 | 0.43 | 0.49 | 0.54 | | | | |
| 28.6 | 0.14 | 0.14 | 0.13 | 0.19 | 0.22 | 0.16 | 0.12 | 0.31 | 0.38 | 0.51 | 0.61 | | | | | |
| 25.6 | 0.26 | 0.22 | 0.24 | 0.30 | 0.36 | 0.33 | 0.30 | 0.50 | 0.51 | 0.61 | | | | | | |
| 23.3 | 0.29 | 0.20 | 0.23 | 0.29 | 0.44 | 0.49 | 0.41 | 0.58 | 0.62 | | | | | | | |
| 21.3 | 0.43 | 0.29 | 0.38 | 0.49 | 0.62 | 0.67 | 0.68 | 0.77 | | | | | | | | |
| 19.6 | 0.47 | 0.31 | 0.50 | 0.61 | 0.76 | 0.74 | 0.87 | | | | | | | | | |
| 18.2 | 0.58 | 0.48 | 0.61 | 0.72 | 0.84 | 0.82 | | | | | | | | | | |
| 17.1 | 0.68 | 0.59 | 0.67 | 0.67 | 0.79 | | | | | | | | | | | |
| 16.2 | 0.70 | 0.67 | 0.77 | 0.78 | | | | | | | | | | | | |
| 15.1 | 0.73 | 0.71 | 0.70 | | | | | | | | | | | | | |
| 14.3 | 0.77 | 0.75 | | | | | | | | | | | | | | |
| 13.5 | 0.72 | | | | | | | | | | | | | | | |

NF CORRELATION

ALBUQUERQUE, NEW MEXICO

APPENDIX III-D (cont'd)

PERIOD (Seconds)

| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 62.5 | -.32 | -.36 | -.13 | -.35 | -.06 | -.14 | -.11 | -.24 | -.42 | -.18 | 0.07 | 0.31 | 0.32 | 0.49 | 0.37 | 0.60 |
| 50.0 | -.36 | -.29 | -.00 | -.21 | -.01 | -.10 | -.17 | -.41 | -.43 | -.33 | -.09 | 0.03 | 0.21 | 0.27 | 0.07 | |
| 44.0 | -.40 | -.37 | -.19 | -.39 | -.15 | -.21 | -.28 | -.47 | -.50 | -.37 | -.11 | 0.02 | 0.13 | 0.26 | | |
| 37.0 | -.53 | -.30 | -.36 | -.56 | -.26 | -.37 | -.53 | -.67 | -.70 | -.56 | -.20 | -.14 | -.19 | | | |
| 32.2 | -.44 | -.36 | -.35 | -.55 | -.32 | -.32 | -.40 | -.54 | -.66 | -.40 | -.17 | -.01 | | | | |
| 28.6 | -.37 | -.38 | -.20 | -.23 | -.36 | -.23 | -.17 | -.36 | -.35 | -.13 | 0.05 | | | | | |
| 25.6 | -.24 | -.08 | 0.11 | 0.17 | -.23 | -.09 | -.10 | -.28 | -.11 | -.12 | | | | | | |
| 23.3 | -.07 | 0.21 | 0.01 | 0.13 | -.19 | 0.12 | 0.03 | -.09 | 0.20 | | | | | | | |
| 21.3 | 0.12 | -.29 | 0.11 | 0.07 | -.50 | -.29 | 0.03 | -.09 | | | | | | | | |
| 19.6 | -.40 | 0.08 | 0.07 | 0.08 | 0.16 | 0.31 | 0.09 | | | | | | | | | |
| 18.2 | -.06 | 0.24 | 0.14 | 0.04 | -.06 | -.07 | | | | | | | | | | |
| 17.1 | -.52 | 0.16 | 0.24 | 0.41 | 0.50 | | | | | | | | | | | |
| 16.2 | -.06 | 0.42 | 0.36 | 0.48 | | | | | | | | | | | | |
| 15.1 | 0.11 | 0.30 | 0.66 | | | | | | | | | | | | | |
| 14.3 | 0.38 | 0.61 | | | | | | | | | | | | | | |
| 13.5 | 0.56 | | | | | | | | | | | | | | | |

ZN CORRELATION

| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 62.5 | -.38 | -.26 | -.04 | -.17 | -.34 | -.21 | -.14 | -.65 | -.21 | -.53 | -.49 | -.25 | -.42 | -.21 | 0.02 | -.01 |
| 50.0 | -.25 | -.00 | 0.10 | 0.08 | 0.00 | 0.10 | 0.20 | -.54 | -.19 | -.40 | -.31 | -.36 | -.39 | -.06 | -.12 | |
| 44.0 | -.26 | -.14 | -.05 | -.16 | -.21 | -.10 | 0.12 | -.85 | -.27 | -.43 | -.39 | -.39 | -.39 | -.11 | | |
| 37.0 | -.18 | -.24 | -.16 | -.33 | -.29 | -.17 | 0.11 | -.54 | -.36 | -.46 | -.40 | -.50 | -.26 | | | |
| 32.2 | -.29 | -.38 | -.37 | -.37 | -.35 | -.19 | 0.15 | -.41 | -.22 | -.30 | -.28 | -.28 | | | | |
| 28.6 | -.09 | -.05 | -.10 | 0.01 | -.06 | -.04 | 0.45 | -.25 | 0.27 | 0.13 | 0.22 | | | | | |
| 25.6 | 0.18 | 0.24 | 0.24 | 0.45 | 0.43 | 0.34 | 0.75 | 0.03 | 0.47 | 0.47 | | | | | | |
| 23.3 | 0.29 | 0.27 | -.03 | 0.36 | 0.42 | 0.35 | 0.86 | 0.50 | 0.56 | | | | | | | |
| 21.3 | 0.10 | 0.12 | 0.13 | 0.27 | 0.38 | 0.04 | 0.63 | 0.25 | | | | | | | | |
| 19.6 | 0.14 | 0.15 | 0.12 | 0.34 | 0.43 | 0.38 | 0.73 | | | | | | | | | |
| 18.2 | 0.13 | 0.38 | 0.29 | 0.35 | 0.35 | 0.36 | | | | | | | | | | |
| 17.1 | 0.46 | 0.54 | 0.65 | 0.65 | 0.51 | | | | | | | | | | | |
| 16.2 | 0.56 | 0.73 | 0.68 | 0.73 | | | | | | | | | | | | |
| 15.1 | 0.23 | 0.72 | 0.78 | | | | | | | | | | | | | |
| 14.3 | 0.31 | 0.60 | | | | | | | | | | | | | | |
| 13.5 | 0.73 | | | | | | | | | | | | | | | |

ZE CORRELATION

| | 13.5 | 14.3 | 15.1 | 16.2 | 17.1 | 18.2 | 19.6 | 21.3 | 23.3 | 25.6 | 28.6 | 32.2 | 37.0 | 44.0 | 50.0 | 62.5 |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 62.5 | -.15 | -.24 | 0.01 | -.09 | -.45 | -.27 | -.22 | -.36 | -.02 | -.34 | -.41 | 0.26 | -.11 | 0.19 | 0.47 | 0.48 |
| 50.0 | -.15 | -.34 | 0.03 | -.04 | -.38 | -.14 | -.33 | -.37 | -.15 | -.31 | -.34 | 0.26 | 0.08 | 0.21 | 0.55 | |
| 44.0 | -.35 | -.25 | 0.12 | 0.15 | -.20 | -.07 | -.20 | -.26 | 0.04 | -.22 | -.20 | 0.47 | 0.14 | 0.24 | | |
| 37.0 | -.35 | -.24 | 0.06 | 0.38 | -.01 | 0.18 | -.02 | -.07 | 0.19 | 0.01 | -.09 | 0.45 | 0.10 | | | |
| 32.2 | -.38 | -.32 | 0.14 | 0.18 | -.19 | -.06 | -.37 | -.38 | 0.05 | -.20 | -.16 | 0.40 | | | | |
| 28.6 | 0.04 | -.28 | 0.03 | 0.20 | -.18 | -.04 | 0.02 | 0.14 | 0.31 | 0.16 | -.10 | | | | | |
| 25.6 | 0.02 | -.24 | -.28 | 0.03 | -.28 | -.20 | -.04 | 0.44 | 0.52 | 0.35 | | | | | | |
| 23.3 | 0.27 | 0.10 | -.05 | 0.15 | -.03 | -.12 | 0.15 | 0.66 | 0.64 | | | | | | | |
| 21.3 | -.23 | -.29 | -.13 | 0.19 | -.05 | -.00 | -.27 | 0.34 | | | | | | | | |
| 19.6 | -.37 | -.35 | -.11 | 0.36 | 0.06 | 0.18 | 0.03 | | | | | | | | | |
| 18.2 | -.12 | -.25 | -.02 | 0.45 | 0.16 | 0.44 | | | | | | | | | | |
| 17.1 | -.24 | -.20 | 0.27 | 0.56 | 0.31 | | | | | | | | | | | |
| 16.2 | -.09 | 0.32 | 0.59 | 0.89 | | | | | | | | | | | | |
| 15.1 | -.40 | 0.17 | 0.63 | | | | | | | | | | | | | |
| 14.3 | 0.26 | 0.13 | | | | | | | | | | | | | | |
| 13.5 | -.04 | | | | | | | | | | | | | | | |

NE CORRELATION

MATSUSHIRO, JAPAN

APPENDIX III-D (cont'd)

APPENDIX V-A
DETERMINATION OF MINIMUM DISTANCE BETWEEN A GROUP
OF POINTS AND A STRAIGHT LINE

APPENDIX V-A

DETERMINATION OF MINIMUM DISTANCE BETWEEN A GROUP OF POINTS AND A STRAIGHT LINE

In describing the general trend of a group of $M_s : m_b$ measurements, it has been the practice to designate one of the magnitudes the independent variable and the other the dependent variable. Since each of these magnitude measurements are independent of the other, it would seem advantageous to obtain an unbiased description of the trend.

Examining Figure III-A, we see that we must determine α and β so that we minimize the distances between the points and the optimum line;

$$(1) \quad F = \sum_{i=1}^n d_i^2 \quad n = \text{total number of } M_s : m_b \text{ pairs}$$

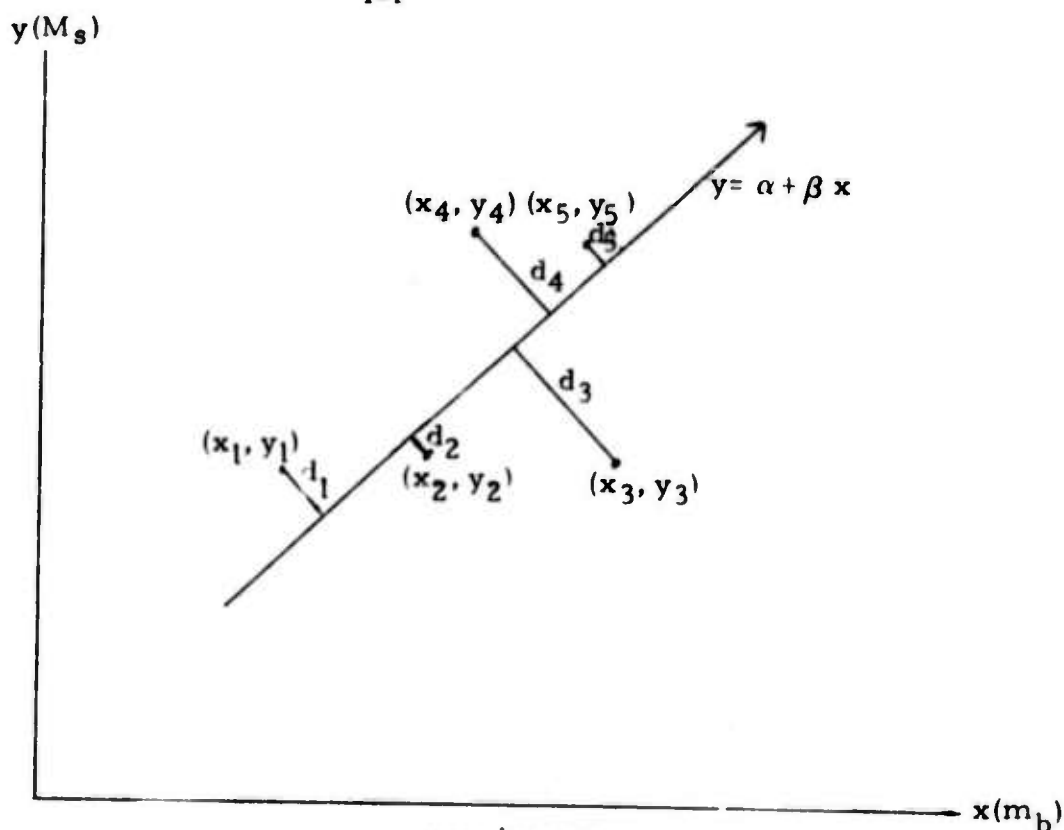


FIGURE III-A

It is quite easy to show that

$$(2) \quad d_i = \frac{|y_i - \beta x_i - \alpha|}{\sqrt{1 + \beta^2}}$$

Therefore, we can write (1) as

$$(3) \quad F = \sum_{i=1}^n \frac{(y_i - \beta x_i - \alpha)^2}{1 + \beta^2}$$

Expanding,

$$(4) \quad F = \frac{1}{1 + \beta^2} \sum_i (y_i^2 + \beta^2 x_i^2 + \alpha^2 - 2\alpha y_i + 2\alpha \beta x_i - 2\beta x_i y_i)$$

Differentiating (4) to obtain the minimum F with respect to α and β , we have

$$(5) \quad \frac{\partial F}{\partial \alpha} = \frac{1}{1 + \beta^2} \sum_i (2\alpha - 2y_i + 2\beta x_i)$$

$$(6) \quad \frac{\partial F}{\partial \beta} = \left[(1 + \beta^2) \left[\sum_i (2\beta x_i^2 + 2\alpha x_i - 2x_i y_i) \right] - 2\beta \left[\sum_i (y_i^2 + \beta^2 x_i^2 + \alpha^2 - 2\alpha y_i + 2\alpha \beta x_i - 2\beta x_i y_i) \right] \right] / (1 + \beta^2)^2$$

Setting (5) and (6) equal to zero

$$\frac{\partial F}{\partial \alpha} = 0; \quad \alpha = \frac{1}{n} \left[\sum y_i - \beta \sum x_i \right]$$

The center of mass of a group of points is defined as

$$\bar{y} = \frac{1}{n} \sum y_i, \quad \bar{x} = \frac{1}{n} \sum x_i$$

$$(7) \quad \alpha = \bar{y} - \beta \bar{x}$$

$$\text{For } \frac{\partial F}{\partial \beta} = 0$$

$$\frac{\partial F}{\partial \beta} = \sum_i [2\beta x_i^2 + 2\alpha x_i - 2x_i y_i - 2\beta y_i^2 - 2\beta \alpha^2 n + 4\beta \alpha y_i - 2\alpha \beta^2 x_i + 2\beta^2 x_i y_i] / [1 + \beta^2]^2 = 0$$

$$\text{Substituting from (7), then } \alpha = \frac{\sum y_i - \beta \sum x_i}{n}$$

$$\begin{aligned} \beta^2 \left(\sum x_i y_i - \frac{\sum x_i \sum y_i}{n} \right) + \beta \left(\sum x_i^2 - \frac{(\sum x_i)^2}{n} + \frac{(\sum y_i)^2}{n} - \sum y_i^2 \right) \\ + \left(\frac{\sum x_i \sum y_i}{n} - \sum x_i y_i \right) = 0 \end{aligned}$$

Or,

$$\begin{aligned} \beta^2 \left[\sum_{i=1}^n (x_i - \bar{x})(y_i - \bar{y}) \right] + \left[\sum_{i=1}^n (x_i - \bar{x})^2 - \sum_{i=1}^n (y_i - \bar{y})^2 \right] \\ - \sum_{i=1}^n (x_i - \bar{x})(y_i - \bar{y}) = 0 \end{aligned}$$

$$\text{Let } A = \sum_{i=1}^n (x_i - \bar{x})(y_i - \bar{y})$$

$$B = \sum_{i=1}^n (x_i - \bar{x})^2 - \sum_{i=1}^n (y_i - \bar{y})^2$$

$$C = - \sum_{i=1}^n (x_i - \bar{x})(y_i - \bar{y})$$

(8) Therefore
$$\beta = \frac{-B \pm \sqrt{B^2 - 4AC}}{2A}$$

The correct solution will be the one which minimizes F, and passes through the center of mass (\bar{x}, \bar{y}) .

APPENDIX V-B
NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)

NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
FOR WINTER EVENTS (1/1/72 - 3/20/72)

| Event Number | m _b | VLPE, NORSAR, and ALPA | | | VLPE | | |
|--------------|----------------|------------------------|------------------------|-------|------|------------------------|-------|
| | | n | Average M _s | S. D. | n | Average M _s | S. D. |
| 1 | 4.1 | 1 | 3.85 | - | 1 | 3.85 | - |
| 3 | 4.0 | 2 | 3.01 | - | | | |
| 5 | 4.2 | 1 | 2.46 | - | | | |
| 6 | 5.2 | 4 | 4.19 | 0.04 | 2 | 4.18 | |
| 7 | 4.8 | 5 | 3.79 | 0.42 | 3 | 3.94 | 0.36 |
| 10 | 4.3 | 1 | 2.60 | - | | | |
| 11 | 4.8 | 1 | 3.92 | - | | | |
| 13 | 4.6* | 3 | 4.53 | 0.40 | 2 | 4.53 | - |
| 14 | 3.9 | 2 | 4.23 | - | 2 | 4.23 | - |
| 16 | 4.5 | 2 | 3.04 | - | | | |
| 17 | 4.0 | 2 | 2.89 | - | 1 | 3.17 | - |
| 18 | 4.5 | 1 | 3.00 | - | | | |
| 19 | 4.0 | 2 | 3.97 | - | 2 | 3.97 | - |
| 20 | 3.9 | 1 | 2.80 | - | | | |
| 21 | 4.7 | 3 | 3.38 | 0.14 | 2 | 3.37 | - |
| 22 | 4.7 | 3 | 3.68 | 0.30 | 1 | 3.65 | - |
| 23 | 5.2 | 4 | 3.42 | 0.20 | 2 | 3.28 | - |
| 25 | 4.2 | 2 | 3.53 | - | 2 | 3.53 | - |
| 26 | 4.7 | 4 | 6.07 | 0.35 | 4 | 6.07 | 0.35 |
| 27 | 4.6 | 3 | 4.35 | 0.43 | 2 | 4.58 | - |
| 29 | 4.3 | 2 | 3.38 | - | 1 | 3.56 | - |
| 30 | 3.8 | 1 | 3.69 | - | 1 | 3.69 | - |
| 31 | 5.0 | 7 | 4.47 | 0.78 | 5 | 4.64 | 0.87 |
| 33 | 3.9 | 1 | 2.40 | - | | | |
| 34 | 4.0 | 1 | 3.93 | - | 1 | 3.93 | - |
| 35 | 4.4 | 3 | 3.72 | 0.93 | 3 | 3.72 | 0.93 |
| 36 | 4.9 | 6 | 3.95 | 0.35 | 4 | 3.82 | 0.37 |
| 37 | 4.8 | 6 | 4.21 | 0.16 | 4 | 4.27 | 0.15 |
| 38 | 4.0 | 5 | 4.09 | 0.34 | 5 | 4.09 | 0.34 |
| 39 | 5.3 | 6 | 5.04 | 0.27 | 4 | 5.11 | 0.21 |
| 40 | 3.9 | 5 | 3.38 | 0.39 | 3 | 3.63 | 0.14 |
| 41 | 5.1 | 3 | 3.61 | 0.05 | 2 | 3.58 | - |
| 43 | 4.7 | 6 | 3.39 | 0.30 | 4 | 3.46 | 0.22 |
| 46 | 3.8 | 1 | 2.50 | - | | | |
| 48 | 4.1 | 1 | 2.75 | - | | | |

NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
FOR WINTER EVENTS (1/1/72 - 3/20/72)

| Event Number | m_b | VLPE, NORSAR, and ALPA | | | VLPE | | |
|--------------|-------|------------------------|---------------|-------|------|---------------|-------|
| | | n | Average M_s | S. D. | n | Average M_s | S. D. |
| 50 | 4.9 | 5 | 3.79 | 0.25 | 3 | 3.91 | 0.19 |
| 52 | 4.8 | 3 | 3.66 | 0.28 | 1 | 3.41 | - |
| 54 | 4.2 | 1 | 2.40 | - | | | |
| 55 | 4.4 | 1 | 2.69 | - | | | |
| 56 | 4.2 | 1 | 2.50 | - | | | |
| 59 | 4.6 | 2 | 3.54 | - | 1 | 3.67 | - |
| 60 | 4.2* | 2 | 3.49 | - | 1 | 3.37 | |
| 61 | 4.8 | 3 | 3.69 | 0.32 | 2 | 3.83 | |
| 62 | 4.6 | 4 | 3.84 | 0.19 | 3 | 3.92 | 0.12 |
| 65 | 3.8 | 2 | 3.35 | - | 1 | 4.00 | |
| 68 | 4.0 | 1 | 3.18 | - | 1 | 3.18 | |
| 69 | 4.8 | 1 | 2.80 | - | | | |
| 70 | 3.8 | 1 | 2.40 | - | | | |
| 71 | 3.8 | 4 | 2.98 | 0.38 | 3 | 3.03 | 0.45 |
| 72 | 4.4 | 1 | 3.99 | - | | | |
| 73 | 5.9 | 7 | 3.99 | 0.14 | 5 | 4.00 | 0.15 |
| 75 | 4.5 | 1 | 2.77 | - | 1 | 2.77 | |
| 76 | 4.4 | 2 | 3.06 | - | 1 | 3.19 | |
| 78 | 3.8 | 1 | 3.19 | - | 1 | 3.19 | |
| 80 | 3.9 | 1 | 3.14 | - | | | |
| 81 | 3.9 | 6 | 3.77 | 0.30 | 4 | 3.73 | 0.26 |
| 82 | 4.1 | 1 | 2.40 | - | | | |
| 85 | 3.6 | 1 | 4.42 | - | 1 | 4.42 | |
| 87 | 4.6 | 7 | 3.47 | 0.11 | 5 | 3.51 | 0.12 |
| 88 | 5.1 | 6 | 4.43 | 0.32 | 4 | 4.43 | 0.35 |
| 89 | 4.5 | 7 | 4.12 | 0.30 | 5 | 4.10 | 0.35 |
| 90 | 4.5* | 7 | 3.83 | 0.46 | 5 | 3.89 | 0.55 |
| 91 | 4.2 | 1 | 3.37 | - | | | |
| 92 | 4.8 | 2 | 3.17 | - | 1 | 3.33 | |
| 93 | 4.8 | 2 | 3.37 | - | 1 | 3.53 | |
| 94 | 4.4 | 6 | 3.51 | 0.26 | 4 | 3.59 | 0.28 |
| 95 | 5.2 | 5 | 4.06 | 0.47 | 5 | 4.06 | 0.47 |
| 96 | 4.5 | 3 | 3.42 | 0.35 | 3 | 3.42 | 0.35 |
| 97 | 4.1* | 7 | 3.37 | 0.34 | 5 | 3.38 | 0.41 |
| 98 | 4.3* | 3 | 3.26 | 0.31 | 2 | 3.39 | |

NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
FOR WINTER EVENTS (1/1/72 - 3/20/72)

| Event Number | m_b | VLPE, NORSAR, and ALPA | | | VLPE | | |
|-----------------|-------|------------------------|------------------|-------|------|------------------|-------|
| | | n | Average M_s | S. D. | n | Average M_s | S. D. |
| 99 | 4.1* | 3 | 2.84 | 0.19 | 1 | 2.89 | |
| 100 | 3.6 | 2 | 2.77 | - | 2 | 2.77 | |
| 102 | 3.7* | 1 | 2.33 | - | | | |
| 103 | 4.0* | 3 | 3.02 | 0.18 | 1 | 3.20 | |
| 104 | 4.3* | 6 | 3.42 | 0.28 | 4 | 3.56 | 0.22 |
| 105 | 4.2* | 7 | 3.62 | 0.19 | 5 | 3.69 | 0.18 |
| 106 | 4.4* | 5 | 3.31 | 0.15 | 4 | 3.36 | 0.12 |
| 108 | 4.7 | 1 | 3.20 | - | | | |
| 111 | 4.8 | 3 | 3.64 | 0.62 | 2 | 3.91 | |
| 112 | 5.7 | 6 | 4.93 | 0.31 | 5 | 4.95 | 0.34 |
| 113 | 4.3* | 1 | 2.48 | - | | | |
| 114 | 4.8 | 5 | 3.70 | 0.18 | 4 | 3.75 | 0.16 |
| 116 | 5.5 | 1 | 2.75 | | | | |
| 117 | 4.5 | 3 | 3.37 | 0.58 | 2 | 3.71 | - |
| 118 | 3.9 | 2 | 3.23 | - | | | |
| 119 | 4.1 | 4 | 3.38 | 0.18 | 2 | 3.50 | - |
| 120 | 4.9 | 4 | 4.25 | 0.22 | 2 | 4.41 | - |
| 121 | 4.3 | 2 | 2.87 | - | 1 | 2.63 | |
| 122 | 3.9 | 3 | 3.16 | 0.83 | 2 | 3.64 | |
| 123 | 4.6 | 6 | 3.85 | 0.21 | 4 | 3.90 | 0.22 |
| 125 | 4.5 | 3 | 3.30 | 0.12 | 1 | 3.35 | |
| 126 | 3.9 | 1 | 3.82 | - | | 3.82 | |
| 127 | 4.1 | 2 | 2.75 | - | | | |
| 128 | 4.5 | 1 | 2.89 | - | | | |
| 129 | 4.8 | 4 | 3.67 | 0.25 | 2 | 3.55 | |
| 130 | 3.7 | 1 | 2.40 | - | | | |
| 131 | 4.7 | 4 | 3.46 | 0.38 | 2 | 3.48 | |
| 132 | 4.0 | 1 | 2.40 | - | | | |
| 133 | 5.2 | 3 | 3.94 | 0.38 | 3 | 3.94 | 0.38 |
| 134 | 5.4 | 3 | 4.83 | 0.13 | 3 | 4.83 | 0.13 |
| 137 | 3.9 | 1 | 3.21 | - | | | |
| 138 | 4.1 | 1 | 3.18 | - | | | |
| 139 | 4.8 | 4 | 3.70 | 0.23 | 2 | 3.76 | |
| 140 | 3.5 | 1 | 3.64 | - | | 3.64 | |
| 141 | 5.3 | 4 | 4.06 | 0.18 | 3 | 4.07 | 0.22 |

NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
FOR WINTER EVENTS (1/1/72 - 3/20/72)

| Event Number | m_b | VLPE, NORSAR, and ALPA | | | VLPE | | |
|--------------|-------|------------------------|---------------|-------|------|---------------|-------|
| | | n | Average M_s | S. D. | n | Average M_s | S. D. |
| 143 | 3.4 | 3 | 3.15 | 0.72 | 2 | 3.53 | |
| 144 | 4.0 | 2 | 3.26 | - | 1 | 3.30 | |
| 145 | 4.8 | 4 | 3.67 | 0.28 | 2 | 3.64 | 0.19 |
| 146 | 4.7 | 4 | 3.62 | 0.23 | 2 | 3.59 | |
| 147 | 4.9 | 5 | 3.58 | 0.40 | 3 | 3.53 | 0.42 |
| 148 | 3.7 | 1 | 2.30 | - | | | |
| 151 | 4.3 | 1 | 3.10 | - | 1 | 3.10 | |
| 153 | 4.5 | 1 | 2.70 | - | | | |
| 156 | 5.0 | 5 | 4.42 | 0.44 | 3 | 4.39 | 0.42 |
| 164 | 4.0 | 2 | 2.91 | - | | | |
| 165 | 4.9 | 5 | 4.26 | 0.39 | 3 | 4.17 | 0.35 |
| 167 | 4.9 | 3 | 3.23 | 0.32 | 1 | 3.27 | |
| 169 | 3.8 | 3 | 3.02 | 0.48 | 2 | 3.28 | |
| 171 | 4.7 | 4 | 3.57 | 0.68 | 2 | 3.24 | |
| 172 | 5.3 | 4 | 4.60 | 0.68 | 3 | 4.74 | 0.81 |
| 175 | 4.9 | 5 | 4.05 | 0.23 | 3 | 4.12 | 0.30 |
| 179 | 4.4 | 4 | 3.03 | 0.19 | 2 | 3.19 | |
| 181 | 4.5 | 1 | 3.14 | - | | | |
| 184 | 4.1 | 1 | 2.50 | - | | | |
| 186 | 3.9 | 3 | 2.80 | 0.40 | 2 | 2.75 | |
| 189 | 4.4 | 2 | 3.16 | - | 1 | 3.11 | |
| 192 | 3.8 | 1 | 3.03 | - | 1 | 3.03 | |
| 193 | 4.4 | 3 | 3.53 | 0.66 | 2 | 3.34 | |
| 200 | 4.4 | 1 | 4.11 | - | 1 | 4.11 | |
| 205 | 3.6 | 3 | 3.45 | 0.57 | 2 | 3.68 | |
| 208 | 4.1 | 1 | 3.32 | - | 1 | 3.32 | |
| 211 | 3.4 | 1 | 2.30 | - | | | |
| 214 | 4.0 | 1 | 3.76 | - | 1 | 3.76 | |
| 218 | 3.7 | 1 | 3.26 | - | 1 | 3.26 | |
| 220 | 3.5 | 1 | 2.30 | - | | | |
| 223 | 4.3* | 2 | 3.73 | - | 2 | 3.73 | |
| 224 | 4.0 | 2 | 3.21 | - | 1 | 3.32 | |
| 226 | 4.6 | 1 | 2.60 | - | | | |
| 227 | 4.1 | 1 | 2.50 | - | | | |
| 228 | 4.6 | 1 | 2.60 | - | | | |

NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
FOR WINTER EVENTS (1/1/72 - 3/20/72)

| Event Number | m_b | VLPE, NORSAR, and ALPA | | | VLPE | | |
|--------------|-------|------------------------|---------------|-------------|-------------|---------------|-------|
| | | n | Average M_s | S. D. | n | Average M_s | S. D. |
| 229 | 3.8 | 1 | 2.20 | - | | | |
| 230 | 4.1 | 1 | 2.30 | - | | | |
| 232 | 4.4* | 4 | 3.12 | 0.31 | 2 | 2.93 | |
| 233 | 4.5 | 3 | 3.41 | 0.40 | 1 | 3.42 | |
| 235 | 4.5 | 2 | 3.72 | - | | | |
| 236 | 4.4 | 1 | 3.40 | - | | | |
| 237 | 3.6 | 1 | 3.14 | - | 1 | 3.14 | |
| 238 | 5.1 | 1 | 3.00 | - | | | |
| 241 | 3.9 | 2 | 2.67 | - | 1 | 2.93 | |
| 243 | 5.4 | 2 | 4.09 | - | 1 | 4.17 | |
| 254 | 4.2 | 2 | 2.99 | - | 1 | 3.18 | |
| 255 | 4.6* | 4 | 3.66 | 0.12 | 2 | 3.63 | |
| 256 | 3.5 | 3 | 3.23 | 0.28 | 2 | 3.39 | |
| 260 | 5.5 | 4 | 3.34 | 0.19 | 2 | 3.49 | |
| 262 | 4.9 | 2 | 4.11 | - | 2 | 4.11 | |
| 264 | 3.8 | 1 | 3.25 | - | 1 | 3.25 | |
| 266 | 3.6 | 2 | 3.21 | - | 1 | 3.42 | |
| 273 | 3.8 | 1 | 3.30 | - | | | |
| 275 | 4.1 | 1 | 2.90 | - | | | |
| 278 | 3.7 | 2 | 4.74 | - | 2 | 4.74 | |
| 280 | 3.7 | 1 | 2.90 | - | | | |
| 281 | 5.3 | 4 | 3.54 | 0.28 | 2 | 3.45 | |
| 286 | 4.5 | 3 | 4.42 | 0.61 | 3 | 4.42 | 0.61 |
| 288 | 3.4 | 1 | 2.98 | - | 1 | 2.98 | |
| 289 | 3.6 | 2 | 3.08 | - | 2 | 3.08 | |
| 290 | 3.5 | 1 | 3.83 | - | 1 | 3.83 | |
| 292 | 5.2 | 4 | 3.84 | 0.22 | 2 | 4.01 | |
| 294 | 5.2 | 6 | 4.53 | 0.36 | 4 | 4.46 | 0.44 |
| 296 | 3.5 | 2 | 2.67 | - | 1 | 2.54 | |
| 297 | 5.0 | 2 | 3.81 | - | 1 | 3.92 | |
| 298 | 3.6 | 2 | 3.31 | - | 1 | 3.71 | |
| 299 | 3.6 | 1 | 3.20 | - | 1 | 3.20 | |
| 300 | 4.7 | 5 | 3.50 | 0.58 | 3 | 3.64 | 0.76 |
| 303 | 3.9 | 1 | 2.70 | - | | | |
| 308 | 3.4 | 3 | 3.35 | 0.52 | 3 | 3.35 | 0.52 |
| | | | | S. D. 0.341 | S. D. 0.352 | | |

NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
FOR SUMMER EVENTS (6/1/72 - 7/31/72)

| Event Number | m_b | VLPE, NORSAR, and ALPA | | | VLPE | | |
|--------------|-------|------------------------|---------------|-------|------|---------------|-------|
| | | n | Average M_s | S. D. | n | Average M_s | S. D. |
| 310 | 3.9 | 2 | 2.90 | | | | |
| 311 | 3.6 | 4 | 3.43 | 0.60 | 3 | 3.64 | 0.52 |
| 312 | 3.7 | 3 | 3.17 | 0.39 | 1 | 3.62 | |
| 314 | 3.8 | 2 | 3.00 | | | | |
| 315 | 4.1 | 2 | 3.12 | - | 1 | 3.03 | |
| 316 | 3.8 | 2 | 3.54 | - | 1 | 4.18 | |
| 319 | 3.5 | 2 | 3.27 | - | 1 | 3.64 | |
| 320 | 3.9 | 3 | 3.42 | 0.73 | 1 | 4.27 | |
| 321 | 3.7 | 3 | 3.56 | 0.19 | 1 | 3.77 | |
| 322 | 4.3 | 2 | 3.33 | - | 1 | 3.56 | |
| 323 | 5.0* | 5 | 4.25 | 0.45 | 3 | 4.34 | 0.09 |
| 324 | 4.2 | 3 | 3.24 | 0.61 | 1 | 3.81 | |
| 325 | 4.2 | 1 | 2.90 | | | | |
| 326 | 4.0 | 2 | 2.80 | | | | |
| 327 | 3.4 | 1 | 3.38 | - | 1 | 3.38 | |
| 328 | 3.5 | 1 | 3.49 | - | 1 | 3.49 | |
| 329 | 4.1 | 2 | 2.75 | | | | |
| 330 | 3.5 | 2 | 3.47 | - | 1 | 3.83 | |
| 331 | 4.0 | 2 | 2.90 | | | | |
| 332 | 4.3* | 5 | 3.71 | 0.17 | 3 | 3.79 | 0.19 |
| 333 | 3.9 | 4 | 2.79 | 0.23 | 2 | 2.62 | |
| 334 | 4.8 | 3 | 3.26 | 0.25 | 1 | 3.27 | |
| 335 | 4.0 | 5 | 3.24 | 0.23 | 3 | 3.37 | 0.21 |
| 338 | 4.7 | 3 | 3.53 | 0.06 | 2 | 3.50 | |
| 339 | 5.5 | 1 | 3.40 | | | | |
| 341 | 5.4 | 5 | 4.86 | 0.71 | 4 | 5.10 | 0.54 |
| 342 | 4.9 | 2 | 4.50 | - | 2 | 4.50 | |
| 343 | 4.9 | 4 | 4.04 | 0.41 | 2 | 3.94 | |
| 344 | 4.1 | 2 | 2.90 | | | | |
| 345 | 4.3 | 1 | 3.70 | | | | |
| 346 | 4.7 | 3 | 3.63 | 0.35 | 3 | 3.63 | 0.35 |
| 347 | 4.5 | 1 | 4.22 | - | 1 | 4.22 | |
| 348 | 4.7 | 3 | 4.16 | 0.54 | 1 | 4.78 | |
| 349 | 4.4 | 1 | 4.05 | - | 1 | 4.05 | |
| 350 | 4.9 | 8 | 3.71 | 0.53 | 6 | 3.60 | 0.58 |

NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
FOR SUMMER EVENTS (6/1/72 - 7/31/72)

| Event Number | m_b | VLPE, NORSAR, and ALPA | | | VLPE | | |
|--------------|-------|------------------------|---------------|-------|------|---------------|-------|
| | | n | Average M_s | S. D. | n | Average M_s | S. D. |
| 351 | 4.9 | 5 | 4.49 | 0.43 | 5 | 4.49 | 0.43 |
| 352 | 4.0 | 1 | 3.88 | - | 1 | 3.88 | |
| 354 | 4.5 | 5 | 3.66 | 0.18 | 3 | 3.57 | 0.19 |
| 355 | 3.7 | 2 | 2.60 | | | | |
| 356 | 4.0 | 2 | 3.15 | | | | |
| 357 | 3.3 | 2 | 2.35 | | | | |
| 361 | 5.4 | 4 | 4.74 | 0.25 | 2 | 4.73 | |
| 362 | 5.1 | 3 | 4.69 | 0.51 | 3 | 4.69 | 0.51 |
| 364 | 5.1 | 3 | 4.04 | 0.20 | 1 | 3.81 | |
| 365 | 3.8 | 2 | 2.80 | - | 1 | 3.29 | |
| 366 | 4.7 | 3 | 3.69 | 0.28 | 2 | 3.69 | |
| 367 | 5.3 | 3 | 4.00 | 0.10 | 1 | 4.10 | |
| 368 | 3.6 | 1 | 2.10 | | | | |
| 369 | 3.5 | 2 | 3.26 | - | 2 | 3.26 | |
| 370 | 3.6 | 1 | 3.00 | | | | |
| 371 | 4.5* | 4 | 4.11 | 0.10 | 3 | 4.14 | 0.09 |
| 372 | 4.3* | 2 | 2.91 | 0.15 | 1 | 3.01 | |
| 373 | 4.9 | 3 | 4.04 | 0.33 | 2 | 3.97 | |
| 374 | 3.5 | 1 | 3.50 | - | 1 | 3.50 | |
| 375 | 3.3 | 1 | 2.93 | - | 1 | 2.93 | |
| 376 | 4.1 | 1 | 2.40 | | | | |
| 379 | 3.7 | 2 | 2.95 | | | | |
| 380 | 4.6 | 3 | 2.79 | 0.01 | 1 | 2.78 | |
| 381 | 4.6 | 4 | 3.34 | 0.24 | 2 | 3.49 | |
| 382 | 4.3 | 3 | 3.65 | 0.19 | 1 | 3.44 | |
| 383 | 3.9 | 1 | 2.50 | | | | |
| 384 | 4.3 | 1 | 2.80 | | | | |
| 385 | 4.4 | 4 | 2.73 | 0.19 | 2 | 2.81 | |
| 386 | 5.0 | 3 | 4.10 | 0.43 | 2 | 4.15 | |
| 388 | 4.5 | 3 | 3.39 | 0.40 | 2 | 3.24 | |
| 389 | 4.1 | 2 | 2.55 | | | | |
| 390 | 4.0 | 1 | 3.46 | - | 1 | 3.46 | |
| 391 | 3.7 | 2 | 2.45 | | | | |
| 392 | 3.6 | 1 | 3.85 | - | 1 | 3.85 | |
| 393 | 4.3 | 2 | 3.24 | - | 1 | 3.37 | |

NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
FOR SUMMER EVENTS (6/1/72 - 7/31/72)

| Event Number | m_b | VLPE, NORSAR, and ALPA | | | VLPE | | |
|--------------|-------|------------------------|---------------|-------|------|---------------|-------|
| | | n | Average M_s | S. D. | n | Average M_s | S. D. |
| 394 | 3.7 | 1 | 2.70 | | | | |
| 395 | 4.1 | 2 | 3.05 | | | | |
| 396 | 4.3 | 3 | 2.78 | 0.23 | 1 | 3.03 | |
| 399 | 4.5 | 1 | 3.93 | - | 1 | 3.93 | |
| 400 | 3.7 | 2 | 2.75 | | | | |
| 401 | 3.4 | 1 | 2.40 | | | | |
| 402 | 4.6 | 4 | 3.23 | 0.36 | 2 | 3.28 | |
| 403 | 3.7 | 1 | 2.70 | | | | |
| 404 | 3.5 | 1 | 3.00 | | | | |
| 405 | 4.5* | 3 | 3.20 | 0.27 | 2 | 3.35 | |
| 406 | 6.0 | 1 | 6.00 | | | | |
| 409 | 3.7* | 2 | 2.65 | | | | |
| 410 | 4.7 | 6 | 4.02 | 0.34 | 4 | 3.03 | 0.36 |
| 411 | 4.1 | 4 | 3.58 | 0.37 | 2 | 3.82 | |
| 412 | 5.0 | 6 | 4.37 | 0.32 | 4 | 4.36 | 0.25 |
| 413 | 3.6 | 1 | 2.40 | | | | |
| 414 | 3.7 | 3 | 3.03 | 0.23 | 1 | 3.29 | |
| 415 | 4.0 | 2 | 2.82 | - | 1 | 3.03 | |
| 416 | 5.5 | 6 | 4.30 | 0.47 | 4 | 4.20 | 0.47 |
| 417 | 3.8 | 1 | 3.60 | | | | |
| 418 | 4.4 | 3 | 3.91 | 0.02 | 1 | 3.93 | |
| 419 | 5.2* | 5 | 3.99 | 0.52 | 3 | 3.98 | 0.62 |
| 421 | 5.1 | 5 | 4.28 | 0.25 | 3 | 4.31 | 0.32 |
| 422 | 4.6* | 3 | 3.18 | 0.68 | 2 | 3.47 | |
| 423 | 3.6 | 2 | 2.95 | | | | |
| 424 | 4.2 | 2 | 2.45 | | | | |
| 425 | 3.4 | 1 | 2.00 | | | | |
| 426 | 4.3 | 2 | 3.13 | - | 1 | 3.46 | |
| 427 | 5.6 | 6 | 4.83 | 0.17 | 4 | 4.87 | 0.16 |
| 428 | 3.9 | 2 | 2.50 | | | | |
| 429 | 3.9 | 1 | 4.08 | - | 1 | 4.08 | |
| 430 | 3.7 | 2 | 2.55 | | | | |
| 431 | 4.6* | 3 | 3.84 | 0.10 | 1 | 3.73 | |
| 432 | 4.4 | 2 | 3.67 | - | 1 | 3.94 | |
| 433 | 4.9 | 5 | 4.24 | 0.45 | 3 | 4.23 | 0.31 |

NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
FOR SUMMER EVENTS (6/1/72 - 7/31/72)

| Event Number | m_b | VLPE, NORSAR, and ALPA | | | VLPE | | |
|--------------|-------|------------------------|---------------|-------|------|---------------|-------|
| | | n | Average M_s | S. D. | n | Average M_s | S. D. |
| 434 | 4.0 | 1 | 2.80 | | | | |
| 435 | 3.4 | 1 | 2.40 | | | | |
| 436 | 5.4 | 3 | 4.94 | 0.22 | 1 | 4.83 | |
| 437 | 4.6 | 3 | 3.47 | 0.16 | 1 | 3.62 | |
| 438 | 5.0 | 4 | 3.90 | 0.24 | 3 | 3.87 | 0.28 |
| 439 | 4.3 | 1 | 2.70 | | | | |
| 440 | 4.0 | 1 | 2.80 | | | | |
| 441 | 4.0 | 2 | 3.29 | - | 1 | 3.48 | |
| 442 | 5.1 | 3 | 3.89 | 0.10 | 1 | 3.86 | |
| 444 | 3.4 | 2 | 2.80 | | | | |
| 445 | 3.9 | 1 | 3.00 | | | | |
| 446 | 4.4 | 3 | 3.11 | 0.34 | 1 | 3.40 | |
| 447 | 3.6 | 1 | 2.70 | | | | |
| 449 | 4.6 | 5 | 3.87 | 0.17 | 3 | 3.84 | 0.23 |
| 450 | 3.5 | 1 | 2.80 | | | | |
| 451 | 4.3 | 3 | 3.37 | 0.30 | 1 | 3.70 | |
| 452 | 3.4 | 1 | 3.67 | - | 1 | 3.67 | |
| 453 | 4.0 | 3 | 3.30 | 0.09 | 1 | 3.27 | |
| 454 | 4.7 | 2 | 3.04 | - | 1 | 3.10 | |
| 455 | 4.1 | 2 | 2.85 | | | | |
| 456 | 4.4 | 2 | 2.89 | - | 1 | 3.17 | |
| 457 | 3.1 | 3 | 2.80 | 0.10 | 1 | 2.70 | |
| 458 | 4.3 | 1 | 3.67 | - | 1 | 3.67 | |
| 460 | 3.7 | 1 | 2.70 | | | | |
| 461 | 5.0 | 3 | 4.59 | 0.09 | 3 | 4.59 | 0.09 |
| 462 | 3.7 | 1 | 3.70 | | | | |
| 463 | 4.7 | 1 | 2.70 | | | | |
| 464 | 4.9 | 3 | 4.02 | 0.06 | 3 | 4.02 | 0.06 |
| 465 | 4.2 | 1 | 3.10 | | | | |
| 466 | 4.0 | 2 | 2.53 | - | 1 | 2.55 | |
| 467 | 4.1 | 3 | 3.34 | 0.65 | 2 | 3.72 | |
| 469 | 4.1 | 1 | 2.77 | | | | |
| 470 | 4.7 | 3 | 3.55 | 0.14 | 1 | 3.42 | |
| 471 | 4.2 | 1 | 2.90 | | | | |
| 472 | 5.2 | 6 | 3.86 | 0.28 | 4 | 3.96 | 0.13 |

NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
FOR SUMMER EVENTS (6/1/72 - 7/31/72)

| Event Number | m_b | VLPE, NORSAR, and ALPA | | | VLPE | | |
|--------------|-------|------------------------|---------------|-------|------|---------------|-------|
| | | n | Average M_s | S. D. | n | Average M_s | S. D. |
| 473 | 3.6 | 1 | 2.52 | | | | |
| 474 | 3.7 | 1 | 2.80 | | | | |
| 475 | 4.7 | 4 | 3.72 | 0.26 | 2 | 3.86 | |
| 476 | 5.2 | 6 | 3.94 | 0.34 | 4 | 4.05 | 0.23 |
| 477 | 3.5 | 1 | 3.10 | | | | |
| 479 | 4.1 | 2 | 3.34 | - | 2 | 3.34 | |
| 481 | 3.9 | 1 | 3.20 | | | | |
| 482 | 4.2 | 4 | 3.50 | 0.26 | 2 | 3.68 | |
| 483 | 3.7 | 1 | 3.30 | | | | |
| 485 | 3.8 | 2 | 3.43 | | | | |
| 486 | 3.9 | 1 | 3.00 | | | | |
| 487 | 4.4 | 2 | 3.06 | | | | |
| 488 | 3.9 | 1 | 2.70 | | | | |
| 489 | 3.4 | 1 | 2.79 | | | | |
| 490 | 3.9 | 1 | 2.50 | | | | |
| 491 | 3.8 | 2 | 2.85 | | | | |
| 492 | 5.1 | 5 | 4.22 | 0.33 | 3 | 4.24 | 0.50 |
| 493 | 4.4 | 2 | 2.81 | 0.44 | 1 | 3.12 | |
| 494 | 3.7 | 1 | 2.20 | | | | |
| 495 | 3.5 | 1 | 2.40 | | | | |
| 496 | 5.2 | 5 | 4.18 | 0.36 | 3 | 4.20 | 0.48 |
| 497 | 4.9 | 5 | 4.34 | 0.16 | 3 | 4.31 | 0.23 |
| 498 | 4.7 | 2 | 3.70 | | | | |
| 499 | 4.6 | 7 | 3.83 | 0.44 | 5 | 3.83 | 0.21 |
| 501 | 4.2 | 2 | 3.05 | | | | |
| 502 | 3.9 | 2 | 3.16 | - | 1 | 3.62 | |
| 503 | 4.2 | 2 | 3.54 | - | 2 | 3.54 | |
| 504 | 3.9 | 1 | 3.00 | | | | |
| 505 | 5.3 | 7 | 3.91 | 0.57 | 5 | 4.05 | 0.58 |
| 506 | 3.3 | 1 | 2.00 | | | | |
| 507 | 3.4 | 1 | 3.00 | | | | |
| 508 | 4.1 | 1 | 3.87 | - | 1 | 3.87 | |
| 509 | 4.5 | 1 | 2.80 | | | | |
| 510 | 4.0 | 2 | 2.75 | | | | |
| 511 | 3.7 | 1 | 2.60 | | | | |

NETWORK RAYLEIGH WAVE MAGNITUDES (M_s)
FOR SUMMER EVENTS (6/1/72 - 7/31/72)

| Event Number | m_b | VLPE, NORSAR, and ALPA | | | VLPE | | |
|-----------------|-------|------------------------|------------------|--------------------------|--------------------------|------------------|-------|
| | | n | Average M_s | S. D. | n | Average M_s | S. D. |
| 512 | 4.0 | 3 | 3.00 | 0.20 | 1 | 3.19 | 0.14 |
| 513 | 5.2 | 2 | 4.02 | - | 2 | 4.02 | |
| 516 | 3.6 | 1 | 2.80 | | | | |
| 517 | 3.9 | 2 | 3.49 | - | 1 | 3.83 | |
| 518 | 4.3 | 1 | 3.38 | | | | |
| 520 | 4.8 | 1 | 4.20 | | | | |
| 521 | 4.6 | 4 | 3.68 | 0.34 | 2 | 3.41 | |
| 522 | 5.5 | 6 | 5.02 | 0.18 | 4 | 4.96 | |
| 523 | 4.7 | 2 | 3.04 | | | | |
| 524 | 3.9 | 1 | 2.90 | | | | |
| 525 | 3.6 | 2 | 3.00 | | | | |
| 526 | 3.7 | 1 | 2.87 | | | | |
| 527 | 4.4 | 3 | 3.06 | 0.06 | 1 | 3.09 | 0.50 |
| 528 | 4.0 | 1 | 3.30 | | | | |
| 529 | 4.8 | 2 | 3.57 | | | | |
| 530 | 4.5 | 2 | 3.38 | - | 1 | 3.55 | |
| 531 | 4.3 | 1 | 2.40 | | | | |
| 532 | 4.0 | 2 | 3.14 | | | | |
| 534 | 5.1 | 4 | 4.33 | 0.25 | 2 | 4.32 | |
| 535 | 5.1 | 4 | 4.36 | 0.18 | 2 | 4.31 | |
| 537 | 3.8 | 1 | 2.80 | | | | |
| 538 | 3.8 | 2 | 3.43 | | | | |
| 539 | 4.8 | 4 | 3.66 | 0.43 | 2 | 3.57 | |
| 541 | 5.1 | 3 | 4.21 | 0.50 | 3 | 4.21 | |
| 543 | 4.9 | 2 | 3.74 | - | 1 | 3.72 | |
| 546 | 4.8 | 3 | 3.53 | 0.14 | 1 | 3.61 | |
| 547 | 4.6 | 1 | 4.44 | - | 1 | 4.44 | |
| 548 | 3.6 | 2 | 2.75 | | | | |
| | | | | $\overline{S. D.}$ 0.295 | $\overline{S. D.}$ 0.328 | | |